

of the rapid changes this value must be taken to be the LMT for the Greenwich meridian and must be corrected for longitude. The longitude correction to apply is given by:

$$\frac{\text{daily change} \times \text{longitude}}{360}$$

The longitude correction may also be obtained from Table II which is directly under Table I referred to above. After correction of the LMT the longitude in time must be applied to get the UT as for the sun.

#### Procedure

1. Extract the LMT tabulated for the date in question interpolating for latitude using Table I.
2. Extract the LMT for the following day if in west longitude or the preceding day if in east longitude and find the daily change.
3. Find the longitude correction from the formula above or from Table II.
4. Apply the longitude correction to the LMT in 1 normally adding if in west longitude and subtracting in east longitude. (This applies only if the times are getting later each day as is usually the case, but if not the rules must be reversed.) The result should always lie between the values found in 1 and 2.
5. Apply longitude in time +ve for west longitude and -ve for east longitude to give the UT.

#### Example 1

Find the UT of moonrise on 9th January to an observer in position 20° 30' S 100° 00' E

LMT moonrise 9th long 0	11h 17m (interpolating for latitude
LMT moonrise 8th long 0	<u>10h 28m</u> between 20 and 30)
difference	49m

$$\text{longitude correction } \frac{(49 \times 100)}{360} \quad 14\text{m}$$

LMT moonrise 9th long 0	11h 17m
longitude correction	<u>14m</u>
LMT moonrise 9th long 100 E	11h 03m
longitude in time	<u>06h 40m</u>
UT	04h 23m 9th

#### Example 2

Find the UT of moonset on 28th June to an observer in position 33° N 170° W

LMT moonset 28th long 0	18h 25m
LMT moonset 29th long 0	<u>19h 21m</u>
difference	56m

$$\text{longitude correction } \frac{56 \times 170}{360} \quad 26\text{m}$$

LMT moonset 26th long 0	18h 25m
longitude correction	<u>26m</u>
LMT moonset 26th long 170 W	18h 51m
longitude in time	<u>11h 20m</u>
UT	30h 11m 28th
	= 06h 11m 29th

For the purpose of the amplitude problem there is no reason why the UT cannot be read from the chronometer at the moment when the body is seen to be rising or setting.

#### Procedure

1. Obtain LMT and UT of rising (or setting) from the almanac.
2. Take the declination for the time of the UT from the almanac.
3. Observe the compass bearing at the time of rising or setting.
4. Obtain the true amplitude by calculator from the formula (or from amplitude tables).
5. Convert the amplitude to a bearing and compare with the observed compass bearing.

#### Example 1

On 1st November in DR position 36° 10' N 28° 20' W at 06h 22m LMT the sun rose bearing 102° C. Find the true amplitude and the error of the compass. If the variation was 3° W find the deviation for the ship's head.

LMT sunrise 1st	06h 22m	declination 07h	14° 19.9' S
Longitude in time	<u>01h 53m</u>	d corr	<u>+0.2'</u>
UT	08h 15m	declination	14° 20.1' S

$$\begin{aligned} \text{sine amplitude} &= \sin 14^\circ 20.1' \sec 36^\circ 10' \\ \text{amplitude} &= 17.9 \end{aligned}$$





## MODULE 2.4

### Altitude and Azimuth. Correction of Altitudes

*Definitions* (see Figure 2.4.1)

*Visible Horizon.* This is the circle which bounds the observer's view of the earth's surface in a clear atmosphere. The range of the visible horizon will depend upon the observer's height of eye.

*Sensible Horizon.* This is a plane which passes through the observer's eye and is at right angles to the vertical of the observer.

*Rational Horizon.* This is the plane which passes through the centre of the earth and is at right angles to the observer's vertical and therefore parallel to the sensible horizon.

*Zenith.* The point on the celestial sphere directly above the observer.

*Nadir.* The point on the celestial sphere diametrically opposed to the zenith.

*Vertical circle.* A great circle passing through the zenith and the nadir, hence cutting the rational horizon in a right angle.

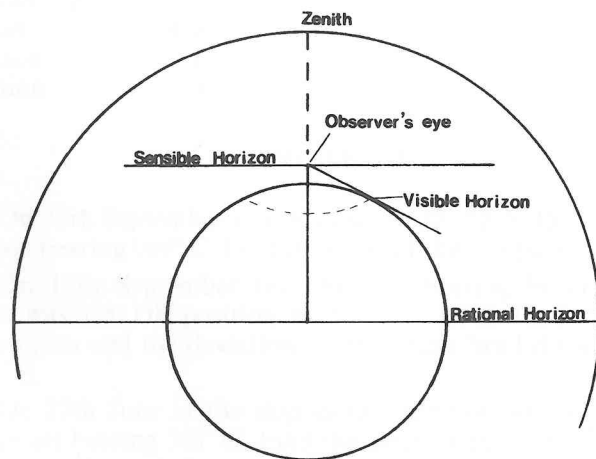


FIG. 2.4.1

The coordinates used to define a position on the celestial sphere with reference to an observer on the earth are altitude and azimuth. These can be measured by the observer, the altitude with a sextant and the azimuth with a compass.

The true altitude is defined as the angle at the centre of the earth between the plane of the rational horizon and a line joining the centre of the earth to the body. Alternatively it can be defined as the arc of a vertical circle between the body and the rational horizon. The zenith distance of the body is the arc of the vertical circle between the body and the zenith and will be equal to  $(90^\circ - \text{true altitude})$ .

The azimuth is defined as the arc of the horizon between the vertical circle through the elevated pole and the vertical circle passing through the body. Thus the terms azimuth and bearing are stating the same thing in different ways (see Module 2.3).

The true altitude (or zenith distance) and the azimuth define the position of the body unambiguously with reference to the observer. This is referred to as the Horizon system of coordinates.

#### Conversion between the horizon system and the equinoctial system

The essential element of the methods of sight reduction to find the observer's position on the earth, which will be discussed in Module 2.7, is a conversion between the horizon system coordinates of altitude and azimuth and the equinoctial system of declination and hour angle (LHA). This may be done by the solution of a spherical triangle formed by the intersection of the three great circles:

- (i) the observer's meridian
- (ii) the meridian through the body
- (iii) the vertical circle through the body.

In Figure 2.4.2 this triangle is shown as triangle PZX, P being the pole, Z the zenith of an observer in latitude  $50^\circ \text{N}$  and X, a body with northerly declination.

The sides of the triangle will be the observer's co-lat ( $90^\circ - \text{latitude}$ ), the co-dec of the body ( $90^\circ - \text{declination}$ ) and the zenith distance of the body.

The main object of celestial navigation is to find the observer's position. The side PZ would enable the latitude to be known and the angle P (LHA) would enable the longitude to be found from the GHA. However three parts of the triangle must be known for a solution and without knowing the observer's position only one

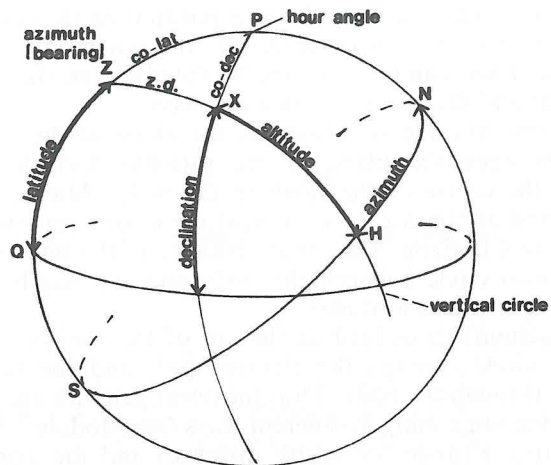


FIG. 2.4.2

part is actually known, that is the side PX or  $(90^\circ - \text{declination})$ . However the side ZX can be measured or more correctly it can be found from the true altitude. But a third part of the triangle is still required. The azimuth can be measured with a compass but alas not with sufficient accuracy to be used for this purpose. The way in which this problem is dealt with is the subject of Module 2.7. The rest of this module is concerned with the way in which the true altitude and zenith distance are obtained from the sextant observation of a bodies altitude above the visible horizon.

#### Observed altitude

If an observer measures the altitude of a heavenly body he will measure the angle at his eye between a line from the eye to the body observed, and a line from the eye to the visible horizon directly beneath the body. This is referred to as the observed altitude and will be obtained from the sextant altitude with any error of the sextant allowed for (index error).

#### Dip

This is defined as the angle at the observer's eye between the plane of the sensible horizon and a line joining the observer's eye to the visible horizon, or alternatively the depression of the visible horizon below the sensible horizon.

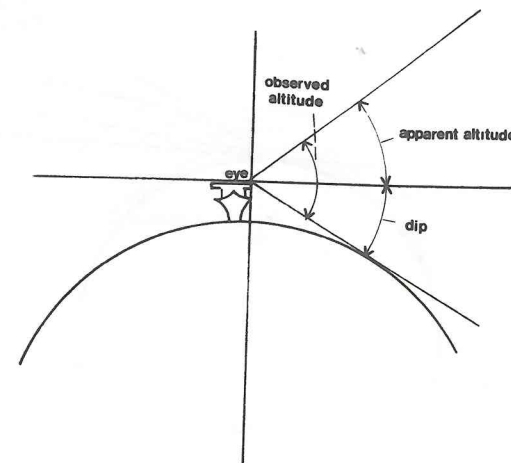


FIG. 2.4.3

The dip is subtracted from the observed altitude to give an altitude above the sensible horizon. The observed altitude corrected for dip is called the apparent altitude. This is illustrated in Figure 2.4.3.

It should be apparent from Figure 2.4.3 that:

$$\text{apparent altitude} = \text{observed altitude} - \text{dip}$$

Dip is always negative and must be applied to altitudes of all bodies. Values of dip are tabulated against height of eye in nautical tables and also in the Nautical Almanac. The table in the Nautical Almanac is usually the most convenient to use.

It should be noted that the value of the dip is affected by the amount of refraction of the observer's line of sight to his horizon. Uncertainty in the amount of refraction makes the dip correction the least accurate of all the corrections to altitude. Dip tables are based upon the formula:

$$\text{dip} = 1.77\sqrt{h} \text{ (where } h \text{ is the observer's height of eye in metres)}$$

#### Refraction

A ray of light entering a medium of greater density than that in which it has been travelling will be bent or refracted towards the



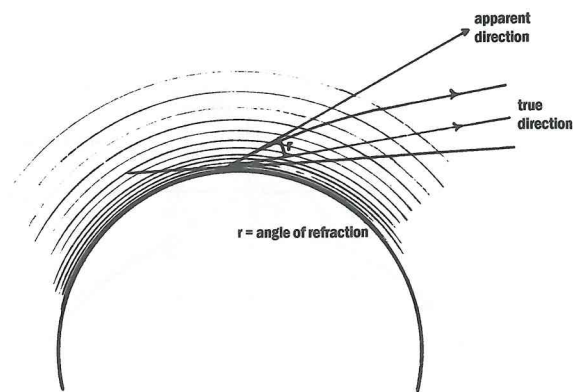


FIG. 2.4.4

normal. The normal is the perpendicular to the interface between the two mediums at the point of entry of the light.

Light entering the earth's atmosphere from the celestial body is entering a progressively more dense medium as it approaches the earth's surface. The light is therefore being continually refracted as it travels through the atmosphere. This causes the light to be coming apparently from a higher altitude than is really the case. This is shown in Figure 2.4.4. The correction for refraction is therefore negative. The refraction is greatest at low altitudes and decreases to zero when the light is entering the atmosphere at  $90^\circ$ , that is from the zenith. Uncertainty in the amount of refraction makes it inadvisable to take low altitude observations unless unavoidable.

Values for the refraction are tabulated against altitude in nautical tables. The correction is applied to the altitude of all bodies.

### Semi Diameter

In the case of the sun and moon it is easier and more accurate to observe the altitude of the upper or lower edge or limb of the body than to observe the estimated centre of the body. A correction for the radius of the visible disc must therefore be applied to obtain the altitude of the centre of the body. This correction is called the semi diameter. The value will be the angle at the observer's eye subtended by the radius of the body. From Figure 2.4.5 it can be seen that the correction will be positive if the lower limb is observed and negative if the upper limb is observed.

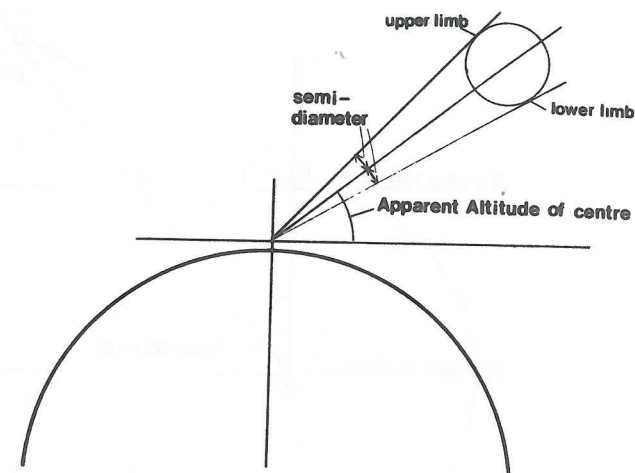


FIG. 2.4.5

Semi diameter varies as the distance of the body from the earth and therefore will change due to the elliptical orbits of the earth around the sun and the moon around the earth. Values are given in the daily pages of the Nautical Almanac at the foot of the appropriate columns. One value is given for the sun for the three days on the page, but three values are given for the moon. The values are in minutes of arc.

There is no semi diameter correction for stars or planets.

### Parallax

This is defined as the angle at the centre of the body subtended by a line from the centre of the earth and a line to the observer's eye. The parallax is maximum when the body is on the sensible horizon and then is called the **Horizontal Parallax**.

The application of the parallax corrects the altitude from that which is observed at the observer's position to that which would be observed at the centre of the earth, that is the true altitude.

In Figure 2.4.6

angle CSO is the angle of parallax,  
 angle AOS is the apparent altitude uncorrected for parallax,  
 angle ACH is the altitude after correction for parallax, that is the true altitude.

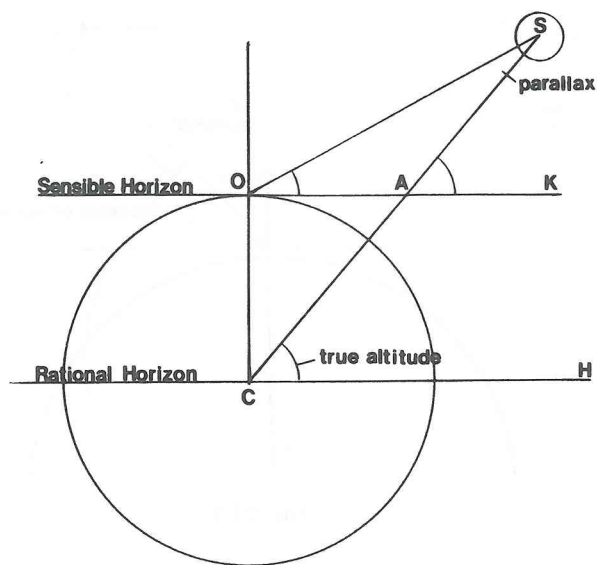


FIG. 2.4.6

Thus angle  $ACH = \text{angle } SAK$   
 and angle  $SAK = \text{angle } CSO + \text{angle } AOS$  (exterior angle of a triangle is equal to the two interior and opposite angles).  
 Thus true altitude = apparent altitude + parallax.

The parallax correction is always positive to the apparent altitude and its value will vary with the altitude, being maximum when the body is in the horizon and zero when the body is in the zenith.

Values for the sun are tabulated against altitude in nautical tables. Parallax must be applied to altitudes of the sun and moon, although the moon's parallax requires a further correction (see correction of the moon's altitude). There is no parallax correction necessary for stars due to their great distance. Planets parallax may sometimes be negligible but sometimes be considerable, sometimes greater than the sun. A planet's minimum parallax value will occur at conjunction (superior conjunction for an inferior planet). The maximum value will occur at opposition for a superior planet and inferior conjunction for an inferior planet. The parallax correction for a planet is conveniently ignored when correcting

altitudes by individual corrections, but it is allowed for in total correction tables which will be introduced at the end of this module.

### Correction of the Moon's Altitude

Due to the proximity of the moon to the earth there are two additional corrections to the moon's altitude which are negligible for other bodies and are therefore ignored.

### Reduction to the moon's horizontal parallax for latitude

The horizontal parallax for the moon is given in the daily pages for each hourly entry in the column headed H.P.

This is in fact the moon's equatorial horizontal parallax, that is the angle at the moon's centre subtended by the earth's equatorial radius. The oblate shape of the earth however means that the lesser polar radius will subtend a smaller angle. Thus the parallax must be reduced for latitude. This is shown in Figure 2.4.7.

The value of the 'Reduction to the Moon's Equatorial Horizontal Parallax for Latitude' is tabulated in nautical tables against latitude. The parallax in altitude can then be found by:

$$\text{Parallax in altitude} = \text{horizontal parallax} \times \cos \text{altitude.}$$

The parallax in altitude is then added to the apparent altitude as for the sun.

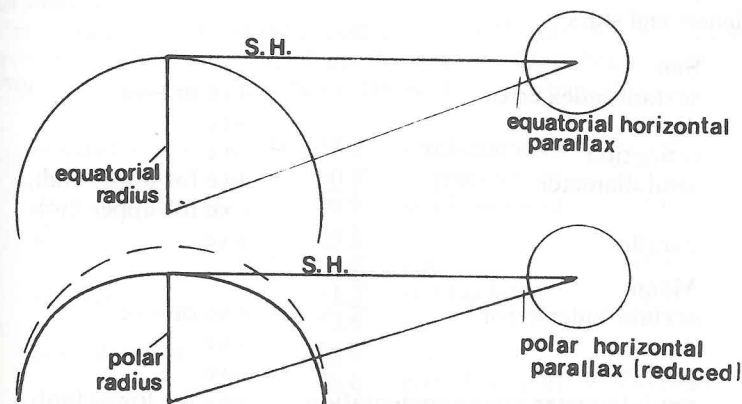


FIG. 2.4.7



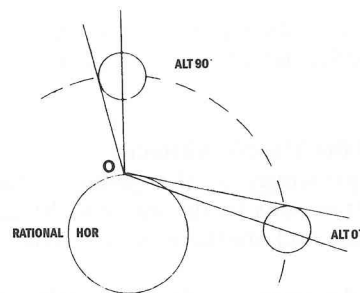


FIG. 2.4.8

### Augmentation of the moon's semi diameter

The only variable which determines the semi diameter of any given body is its distance from the observer. A body will be closest to the observer when it is at his zenith, that is with altitude  $90^\circ$ . The distance and therefore the semi diameter decreases as the altitude decreases as illustrated in Figure 2.4.8. In the case of the sun the earth's radius is extremely small compared to the distance of the sun and therefore has a negligible effect. This is not so in the case of the moon. The values for semi diameter of the moon which are given in the almanac are for when the body is on the rational horizon, that is with altitude  $0^\circ$ . The Augmentation of the Moon's Semi-diameter is a positive correction to these values. The augmentation is tabulated in nautical tables against altitude.

### To summarize the corrections required for the sun, the moon, the planets and stars

<b>Sun</b>	
sextant index error	+ve or -ve
dip	-ve
refraction	-ve
semi diameter	+ve for lower limb, -ve for upper limb
parallax	+ve
<b>Moon</b>	
sextant index error	+ve or -ve
dip	-ve
refraction	-ve
semi-diameter after augmentation	+ve for lower limb, -ve for upper limb

parallax after reduction of the h.p.  
for latitude +ve

### Stars and Planets

sextant index error +ve or -ve  
dip -ve  
refraction -ve

### Example 1

If the sextant altitude of the sun's lower limb was  $45^\circ 20'$ , sextant index error  $1.2'$  on the arc, height of eye 15.4 metres and date 5th January, find the true altitude.

sext. alt.	$45^\circ 20.0'$	
i.e.	$\underline{-1.2'}$	
obs. alt.	$45^\circ 18.8'$	
dip	$\underline{-6.9'}$	from table in almanac
app. alt.	$45^\circ 11.9'$	
refr.	$\underline{-0.9'}$	from table in Norie's Tables
	$45^\circ 11.0'$	
semi diam.	$\underline{+16.3'}$	from almanac for 5th Jan.
	$45^\circ 27.3'$	
parallax	$\underline{+0.1'}$	from table in Norie's Tables
true alt.	$45^\circ 27.4'$	

### Example 2

The sextant altitude of the moon's lower limb was  $36^\circ 58.2'$ . Index error  $0.8'$  off the arc. ht. of eye 5.4 metres. Date 8th January at 1200. DR position  $32^\circ 50' N 34^\circ 00' W$ . Find the true altitude.

sextant altitude	$36^\circ 58.2'$	semi-diameter	$14.9'$
index error	$\underline{+0.8'}$	augmentation	$\underline{0.1'}$
observed altitude	$36^\circ 59.0'$	semi diameter	$15.0'$
dip	$\underline{-4.1'}$		
	$36^\circ 54.9'$	equ. h.p.	$54.8'$
refraction	$\underline{-1.3'}$	red for lat.	$\underline{0.1'}$
	$36^\circ 53.6'$	h.p.	$54.7'$
semi diameter	$\underline{+15.0'}$		
	$37^\circ 08.6'$	parallax in alt. $54.7' \cos \text{alt.}$	
parallax in alt.	$\underline{+43.7'}$		$= 43.7'$
true altitude	$37^\circ 52.3'$		

**Example 3**

Find the true altitude of the star Rigel if the sextant altitude is  $29^{\circ} 17.2'$ , the index error  $1.8'$  off the arc, and the height of eye 14 metres.

sextant alt.	$29^{\circ} 17.2'$
index error	$+1.8'$
observed alt.	$29^{\circ} 19.0'$
dip	$-6.6'$
	$29^{\circ} 12.4'$
refr.	$-1.7'$
true altitude	$29^{\circ} 10.7'$

**EXERCISE 2.4.1**

Find the true altitude in the following cases using individual corrections. Answers given are worked using Burton's nautical tables.

Body	Sext. alt.	I.E.	Ht. eye	Date
1. Sun LL	$52^{\circ} 31.2'$	2.2' on the arc	8.3m	4th Jan.
2. Sun LL	$33^{\circ} 10.8'$	1.0' off the arc	12.0m	27th June
3. Sun UL	$71^{\circ} 53.5'$	1.8' off the arc	11.0m	20th Sept.
4. Sun UL	$27^{\circ} 46.7'$	nil	7.7m	30th Sept.
5. Sun LL	$62^{\circ} 34.3'$	2.2' off the arc	9.0m	18th Dec.
6. Sun UL	$55^{\circ} 55.8'$	1.0' on the arc	7.4m	28th June

**EXERCISE 2.4.2**

Find the true altitude in the following cases using individual corrections.

Body	Sext. alt.	I.E.	Ht. eye
1. Altair	$47^{\circ} 29.6'$	1.0' on the arc	11.2m
2. Canopus	$32^{\circ} 24.2'$	0.8' on the arc	7.3m
3. Arcturus	$21^{\circ} 13.6'$	0.4' off the arc	11.6m
4. Polaris	$47^{\circ} 15.8'$	1.4' on the arc	15.3m
5. Dubhe	$37^{\circ} 10.4'$	1.8' on the arc	8.4m

6. Saturn	$12^{\circ} 17.0'$	2.0' off the arc	14.0m
7. Venus	$53^{\circ} 20.2'$	0.6' on the arc	7.7m
8. Jupiter	$23^{\circ} 14.0'$	2.2' off the arc	11.0m
9. Mars	$51^{\circ} 56.0'$	0.4' on the arc	17.0m
10. Venus	$14^{\circ} 38.2'$	2.8' on the arc	9.9m

**EXERCISE 2.4.3**

Find the true altitude in the following cases using individual corrections.

Body	Sext. alt.	I.E.	Ht. eye (m)	Date (UT)	Latitude
1. Moon LL	$63^{\circ} 12.8'$	1.6' off the arc	7.3	2200 18th Dec.	$44^{\circ} 56.3' N$
2. Moon LL	$34^{\circ} 14.8'$	2.2' on the arc	13.0	0800 30th Sept.	$34^{\circ} 23.0' S$
3. Moon UL	$58^{\circ} 16.2'$	1.0' on the arc	10.4	1900 19th Sept.	$50^{\circ} 00' N$
4. Moon UL	$77^{\circ} 51.6'$	1.2' off the arc	14.8	1500 27th June	$56^{\circ} 30' N$
5. Moon LL	$21^{\circ} 38.8'$	3.4' on the arc	11.5	0200 9th Jan.	$23^{\circ} 00' S$
6. Moon LL	$38^{\circ} 21.8'$	2.4' off the arc	9.0	1600 28th June	$34^{\circ} 30' N$
7. Moon UL	$51^{\circ} 17.0'$	1.6' on the arc	16.0	1200 19th Sept.	$40^{\circ} 00' N$
8. Moon LL	$43^{\circ} 18.4'$	nil	13.7	0300 2nd Nov.	$2^{\circ} 00' S$

**Total Correction Tables**

In practice correction of altitude is simplified by the use of total correction tables, which combine individual corrections. Nautical tables contain their own versions of total correction tables but the most commonly used, and described here, are the convenient tables included in the Nautical Almanac. These are in three tables, one for the sun, one for the moon, and one for the stars and planets. Each table is compiled with the apparent altitude as the argument so that the dip correction must be first applied to the observed altitude. A dip table is included.

The dip table is tabulated against height of eye and is based upon the formula:

$$1.76\sqrt{\text{ht of eye in metres}}$$

The table is arranged as a critical entry table which means that one value of the correction is given for an interval of the argument. This means that no interpolation is required and it



should be remembered that if the height of eye is a tabulated value the upper of the two figures should be extracted. Thus a height of 13.0 metres gives a dip correction of  $-6.3'$  (see extracts from Nautical Almanac).

#### Sun's total correction table

The sun's correction table found on the first page of the almanac, corrects for mean refraction, semi diameter and parallax. The argument is the apparent altitude, that is the observed altitude corrected for dip. Two separate tables are used, one for the months April to September and one for the months October to March. This allows for annual variations in the semi-diameter to be allowed for. Each table contains corrections for the lower limb in bold type and corrections for the upper limb observations in feint type. The tables are arranged as critical entry tables as described for the dip table. For example an argument of  $51^{\circ} 08'$  for the apparent altitude will give a correction of  $+15.5'$  for the lower limb in the October to March table, while a value of  $50^{\circ} 46'$  will give a correction of  $+15.4'$ .

#### Example

The sextant altitude of the sun's lower limb was  $48^{\circ} 56.3'$ . Index error  $1.2'$  on the arc. Height of eye 7.2 metres. Date 16th June. Find the true altitude.

sextant altitude	$48^{\circ} 56.3'$
index error	$\underline{-1.2'}$
observed altitude	$48^{\circ} 55.1'$
dip	$\underline{-4.7'}$
apparent altitude	$48^{\circ} 50.4'$
total correction	$\underline{+15.1'}$
true altitude	$49^{\circ} 05.5'$

#### Stars and planets

The correction table for stars and planets found on the first page of the almanac, corrects for the refraction only. Again it is arranged as a critical entry table with the argument apparent altitude, that is observed altitude corrected for the dip.

Additional corrections for planets are given for some dates and for some apparent altitudes. These correct for parallax when its value cannot be considered negligible.

#### Example

The sextant altitude of the star Procyon was  $57^{\circ} 18.9'$ . Index error  $1.0'$  off the arc. Height of eye 6.5 metres. Find the true altitude.

sextant altitude	$57^{\circ} 18.9'$
index error	$\underline{+1.0'}$
observed altitude	$57^{\circ} 19.9'$
dip	$\underline{-4.5'}$
apparent altitude	$57^{\circ} 15.4'$
total correction	$\underline{-0.6'}$
true altitude	$57^{\circ} 14.8'$

#### Example

The sextant altitude of the Venus on 1st December was  $38^{\circ} 06.5'$ . Index error  $0.5'$  off the arc. Height of eye 5.0 metres. Find the true altitude.

sextant altitude	$38^{\circ} 06.5'$
index error	$\underline{+0.5'}$
observed altitude	$38^{\circ} 07.0'$
dip	$\underline{-3.9'}$
apparent altitude	$38^{\circ} 03.1'$
total correction	$\underline{-1.2'}$
	$38^{\circ} 01.9'$
additional correction	$\underline{+0.3'}$
true altitude	$38^{\circ} 02.2'$

#### Moon's total correction table

The moon's total correction table is found on the last pages of the almanac and is in two parts. The main correction in the upper part of the table corrects for refraction, semi diameter and parallax, using mean values. It is tabulated against apparent altitude and some interpolation is required to obtain the accuracy to within one decimal place.

The second correction allows for variations in the semi diameter and parallax, both of which depend upon the horizontal parallax. The arguments are therefore apparent altitude and horizontal parallax. Two values are given one for lower limb and one for upper limb observations. They are arranged in columns the correction being taken from the same column as that from which the main correction was taken, and against the H.P.

All corrections for the moon are additive to the apparent altitude but those for the upper limb observations have had 30' added to them to maintain them positive. This 30' must therefore be subtracted from the final result.

**Example**

The sextant altitude of the moon's lower limb was  $16^{\circ} 58.2'$ . Index error  $10.8'$  off the arc. Height of eye 5.4 metres. GMT 1400 on 27th June. Find the true altitude.

from the almanac H.P.	54.5'
sextant altitude	$16^{\circ} 58.2'$
index error	<u>+0.8'</u>
observed altitude	$16^{\circ} 59.0'$
dip	<u>-4.1'</u>
apparent altitude	$16^{\circ} 54.9'$
main correction	<u>+62.7'</u>
second correction	<u>+1.1'</u>
true altitude	$17^{\circ} 58.7'$

Exercises 4, 5 and 6 are the same as exercises 1, 2 and 3 but to be worked with total correction tables. Answers given have been found using the correction tables in the almanac. Small variations may be found between solutions using individual corrections and total corrections.

**EXERCISE 2.4.4**

Find the true altitude in the following cases using total corrections.

Body	Sext. alt.	I.E.	Ht. eye	Date
1. Sun LL	$52^{\circ} 31.2'$	2.2' on the arc	8.3m	4th Jan.
2. Sun LL	$33^{\circ} 10.8'$	1.0' off the arc	12.0m	27th June
3. Sun UL	$71^{\circ} 53.5'$	1.8' off the arc	11.0m	20th Sept.
4. Sun UL	$27^{\circ} 46.7'$	nil	7.7m	30th Sept.
5. Sun LL	$62^{\circ} 34.3'$	2.2' off the arc	9.0m	18th Dec.
6. Sun UL	$55^{\circ} 55.8'$	1.0' on the arc	7.4m	28th June

**EXERCISE 2.4.5**

Find the true altitude in the following cases using total corrections.

Body	Sext. alt.	I.E.	Ht. eye
1. Altair	$47^{\circ} 29.6'$	1.0' on the arc	11.2m
2. Canopus	$32^{\circ} 24.2'$	0.8' on the arc	7.3m
3. Arcturus	$21^{\circ} 13.6'$	0.4' off the arc	11.6m
4. Polaris	$47^{\circ} 15.8'$	1.4' on the arc	15.3m
5. Dubhe	$37^{\circ} 10.4'$	1.8' on the arc	8.4m
6. Saturn	$12^{\circ} 17.0'$	2.0' off the arc	14.0m
7. Venus	$53^{\circ} 20.2'$	0.6' on the arc	7.7m
8. Jupiter	$23^{\circ} 14.0'$	2.2' off the arc	11.0m
9. Mars	$51^{\circ} 56.0'$	0.4' on the arc	17.0m
10. Venus	$14^{\circ} 38.2'$	2.8' on the arc	9.9m

**EXERCISE 2.4.6**

Find the true altitude in the following cases using total corrections.

Body	Sext. alt.	I.E.	Ht. eye (m)	Date (UT)
1. Moon LL	$63^{\circ} 12.8'$	1.6' off the arc	7.3	2200 18th Dec.
2. Moon LL	$34^{\circ} 14.8'$	2.2' on the arc	13.0	0800 30th Sept.
3. Moon UL	$58^{\circ} 16.2'$	1.0' on the arc	10.4	1900 19th Sept.
4. Moon UL	$77^{\circ} 51.6'$	1.2' off the arc	14.8	1500 27th June
5. Moon LL	$21^{\circ} 38.8'$	3.4' on the arc	11.5	0200 9th Jan.
6. Moon LL	$38^{\circ} 21.8'$	2.4' off the arc	9.0	1600 28th June
7. Moon UL	$51^{\circ} 17.0'$	1.6' on the arc	16.0	1200 19th Sept.
8. Moon LL	$43^{\circ} 18.4'$	nil	13.7	0300 2nd Nov.



## MODULE 2.5

## Position Lines and Position Circles

One timed observation of the altitude of a heavenly body will give a position circle. There will be many positions from which the same altitude would be observed at any one time. If all these positions were joined they would form a circle on the earth's surface and this circle could be drawn around the geographical position of the body as shown in Figure 2.5.1. The radius of the circle as measured as an arc along the earth's surface is the zenith distance ( $90^\circ - \text{true altitude}$ ). To obtain a position we will need at least two observations of two different bodies so that the two position circles intersect to define the observer's position.

It is not practical to simply draw the circle or circles on a chart. The scale of the chart would have to be far too small, and such large circles would be distorted by the projection of the chart.

If one position circle is considered then although we do not know at which point on the circle the ship lies, we can say fairly confidently that it will be reasonably close to the DR position. Furthermore the area over which the ship is likely to be should be small compared to the radius of the circle (as long as the body observed is not too close to the zenith), and over this small area the curve of the position circle can be represented by a straight line without too much error. The problem becomes to find a position

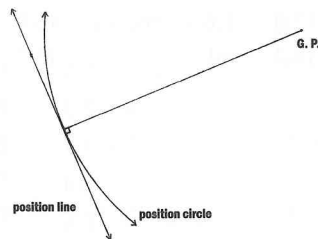


FIG. 2.5.1

through which the position line passes and the direction in which it runs at that position, so that it can be drawn on a navigator's chart and used as a position line. The direction of the position line will be perpendicular to the bearing of the body at the time of the observation which can be found as described in Module 2.3. The position through which it passes near to the DR position requires some calculation and there are various methods of obtaining this. The calculations will be dealt with in Module 2.7. Here we will concern ourselves only with the manipulation of the position lines.

**The Intercept Method (Marcq St. Hilaire Method)**

It may be said that the intercept method is the only method which the navigator needs to know as any observation may be worked by this method. The only case when it would not be used is the case when the body is bearing due north or due south when the calculations can be made much shorter and easier. This case will be dealt with in Module 2.6.

A position is assumed, probably the DR position but not necessarily so as long as it is reasonably close to the true position. Calculations are then made to find the zenith distance that would have been observed from that position. The bearing of the body is also calculated. If the ship was actually in the assumed position the position line could be drawn through it in a direction at right angles to the bearing. However by taking the real or true zenith distance from the observation, it will be seen whether the ship lies closer to or further away from the geographical position than the assumed position. If the true zenith distance is greater than the calculated zenith distance then the ship must be further from the geographical position than was assumed. If the true zenith distance is less than the calculated zenith distance then the ship must lie towards the geographical position from the assumed position. The difference between the true and calculated zenith distances is called the intercept and it is named either away or towards depending on the foregoing considerations.

The true position should be close enough to the assumed position that the true bearing may be taken to be the same as the calculated bearing. The calculated and the true position lines should therefore be parallel.

In practice only the true position line need be drawn. This is done by plotting the assumed position and drawing the intercept either towards or away from the body in the direction or

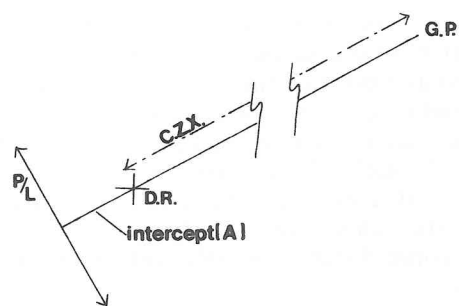


FIG. 2.5.2

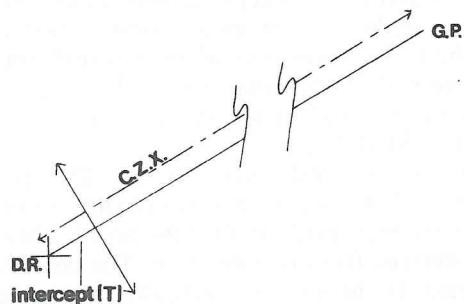


FIG. 2.5.3

reciprocal of the bearing, marking off the intercept along this line, and drawing the true position at right angles at this intercept terminal position. (ITP). Figure 2.5.2 shows a DR or assumed position with the GP. The distance between them will be the calculated zenith distance (CZX). The intercept is away (TZX greater than CZX). Similarly Figure 2.5.3 shows the intercept towards (TZX less than CZX).

It is necessary to plot only the intercept and true position line so that the plot for one observation may look like Figure 2.5.4.

If two such position lines are plotted to scale on a plotting sheet, the intersection of the two position lines can be taken to be the observed position and the latitude and longitude obtained by measuring its d'lat and d'long from the assumed position. It is sensible to use the same assumed position when calculating the two (or more) position lines.

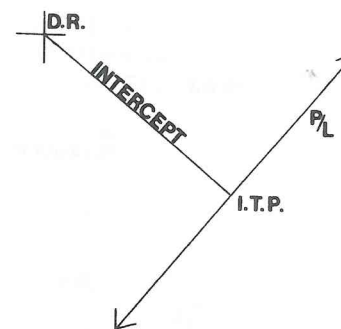


FIG. 2.5.4

### To find the position by plotting the position lines of two simultaneous sights

#### Procedure

1. On a plotting sheet or graph paper plot a convenient point to represent the assumed position.
2. From this point draw the intercepts in the direction (if named towards), or in the opposite direction (if named away) of the respective bearings.
3. Mark off along these lines the lengths of the intercepts.
4. Through the intercept terminal positions draw the position lines at right angles to the intercepts, and mark with a small circle where the two position lines cross.
5. Measure the d'lat and the departure between the assumed position and the plotted observed position.
6. Convert departure to d'long and apply d'lat and d'long to the assumed position to obtain the observed position.

#### Example 1

Two simultaneous observations, when worked using an assumed position of  $52^{\circ} 15' N 40^{\circ} 30' W$  gave the following results:

- Observation 1; intercept  $5.5'$  away, bearing  $175^{\circ} T$ .  
 Observation 2; intercept  $4.2'$  towards, bearing  $250^{\circ} T$ .

Find the ship's observed position.  
 By measurement from Figure 2.5.5



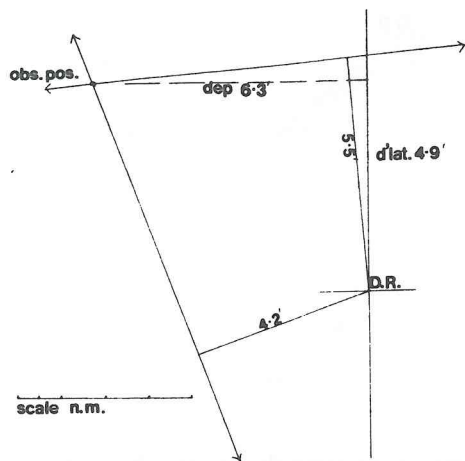


FIG. 2.5.5

d'lat = 4.9' N  
 dep = 6.3' W  
 d'long = 6.3 sec 52° 15'  
 = 10.3' W

assumed position	d'lat	52° 15.0' N	d'long	40° 30.0' W
		4.9' N		10.3' W
observed position		52° 19.9' N		40° 40.3' W

In practice it is usual to observe if possible at least three bodies. More if available can be used as checks. This is the practice when taking star sights at morning and evening twilight. However it is rarely possible during daylight when the sun, sometimes the moon, and occasionally a planet are the only available bodies. In these circumstances transferred position lines are used to obtain positions.

**Transferring the position line**

During daylight hours if there is only one body available for observation, usually the sun, a position may be obtained by using a position line from one observation and transferring it to a later time by applying a course and distance run. At this later time the sun will have changed its bearing and another position line can be obtained to cross with the transferred or 'run up' position line. The transferred position line is marked by double arrows at each end. The run up position can be used as the assumed position for the second

observation so that the two position lines can be plotted from the same position. The running up of the first position is done by calculation so that it is not necessary to plot the run.

**Example 2**

From an observation of a body bearing 132° T an intercept of 6.2' towards is obtained, using an assumed position of 25° 18' S 38° 20' E. The ship then steamed 245° T for 45 miles when a second observation gave an intercept of 5.0' towards bearing 205° T. The DR position obtained by running up the first assumed position by plane sailing was used to calculate the second intercept. Find the ship's position at the time of the second observation.

Run 245 by 45 miles

d'lat made good 45 cos 245° = 19.0' S  
 departure made good 45 sin 245° = 40.8' W

difference of longitude 40.8 sec 25° 28' = 45.2' W

assumed position	25° 18.0' S	38° 20.0' E
d'lat	19.0' S	45.2' W
DR position	25° 37.0' S	37° 34.8' E (Used as the assumed position for the second observation)

From Figure 2.5.6

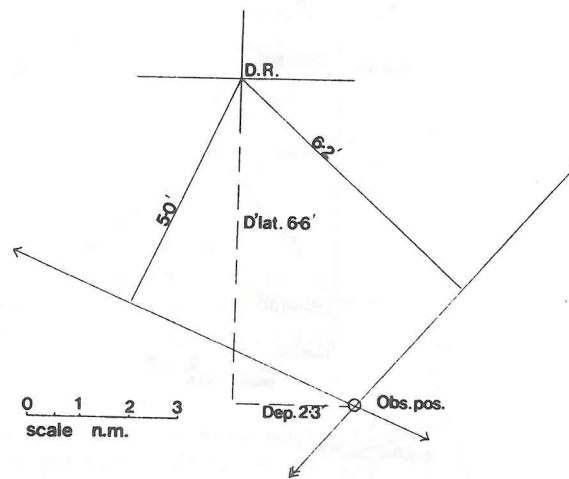


FIG. 2.5.6

between the observed position and the DR

d'lat = 6.6' S	departure = 2.3' E	d'long = 2.3 sec 25° 37' = 2.6' E
DR position	25° 37.0' S	37° 34.8' E
d'lat	<u>6.6' S</u>	d'long <u>2.6' E</u>
observed pos.	25° 43.6' S	37° 37.4' E

**Example 3**

From an assumed position 32° 48' S 15° 35' W a body bearing 220° T was observed and an intercept of 4.8' away was calculated. The ship then steamed 335° T for 68 miles. A second observation then gave an intercept of 2.0' towards bearing 290° T using an assumed position of 31° 50' S 16° 10' W. Find the ship's position at the time of the second observation.

course = 335	d'lat = 61.6' N	departure = 28.7' W
		d'long = 28.7 sec 32° 18' = 33.9' W

first assumed position	32° 48.0' S	15° 35.0' W
d'lat	<u>1° 1.6' N</u>	d'long <u>33.9' W</u>
DR position	31° 46.4' S	16° 08.9' W
second assumed position	31° 50.0' S	<u>16° 10.0' W</u>
d'lat	<u>3.6' S</u>	d'long <u>1.1' W</u>
		dep = 1.1 cos 31° 50' = 0.9' W

From Figure 2.5.7

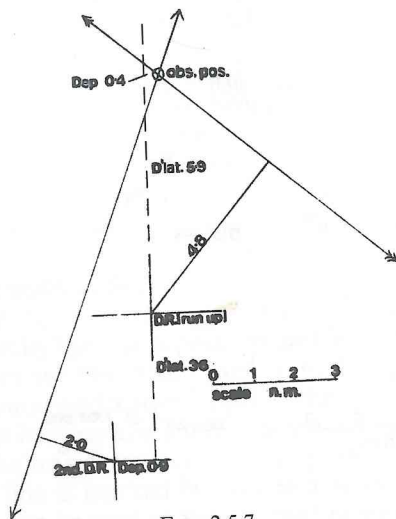


FIG. 2.5.7

between observed position and DR (run up) position:

d'lat = 5.9' N	departure = 0.4' E	d'long = 0.4 sec 31° 46' = 0.5'
Run up position	31° 46.4' S	16° 08.9' W
d'lat	<u>5.9' N</u>	d'long <u>0.5' E</u>
observed position	31° 40.5' S	16° 08.4' W

It is common practice at sea to obtain a position line during the forenoon when the sun is bearing near to east and then run this position line up to the time of noon. The transferred position line would then be crossed with a latitude by meridian altitude (see Module 2.6). At this time the sun is bearing south or north and the position line runs east-west along a parallel of latitude. The full calculations for this problem are given in Module 2.7.

**Longitude by chronometer method**

It has been said that the intercept method can be used for all observations out of the meridian. The alternative longitude by chronometer method of reducing a sight has been popular in the past because the problem of finding a noon position by a forenoon observation of the sun combined with a meridian altitude can be done without any plotting with slightly less work than by the intercept method. It should be noted however that the method is not suitable for bodies which are close to the meridian when the bearing is close to north or south.

An assumed latitude is used, and the longitude in which the position line cuts that parallel is calculated (see Module 2.7). This is a position through which the position line passes albeit a different position from the intercept terminal position which is obtained by the intercept method. The bearing is calculated to give the direction of the position line at right angles to it. The plotting of the position line only requires the assumed latitude and the calculated longitude to be plotted and the position line drawn through it. If two observations are obtained simultaneously it makes sense to use the same latitude for both calculations, but clearly two different longitudes will be calculated.

**Procedure**

1. Plot the two positions through which the position lines pass. These two positions will be on the same parallel as long as the same latitude has been used for both calculations but a different longitude will result from each calculation. The departure will



have to be obtained between the two longitudes so that they are plotted in the correct position relative to each other.

2. Draw the two positions through their respective positions in the appropriate directions.

3. Measure the d'lat and the departure between the observed position where the position lines cross and one of the other positions to obtain the latitude and longitude of the observed position.

**Example 4**

By using an assumed latitude of 49° 00' N simultaneous observations of two stars gave longitudes of 9° 46.5' W and 9° 52.4' W bearing 135° T and 215° T respectively. Find the ship's position.

d'long between the two longitudes = 5.9' departure = 5.9 cos 49° 00' = 3.9'

From Figure 2.5.8

d'lat between observed position and position 49° 00' N 9° 52.4' W = 1.6' S

departure = 2.3' E

d'long = 2.3 sec 49° = 3.5' E

position	49° 00.0' N	d'long	9° 52.4' W
d'lat	<u>1.6' S</u>	d'long	<u>3.5' E</u>
observed pos.	48° 58.4' N		9° 48.9' W

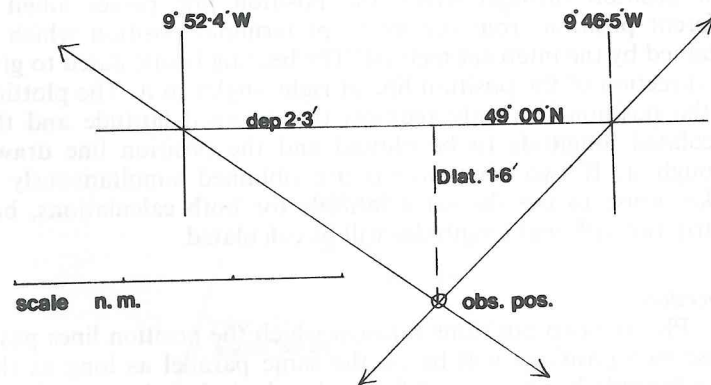


FIG. 2.5.8

**Example 5**

An observation of a body bearing 100° T when worked by longitude by chronometer gave a longitude of 179° 45' E when using an assumed latitude of 10° 07' N. The ship then steamed 095° T for 38 miles and a second observation of a body bearing 152° T gave an intercept of 4.8' towards. The position assumed for the second observation was obtained by running up the first assumed latitude and calculated longitude by plane sailing. Find the ship's position at the time of the second observation.

Run 095° T by 38 miles

d'lat 3.3' S departure 37.9' E d'long 38.5' E

first assumed latitude	10° 07.0' N	calculated longitude	179° 45.0' E
d'lat	<u>3.3' S</u>	d'long	<u>38.5' E</u>
DR position	10° 03.7' N		<u>180° 23.5' E</u>
			= 179° 36.5' W

From Figure 2.5.9

between observed position and position 10° 03.7' N 179° 36.5' W and the observed position:

d'lat = 6.0' S

departure = 1.1' W

d'long = 1.1 sec 10 = 1.1' W

DR position	10° 03.7' N	d'long	179° 36.5' W
d'lat	<u>6.0' S</u>	d'long	<u>1.1' W</u>
observed position	9° 57.7' N		<u>179° 37.6' W</u>

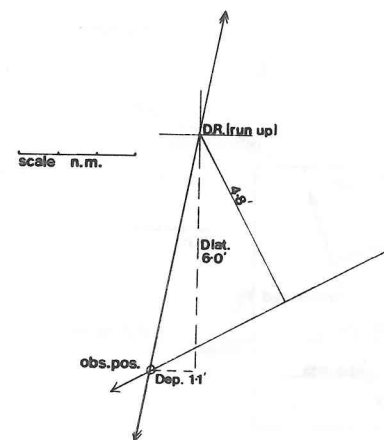


FIG. 2.5.9

**Latitude by Meridian Altitude method**

The meridian altitude is the altitude of the body when it is on the observer's meridian and bearing either north or south. The position line will therefore run east and west and can represent the parallel of latitude of the observer. The calculations involved to find the latitude are very quick and easy and invariably at sea the noon latitude will be obtained from the sun's meridian passage. This position line is then crossed with a transferred position line run up from an earlier sight of the sun when it was bearing to the east.

**Example 7**

An observation of the sun bearing 110° T during the forenoon gave an intercept of 5.5' towards using an assumed position of 40° 15' N 36° 40' W. The ship then steamed 250° T for 20 miles when the latitude by meridian altitude of the sun was found to be 40° 01.5' N. Find the ship's position at noon.

A plot of the complete problem would appear as in Figure 2.5.10. However the course and distance run is calculated and only that part of the figure inside the dotted lines would be plotted and will appear as in Figure 2.5.11.

**Procedure**

1. Calculate and apply the course and distance run to the assumed position used for the forenoon sight to obtain a DR for noon.

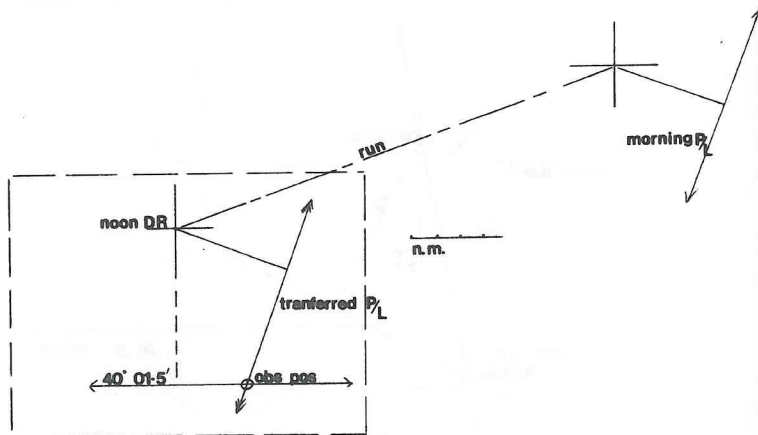


FIG. 2.5.10

2. When the latitude by meridian altitude is obtained plot the noon DR position and lay off the transferred intercept and position line from the morning observation.

3. Take the d'lat between the DR latitude and the observed latitude and plot the noon position line in the east/west direction. The observed position is where the transferred position line cuts the noon latitude.

4. Measure the departure between the DR and the observed position, convert to d'long to give the noon longitude.

forenoon assumed position	40° 15.0' N	36° 40.0' W
250° by 20 miles	<u>6.8' S</u>	<u>24.6' W</u>
noon DR position	40° 08.2' N	37° 04.6' W

From Figure 2.5.8

between the observed position and noon DR  
 departure = 3.4' E  
 d'long = 3.4 sec 40° = 4.4' E

noon DR longitude	37° 04.6' W
d'long	<u>4.4' E</u>
noon longitude	37° 00.2' W

noon position 40° 01.5' N 37° 00.2' W

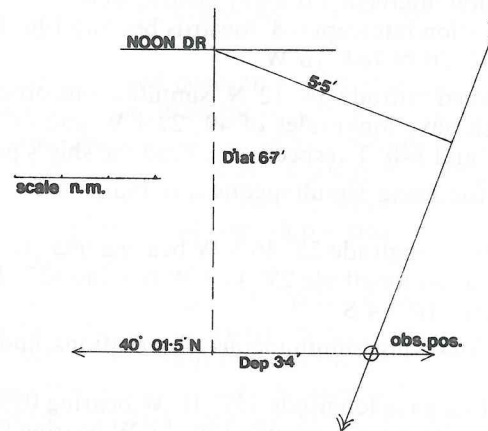


FIG. 2.5.11



Note: If this problem is done using the longitude by chronometer method for the forenoon sight then the necessity for this type of plot at noon is removed as there is a simple solution to find the longitude using the value 'C' from the computation of the bearing (see Module 2.6).

## EXERCISE 2.5.1

1. From the following simultaneous observations find the observed position.

First observation intercept 6.0' away bearing 050° T.  
Second observation intercept 2.0' towards bearing 290° T.  
DR position 47° 00' N 6° 40' W.

2. Using assumed position 36° 05' S 122° 15' E, simultaneous observations were made which gave intercepts of 9.5' away and 4.3' towards bearing 342° T and 035° T respectively. Find the ship's position.

3. From the following simultaneous observations find the observed position.

First observation intercept 2.5' towards bearing 175° T.  
Second observation intercept 2.5' towards bearing 270° T.  
DR position 9° 30' N 177° 50' E.

4. From the following simultaneous observations find the observed position.

First observation intercept 1.0' away bearing 080° T.  
Second observation intercept 6.8' towards bearing 140° T.  
DR position 52° 20' N 164° 16' W.

5. Using assumed latitude 34° 12' N, simultaneous observations were made which gave longitudes of 40° 27.4' W and 40° 31.9' W bearing 255.5° T and 140° T respectively. Find the ship's position.

6. From the following simultaneous observations find the observed position.

First observation longitude 25° 46.3' W bearing 093° T.  
Second observation longitude 25° 44.7' W bearing 327° T.  
DR latitude used 10° 14' S.

7. From the following simultaneous observations find the observed position.

First observation gave longitude 159° 18' W bearing 095° T.  
Second observation gave longitude 159° 12' W bearing 050° T.  
DR latitude used 15° 20' S.

8. From the following simultaneous observations find the observed position.

First observation gave longitude 146° 59' E bearing 310° T.  
Second observation gave longitude 147° 10' E bearing 260° T.  
DR latitude used 36° 40' N.

9. From assumed position 23° 40' N 52° 30' W a stellar observation gave an intercept of 4.0' towards bearing 040° T. The ship then steamed 090° T for 24 miles through a current setting 000° T. Drift experienced was 5 miles. A second observation then gave an intercept of 5.0' towards bearing 120° T when using an assumed position obtained by applying the run and the current to the first assumed position. Find the ship's position at the time of the second observation.

10. From assumed position 6° 18' S 42° 19' W an observation of the sun gave an intercept of 5.6' away bearing 130° T. The ship then steamed 145° T for 53 miles. A second observation of the moon then gave an intercept of 1.6' towards bearing 200° T when using an assumed position obtained by applying the run to the first assumed position. Find the ship's position at the time of the second observation.

11. From assumed position 41° 10' S 114° 00' E an observation of venus gave an intercept of 1.0' away bearing 100° T. The ship then steamed 100° T for 30 miles. A second observation of the sun then gave an intercept of 4.0' away bearing 314° T when using an assumed position obtained by applying the run to the first assumed position. Find the ship's position at the time of the second observation.

12. From assumed position 19° 18' N 160° 42' W an observation of Jupiter gave an intercept of 4.0' towards bearing 100° T. The ship then steamed 289° T for 34 miles. A second observation of the sun then gave an intercept of 7.0' away bearing 200° T when using an assumed position obtained by applying the run to the first assumed position. Find the ship's position at the time of the second observation.

13. In assumed latitude 52° 50' N an observation when worked by longitude by chronometer gave a longitude of 136° 10' W bearing 285° T. The ship then steamed 150° T for 15 miles when a second observation using assumed latitude 52° 40' N gave a longitude of 136° 05' W bearing 205° T. Find the ship's position at the time of the second observation.

14. In assumed latitude  $52^{\circ} 20' N$  an observation when worked by longitude by chronometer gave a longitude of  $164^{\circ} 20' W$  bearing  $080^{\circ} T$ . The ship then steamed  $240^{\circ} T$  for 10 miles when a second observation using assumed latitude obtained by running up the first assumed latitude gave a longitude of  $164^{\circ} 29' W$  bearing  $140^{\circ} T$ . Find the ship's position at the time of the second observation.

15. In assumed position  $50^{\circ} 24' N 22^{\circ} 26' W$  a forenoon sight of the sun gave an intercept of 3.1' away bearing  $102^{\circ} T$ . The ship then steamed  $265^{\circ} T$  for 48 miles when a latitude by meridian altitude of the sun gave  $50^{\circ} 21.8' N$ . Find the ship's position at noon.

16. In assumed position  $5^{\circ} 57' N 88^{\circ} 16' E$  a forenoon sight of the sun gave an intercept of 4.4' towards bearing  $121^{\circ} T$ . The ship then steamed  $088^{\circ} T$  for 33 miles when a latitude by meridian altitude of the sun gave  $5^{\circ} 55.8' N$ . Find the ship's position at noon.

17. In assumed position  $30^{\circ} 45' N 46^{\circ} 40' W$  a forenoon sight of the sun gave an intercept of 6.5 towards bearing  $110^{\circ} T$ . The ship then steamed  $115^{\circ} T$  for 20 miles when a latitude by meridian altitude of the sun gave  $30^{\circ} 30' N$ . Find the ship's position at noon.

18. An observation of a celestial body gave an intercept of 3.5' away bearing  $220^{\circ} T$  using an assumed position of  $32^{\circ} 00' S 115^{\circ} 00' E$ . The ship then steamed  $145^{\circ} T$  for 17 miles and then  $063^{\circ} T$  for 12 miles when a point of land in position  $32^{\circ} 05' S 115^{\circ} 31' E$  then bore  $070^{\circ} T$ . Find the ship's position at the time of the second position line.

## MODULE 2.6

### Latitude by Meridian Altitude

An observation of a body when crossing the observer's meridian is of particular value to the navigator as it provides a quick and easy method of finding a position line which will run east/west near the observer's position and will therefore be coincident with the observer's parallel of latitude. At this time the altitude of a body with constant declination is maximum to a stationary observer and the observation is made by watching the altitude climb to a maximum and recording the value. A closing or opening of the declination and latitude will retard or advance maximum altitude relative to meridian passage, but this effect is often ignored. The accurate time is not required but a time to the nearest minute must be predicted beforehand in order to extract the declination and in order to know at what time to take the observations. It is common practice to take a noon observation of the sun's meridian passage and it is convenient if a star can be found whose meridian passage occurs during morning or evening twilight.

#### Maximum and meridian altitude

As stated above if the ship's speed and the rate of change of declination are causing the latitude and declination to close then maximum altitude will occur after meridian passage. If latitude and declination are opening then maximum altitude will occur before meridian passage. An appreciation of the magnitude of this effect is given by considering the formula:

$$\frac{15.3 y (\tan \text{lat} \pm \tan \text{dec})}{60}$$

which gives the time interval in minutes between meridian and maximum altitude for a vessel steaming north or south when  $y$  is the combined change of latitude and declination. Any east or west motion of the vessel will also have an effect and modify the factor  $y$  by a small amount positive if going west and negative if going



east. A vessel in latitude  $60^{\circ}$  N steaming north at 19 knots observing the sun with declination  $5^{\circ}$  S and changing south by  $1.0'$  per hour, will have maximum altitude 9.3 minutes before meridian passage. In latitude  $20^{\circ}$  N this would reduce to 2.3 minutes. If this is not taken into account when observing meridian altitudes then the former case will result in an error in the latitude of about  $1.5'$  and the latter case of less than  $0.5'$ . In practice in the open ocean these errors are not substantial and are often ignored. On fast vessels however they should be considered and if appropriate reduced by observing the meridian altitude at the correct time of meridian passage rather than observing the maximum altitude.

#### Time of meridian passage

There are two methods of finding the time of meridian passage from the Nautical Almanac.

##### Method 1

At meridian passage, by definition the Local Hour Angle (LHA) of the body is zero. The Greenwich Hour Angle (GHA) is therefore equal to the longitude of the observer. Longitude must be expressed westerly from Greenwich as is the GHA.

$$\text{GHA} = \text{W Longitude}$$

Thus the time of the meridian passage can be found by inspection of the Nautical Almanac to find the time at which the particular GHA occurs. Care must be taken to use the correct date at Greenwich. By convention all dates given are at the ship as would be the case in practice. The date at Greenwich may be the following date if the observer's longitude is west and the preceding date if in east longitude.

##### Procedure

1. Write down the GHA (west longitude or (360 - east longitude)).
2. Inspect the almanac on the date in question to extract the hour when the GHA is the next value below the value in 1. Take the difference between the two values which will be the increment.
3. Inspect the increment tables to find the minutes and seconds of the time. For appropriate bodies the increment should be adjusted for the  $v$  correction if absolute accuracy is required but in practice this can be ignored.

4. The hour from 2 and the minutes and seconds from 3 give the UT of meridian passage.

5. Check that the UT with the longitude in time applied still give the correct date at the ship. If not the problem must be reworked using the preceding Greenwich date if in east longitude or the following Greenwich date if in west longitude. With practice this check can be done mentally before starting.

#### Example 1

Find the UT and LMT of meridian passage of the sun over the meridian of an observer in longitude  $50^{\circ} 14' \text{ W}$  on 5th January.

GHA = W longitude	$50^{\circ} 14.0'$
For UT 15h on 5th GHA	$43^{\circ} 40.1'$
difference (increment)	$6^{\circ} 33.9'$

from sun increment tables  $6^{\circ} 33.9'$  corresponds to an increment of 26m 15s

UT mer pass.	15h 26m 15s 5th Jan.
longitude in time	$3\text{h } 20\text{m } 56\text{s}$
LMT for long $50^{\circ} 14' \text{ W}$	$12\text{h } 05\text{m } 19\text{s } 5\text{th Jan.}$

#### Example 2

Find the UT and LMT of meridian passage of the moon over the meridian of  $168^{\circ} 30' \text{ E}$  on 19th December.

GHA = W longitude	$191^{\circ} 30.0'$
GHA for UT 20h on 18th	$184^{\circ} 37.6'$ $v = 11.3$
difference	$6^{\circ} 52.4'$
'v'	$-5.4'$
increment	$6^{\circ} 47.0'$

from increment tables increment = 28m 26s

GHA meridian passage	20h 28m 26s 18th Dec.
longitude in time	$11\text{h } 14\text{m } 00\text{s}$
LMT for longitude $40^{\circ} 38' \text{ E}$	$31\text{h } 42\text{m } 26\text{s}$
=	$07\text{h } 42\text{m } 26\text{s } 19\text{th Dec.}$

#### Notes:

1. The longitude in time added to the UT for E longitude was going to produce a change in date. The previous date at Greenwich was therefore used.

2. In practice the 'v' correction may be ignored and this will not produce any significant error. To get the time to the nearest second however it must be applied in the opposite way to that when taking out the GHA.

**Example 3**

Find the UT and LMT of meridian passage of the star Aldebaran over the meridian of 150° 30' W on 31st October.

GHA star	150° 30.0'
	<u>360°</u>
	510° 30.0'
SHA star	<u>290° 57.8'</u>
GHA $\gamma$	219° 32.2'
GHA $\gamma$ 12h 31st	<u>219° 22.7'</u>
difference = increment	0° 09.5'
from Aries increment table    increment = 0m 40s	
UT meridian passage	12h 00m 40s 31st Oct.
longitude in time	<u>10h 02m 00s</u>
LMT for 150° 30' W	01h 58m 40s 31st Oct.

Note: For a star the SHA must be subtracted from the GHA to get GHA Aries.

**Method 2**

The daily pages of the Nautical Almanac give times to the nearest minute for meridian passage of the sun, moon, planets, and the first point of Aries. The sun's and the moon's meridian passage is given in a box at the lower right of the right hand page once for each day on the page. For the planets it is given in a box at the lower right hand corner of the left page, once for the three days, and for Aries at the foot of the Aries GHA column. These times are local mean times and require correction for longitude to give the UT.

**Sun**

The values given under the heading 'Sun mer pass.' vary between 1144 and 1216 and may be taken to be the LMT of meridian passage of the sun across any meridian. The difference between the figure given and 1200 will be the Equation of Time to the nearest minute. The UT of the sun's meridian passage may very quickly be found by applying the longitude in time to this figure.

The examples that were used for Method 1 will be repeated here.

**Example 1**

Find the UT and LMT of meridian passage of the sun over the meridian of an observer in longitude 50° 14' W on 5th January.

From almanac for 5th LMT mer pass.	1205
longitude in time	<u>0321</u>
UT meridian passage	1526

The time to the nearest minute is acceptable considering the moderate rate of change of declination of the sun, and is clearly quicker and easier than Method 1.

**Moon**

The LMT of meridian passage of the moon is given once for each day at the foot of the right hand daily page for upper and lower meridian passages. It will be seen that the times given get later each day by an average of about 50 minutes. The figures given must be taken to apply only to the Greenwich meridian and a longitude correction which is a proportion of the daily retardation must be applied, that proportion being the longitude divided by 360°.

Thus

$$\text{longitude correction} = \frac{\text{daily retardation} \times \text{longitude}}{360}$$

Any meridian in easterly longitude will pass beneath the sun before the meridian of Greenwich. In this case the daily retardation is taken as the difference between meridian passages on the day in question and the previous day, and the longitude correction is negative. For a meridian in westerly longitude the daily retardation is taken as the difference between meridian passages for the day in question and the following day, and the correction is positive. The longitude correction is tabulated in the Nautical Almanac under the name of Table II on the penultimate page of the almanac. Tabulation is against longitude and daily retardation. It must however be quicker to obtain the solution from a calculator using the above formula.

The correction will give the LMT for the observer's meridian. After correction the longitude in time is applied in the usual way to obtain the UT.



*Procedure*

1. Write down the time of the moon's meridian passage for the day in question.

2. Under this write the time of the preceding meridian passage if in east longitude or the following meridian passage if in west longitude. Note that as there is more than 24 hours between meridian passages the two times written down do not necessarily occur on consecutive dates.

3. Take the difference between the two meridian passage times and calculate the longitude correction by:

$$\text{correction} = \frac{\text{longitude} \times \text{difference}}{360}$$

4. Apply the longitude correction to the LMT of meridian passage for the day in question positive if in west longitude and negative if in east longitude (the result must lie between the two times extracted).

5. Apply the longitude in time to obtain the UT.

**Example 2**

Find the UT and LMT of meridian passage of the moon over the meridian of 168° 30' E on 19th December.

LMT meridian passage for longitude 0° on 19th Dec.	0806
LMT meridian passage for longitude 0° on 18th Dec.	<u>0717</u>
difference = retardation	49m

$$\text{longitude correction} = \frac{49 \times 168.5'}{360} = 23\text{m}$$

LMT meridian passage for longitude 0° on 2nd Nov.	0806
longitude correction	<u>23</u>
LMT meridian passage for longitude 168° 30' E	0743
longitude in time	<u>1114</u>
UT meridian passage longitude 168° 30' E	2029 18th Dec.

**Planets**

The LMT of meridian passage for the four navigational planets are given at the foot of the left hand page in the almanac. One figure is given for the three days for each planet referring to the middle day on the page. Again this is an LMT for the Greenwich meridian and theoretically a longitude correction should be applied. However the amount of change over a day is never more

than a few minutes and the rate of change of declination of the planets is small. Any error by not applying the longitude correction will be negligible and the correction may be ignored. It only remains to apply the longitude in time to obtain the UT.

**Example 3**

Find the UT and LMT of meridian passage of the planet Mars over the meridian of 165° 15' E on 31st October.

LMT meridian passage Mars 31st	2000
longitude in time	<u>1101</u>
UT meridian passage Mars	0859 31st

**Stars**

The time of meridian passage of a star is required only to enable the navigator to know when to commence his observations. The declination of a star remains constant over long periods and therefore extreme accuracy in the time of meridian passage is not required.

The LMT of the meridian passage of the First Point of Aries is given at the foot of the Aries column in the almanac. This will always get approximately four minutes earlier each successive day. The time given refers to the middle day of the page and the time for the first day can be found by adding four minutes and that for the third day by subtracting four minutes. The longitude correction will never exceed two minutes and can be ignored.

A star will cross any meridian earlier than Aries by the amount of its SHA in time. Strictly speaking this should be calculated by:

$$\frac{\text{SHA}}{15^\circ 02.5'}$$

as 15° 02.5' is the hourly rotation of the earth. No significant error will be caused if 15° is used.

**Example 4**

Find the UT and LMT of meridian passage of the star Aldebaran over the meridian of 150° 30' W on 31st October.

LMT meridian passage ♃ 31st	2121 (2117 + 4 minutes)
SHA in time	<u>1924</u>
LMT meridian passage star	0157
longitude in time	<u>1002</u>
UT meridian passage star	1159 31st

**To find if any stars will cross the observer's meridian during the period of twilight**

If the SHA of the celestial meridian of the observer is found for the beginning of twilight and also for the end of twilight, then any star with an SHA between the two values will cross the observer's meridian during twilight and can be observed as part of star sights.

**Example**

Find any stars which will cross the meridian of  $161^\circ$  W during the period 1712 to 1750 LMT on 31st October.

LMT beginning of twilight	1712
longitude in time	<u>1044</u>
UT beginning of twilight	0356 1st November

GHA $\sphericalcap$ 03h	$84^\circ 59.6'$
increment 56m	<u><math>14^\circ 02.3'</math></u>
GHA $\sphericalcap$ 0356	$98^\circ 01.9'$
GHA star = W'ly long	<u><math>161^\circ 00.0'</math></u>
SHA star	$62^\circ 58.1'$ will cross meridian at 1712

At 1750, that is 38 minutes later the earth will have rotated through:

$$\frac{38 \times 15^\circ 02.5'}{60} = 9.5 \text{ approximately}$$

Hence at 1750 the meridian of SHA  $62^\circ 58.1' - 9^\circ 30'$  will cross the observer's meridian.

Thus between 1712 and 1750 any stars with SHA between  $62^\circ 58.1'$  and  $53^\circ 28.1'$  will cross an observer's meridian in  $161^\circ$  W.

By inspection of the almanac the star Peacock with SHA  $53^\circ 31.1'$  and the star Altair with SHA  $62^\circ 15.7'$  will be suitable.

**Finding the Latitude**

When a celestial body is on the observer's meridian then the three arcs which represent declination, zenith distance and latitude are all measured along the same meridian, in other words the meridians of the observer and the body are coincident. In this case there is a simple relationship between declination, zenith distance and latitude, which enables the unknown, the latitude to be found. The relationship is shown in Figure 2.6.1.

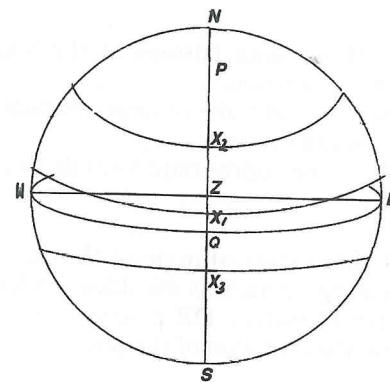


FIG. 2.6.1

In Figure 2.6.1.

Z is the observer's zenith.

WQE is the equinoctial.

ZQ represents the observer's latitude.

NS is the observer's meridian.

P is the elevated pole.

$X_1$ ,  $X_2$  and  $X_3$  are three bodies which are on the observer's meridian.

$X_1$  has declination the same name as the latitude but less than the latitude, and its zenith distance is  $ZX_1$ , and declination  $QX_1$ .

$X_2$  has declination the same name and greater than the latitude, and its zenith distance is  $ZX_2$ , and declination  $QX_2$ .

$X_3$  has declination of opposite name to the latitude, and its zenith distance is  $ZX_3$  and declination  $QX_3$ .

From Figure 2.5.1 it can be seen that:

for body  $X_1$  the latitude will be given by:

$$ZQ = ZX_1 + QX_1 \text{ (latitude = zenith distance + declination)}$$

for body  $X_2$  the latitude will be given by:

$$ZQ = QX_2 - ZX_2 \text{ (latitude = declination - zenith distance)}$$

for body  $X_3$  the latitude will be given by:

$$ZQ = ZX_3 - QX_3 \text{ (latitude = zenith distance - declination)}$$

These circumstances and results are difficult to remember but may easily be deduced in each problem as shown in the following examples.



*Procedure*

1. Find the time of meridian passage of the body and extract the declination from the almanac.
2. Correct the sextant altitude to true altitude and subtract from  $90^\circ$  to give the zenith distance.
3. Deduce and apply the appropriate formula to give latitude.

**Example 1**

On 18th December the sextant altitude of the star Diphda whilst on the meridian bearing south was  $46^\circ 15.4'$ . Index error  $1.4'$  on the arc. Height of eye 12 metres. DR position  $25^\circ 33' N 33^\circ 52' W$ . Find the latitude and the direction of the position line.

Sextant altitude	$46^\circ 15.4'$
index error	$-1.4'$
observed altitude	$46^\circ 14.0'$
dip	$-6.1'$
apparent altitude	$46^\circ 07.9'$
total correction	$-0.9'$
true altitude	$46^\circ 07.0'$
	$90^\circ$
zenith distance	$43^\circ 53.0'$
declination	$17^\circ 58.0' S$
latitude	$25^\circ 55.0' N$

position line was 090/270

Notes: No time for the meridian passage was necessary because the declination is the same for the three days on the daily page.

The Figure 2.6.2 was drawn to represent a small sketch of the meridian as shown in Figure 2.6.1 in order to establish the

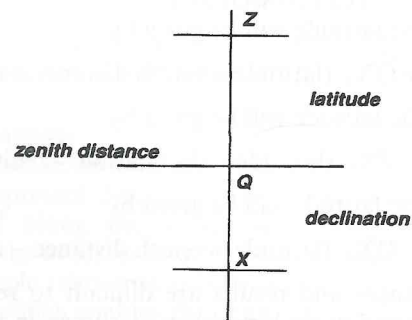


FIG. 2.6.2

appropriate rule to apply to find latitude. If the point Q is inserted first to represent the point on the equinoctial where it crosses the observer's meridian, the point X can be inserted, but it must be to the south of Q because the declination is south. The point Z representing the observer's zenith can then be inserted. This must be to the north of X because the bearing of the body was south when it was on the meridian. The point Z must also be to the north of Q because the zenith distance was more than the declination. Hence Z is to the north of Q denoting that the latitude is north and equal to (zenith distance - declination).

**Example 2**

On 5th January the sextant altitude of the star Fomalhaut whilst on the meridian bearing south was  $77^\circ 52.4'$ . Index error  $3.0'$  off the arc. Height of eye 11 metres. Find the latitude and the direction of the position line.

Sextant altitude	$77^\circ 52.4'$
index error	$+3.0'$
observed altitude	$77^\circ 55.4'$
dip	$-5.8'$
apparent altitude	$77^\circ 49.6'$
total correction	$-0.2'$
true altitude	$77^\circ 49.4'$
	$90^\circ$
zenith distance	$12^\circ 10.6'$
declination	$29^\circ 36.7' S$
latitude	$17^\circ 26.1' S$

position line was 090/270

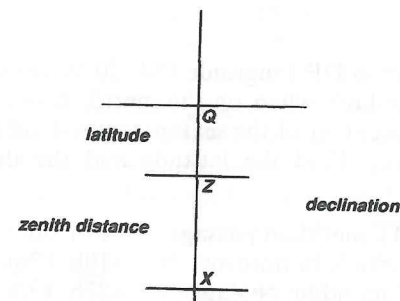


FIG. 2.6.3

Note: The diagram was drawn in the same way as for the previous example but because the zenith distance was less than the declination, Z, the zenith, must lie to the south of Q giving a south latitude.

## EXERCISE 2.6.1

1. On 19th September the sextant altitude of the star Aldebaran on the meridian was  $71^{\circ} 22.8'$ . Index error  $1.4'$  off the arc. Height of eye 14.5 metres. The star was bearing south. Find the latitude and the direction of the position line.

2. On 19th December the sextant altitude of the star Dubhe on the meridian was  $28^{\circ} 06.2'$ . Index error  $0.6'$  on the arc. Height of eye 15.3 metres. The star was bearing north. Find the latitude and the direction of the position line.

3. On 5th January the sextant altitude of the star Regulus on the meridian was  $28^{\circ} 14.4'$ . Index error  $1.4'$  off the arc. Height of eye 14.4 metres. The star was bearing north. Find the latitude and the direction of the position line.

4. On 20th September the sextant altitude of the star Rigel on the meridian was  $71^{\circ} 22.8'$ . Index error  $0.4'$  on the arc. Height of eye 14.5 metres. The star was bearing north. Find the latitude and the direction of the position line.

5. On 27th June the sextant altitude of the star Alioth on the meridian was  $34^{\circ} 03.5'$ . Index error  $1.8'$  off the arc. Height of eye 12.0 metres. The star was bearing north. Find the latitude and the direction of the position line.

In the following examples using the sun and the moon, the time of meridian passage must first be found to obtain the declination.

**Example 3**

On 18th December in DR longitude  $154^{\circ} 20' W$  the sextant altitude of the sun's lower limb when on the meridian bearing south was  $44^{\circ} 20.8'$ . The index error of the sextant was  $0.4'$  off the arc. Height of eye 15.3 metres. Find the latitude and the direction of the position line.

LMT meridian passage	11h 56m
longitude in time	<u>10h 17m</u>
UT meridian passage	22h 13m
declination	$23^{\circ} 23.7' S$

sextant altitude	$44^{\circ} 20.8'$
index error	<u>+0.4'</u>
observed altitude	$44^{\circ} 21.2'$
dip	<u>-6.9'</u>
apparent altitude	$44^{\circ} 14.3'$
total correction	<u>+15.3'</u>
true altitude	$44^{\circ} 29.6'$
	<u>90^{\circ}</u>
zenith distance	$45^{\circ} 30.4'$
declination	<u><math>23^{\circ} 23.7' S</math></u>
latitude	$22^{\circ} 06.7' N$

position line runs 090/270 through  $22^{\circ} 06.7' N 154^{\circ} 20' W$

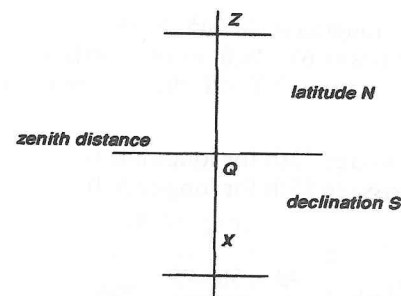


FIG. 2.6.4

## EXERCISE 2.6.2

1. On 18th December in DR position  $00^{\circ} 20' N 162^{\circ} 20' W$  the sextant altitude of the sun's lower limb when on the meridian was  $66^{\circ} 10.4'$  bearing south. Sextant index error was  $1.2'$  on the arc. Height of eye 13.2 metres. Find the latitude and the direction of the position line.

2. On 28th June in DR position  $25^{\circ} 10' S 40^{\circ} 20' W$  the sextant altitude of the sun's lower limb when on the meridian was  $41^{\circ} 26.4'$  bearing north. Sextant index error was  $2.4'$  off the arc. Height of eye 7.3 metres. Find the latitude and the direction of the position line.

3. On 6th January in DR position  $51^{\circ} 30' S 96^{\circ} 35' W$  the sextant altitude of the sun's upper limb when on the meridian was  $61^{\circ} 25.0'$  bearing north. Sextant index error was  $1.4'$  on the arc.



Height of eye 11.5 metres. Find the latitude and the direction of the position line.

4. On 30th September in DR position  $36^{\circ} 55' N 165^{\circ} 30' E$  the sextant altitude of the sun's lower limb when on the meridian was  $50^{\circ} 11.8'$  bearing south. Sextant index error was  $1.6'$  off the arc. Height of eye 14.0 metres. Find the latitude and the direction of the position line.

5. On 19th September in DR longitude  $141^{\circ} 10.8' E$  the sextant altitude of the sun's lower limb when on the meridian was  $36^{\circ} 37.6'$  bearing  $000^{\circ} T$ . Sextant index error was  $1.6'$  off the arc. Height of eye 13.0 metres. Find the latitude and the direction of the position line.

#### Example 4

On 27th June in longitude  $58^{\circ} 45' W$  the sextant altitude of the moon's lower limb was  $67^{\circ} 48.6'$  to the north of the observer. The sextant index error was  $2.0'$  off the arc and the height of eye 9.5 metres.

LMT meridian passage 27th for longitude 0	10h 08m
LMT meridian passage 28th for longitude 0	<u>10h 57m</u>
difference	49m

$$\text{correction for longitude } \frac{49 \times 58^{\circ} 45'}{360^{\circ}} = 8m$$

LMT meridian passage 27th for longitude $0^{\circ}$	10h 08m
longitude correction	<u>8m</u>
LMT meridian passage for longitude $58^{\circ} 45' W$	10h 16m
longitude in time	<u>3h 55m</u>
UT meridian passage for longitude $58^{\circ} 45' W$	14h 11m 27th

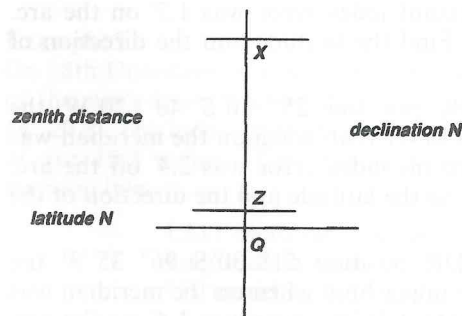


FIG. 2.6.5

declination	$23^{\circ} 06.9' N$ H.P. 54.5
'd' corr	<u>+1.3'</u>
declination	$23^{\circ} 08.2' N$
sextant altitude	$67^{\circ} 48.6'$
index error	<u>+2.0'</u>
observed alt.	$67^{\circ} 50.6'$
dip	<u>-5.4'</u>
apparent alt.	$67^{\circ} 45.2'$
main corr.	<u>+32.1'</u>
2nd corr.	<u>2.9'</u>
true altitude	$68^{\circ} 20.2'$
zenith distance	$21^{\circ} 39.8' N$
declination	$23^{\circ} 08.2' N$
latitude	$1^{\circ} 28.4' N$

position line runs 090/270 through  $1^{\circ} 28.4' N 58^{\circ} 45' W$

#### EXERCISE 2.6.3

1. On 5th January in DR longitude  $45^{\circ} 20' E$  the sextant altitude of the moon's lower limb when on the meridian was  $40^{\circ} 18.5'$  bearing south. Sextant index error was nil. Height of eye 5.5 metres. Find the latitude and the direction of the position line.

2. On 19th September in DR longitude  $162^{\circ} 45' W$  the sextant altitude of the moon's upper limb when on the meridian was  $30^{\circ} 30.5'$  bearing north. Sextant index error was  $1.5'$  on the arc. Height of eye 10 metres. Find the latitude and the direction of the position line.

3. On 19th December in DR longitude  $130^{\circ} E$  the sextant altitude of the moon's upper limb when on the meridian was  $70^{\circ} 30'$  bearing north. Sextant index error was nil. Height of eye 9.0 metres. Find the latitude and the direction of the position line.

4. On 30th September in DR longitude  $0^{\circ}$  the sextant altitude of the moon's lower limb when on the meridian was  $68^{\circ} 18.6'$  bearing south. Sextant index error was nil. Height of eye 8.6 metres. Find the latitude and the direction of the position line.

#### Computing the sextant altitude of a star when on the meridian

If it is required to observe the meridian passage of a star then not only is it necessary to find the time when the star is on the





to be circumpolar. In order to find the time of a star's lower meridian passage then the almanac should be consulted for the time when the star's GHA is equal to the (observer's westerly longitude + 180°). Otherwise the procedure is the same as described for finding the time of upper meridian passage.

#### Procedure

1. Find the LMT of lower meridian passage in order to know at what time to commence observation.
2. Extract the star's declination from the almanac.
3. Correct the altitude of the star.
4. Add the polar distance of the star to the true altitude. The latitude must be named the same as the declination.

#### Example

On 18th September, the sextant altitude of Atria on the meridian below the pole was 19° 41.8'. The observer's longitude was 138° 30' E. The index error was 0.8' on the arc and the height of eye 9.7 metres. Find the latitude and the direction of the position line.

sextant altitude	19° 41.8'	declination	69° 02.3' S
index error	<u>-0.8'</u>		<u>90°</u>
observed altitude	19° 41.0'	polar dist.	20° 57.7'
dip	<u>-5.5'</u>		
apparent altitude	19° 35.5'		
total corr	<u>-2.7'</u>		
true altitude	19° 32.8'		
polar distance	<u>20° 57.7'</u>		
latitude	40° 30.5' S		

position line runs 090/270 through 40° 30.5' S 138° 30' E

#### EXERCISE 2.6.4

1. On 18th December the sextant altitude of the star Dubhe on the meridian below the pole was 22° 19.5'. Sextant index error 2.2' on the arc. Height of eye 12.8 metres. Find the latitude.
2. On 19th December the sextant altitude of the star Alkaid on the meridian below the pole was 12° 27.9'. Sextant index error 2.4' on the arc. Height of eye 12.8 metres. Find the latitude.

3. On 7th January the sextant altitude of the star Schedar on the meridian below the pole was 21° 48.0'. Sextant index error 0.8' off the arc. Height of eye 13.2 metres. Find the latitude.

4. On 20th September the sextant altitude of the star Avior on the meridian below the pole was 19° 32.4'. Sextant index error 1.2' off the arc. Height of eye 14 metres. Find the latitude.

5. On 28th June the sextant altitude of the star Achernar on the meridian below the pole was 13° 00.4'. Sextant index error 1.4' on the arc. Height of eye 12.5 metres. Find the latitude.

### Calculation of position lines from bodies out of the meridian

There have been many methods devised in the past of obtaining position information from astronomical observations. Most of them have been devised with the quickest possible solution in mind. Many have been in tabular form to reduce the amount of calculation required of the navigator and these have been known as short method tables or sight reduction tables. They are no doubt still in use and most navigators have found his most favoured tabular method. In professional examinations these tables have traditionally not been allowed and full solution of the PZX triangle has been taught in navigation schools. Before the ubiquitous hand held calculator a logarithmic solution was used and the haversine formula best suited this method. With the availability of calculators the importance of 'short method' tables has decreased and the haversine formula is no longer the most convenient for manual solution. Here basic principles are best demonstrated by reverting back to manual solution using the fundamental spherical cosine formula. The calculations are no longer onerous and this is probably the quickest way of producing a result. It is now accepted in professional examinations and is used here.

The navigator may want to experiment himself with his personal programmable calculator or with his computer. It is within the abilities of most competent computer owners to programme the mathematics and for this purpose the fundamental formula described is the best basis for the calculations. The Nautical Almanac gives instructions on one efficient approach to this in its explanation pages and also gives a tabular method. Commercial software is available which stores almanac data to further ease the navigator's task. Most people would agree however that complete reliance on the microchip is not desirable, certainly not without understanding the basic principles involved. It is these basic principles with which we are concerned here.

#### Definitions

*Vertical circle.* A great circle on the celestial sphere which passes through the observer's zenith.

*Prime vertical.* The vertical circle whose direction is east/west.

The reduction of sights of bodies out of the meridian is essentially the solution of a spherical triangle on the celestial sphere. This triangle is formed by the intersection of the three great circles, the observer's celestial meridian, the celestial meridian of the body observed and the vertical circle through the body. This triangle is represented in Figure 2.7.1.

The angles of the triangle will be:

1. Angle P. The angle at the pole between the meridians of the observer and that of the body. This is the Local Hour Angle of the body when the body is to the west of the observer's meridian and  $(360^\circ - \text{Local Hour Angle})$  when the body is to the east of the observer's meridian.

2. Angle Z. The angle at the zenith between the observer's meridian and the vertical circle through the body. This is the azimuth of the body.

3. Angle X. The parallactic angle. This is not used in the calculations.

The three sides of the triangle will be:

1. Side PZ. The angular distance of the zenith from the pole. This is the complement of the latitude or co-lat.  $(90^\circ - \text{latitude})$ .

2. Side PX. The angular distance of the body from the pole. This is called the polar distance and will be equal to  $(90^\circ - \text{declination})$ .

3. Side ZX. The angular distance of the body from the zenith. This is the zenith distance and will be equal to  $(90^\circ - \text{true altitude})$ .

Figure 2.7.1 represents the celestial sphere drawn on the plane of the rational horizon, that is looking down from above the observer's zenith. The great circle WZE is the prime vertical and any great circle passing through Z will be a vertical circle. NS is the observer's meridian with the elevated pole in this case the north pole shown at P. The great circle WQE is the equinoctial or celestial equator. The declination circle of a body in north latitude with declination less than the latitude is shown with the body at X. Because the declination is less than the latitude the declination circle will pass closer to the equinoctial than the zenith and the body will be to the south of the observer at meridian passage. This figure is the usual projection used to illustrate the PZX triangle. As for any triangle in



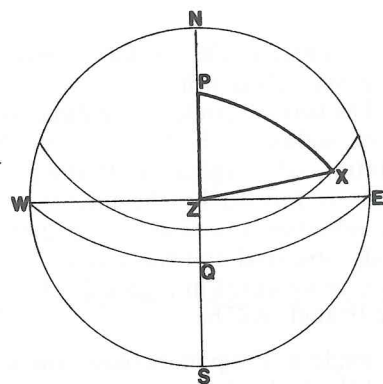


FIG. 2.7.1

order to solve we need to know, or be able to find, at least three parts either angles or sides. In fact we can only know two of its parts. PX is the complement of the declination which we can obtain from the nautical almanac as long as we have taken an accurate time of the observation. The observation of altitude when corrected will give the side ZX, the zenith distance, that is  $(90^\circ - \text{true altitude})$ . The triangle can only be solved by making assumptions about one or more parts of the triangle, and therefore the solution will only be correct if the assumptions made are correct. The part or parts assumed will depend upon the method used.

#### The Intercept Method (Marcq St. Hilaire)

Module 2.5 (Position Lines and Position Circles) should have been studied and understood before reading the explanation of the calculations involved in this method.

It has been stated that any observation may be solved by this method. There are other methods which have been favoured in the past and one of these will be looked at later.

In the intercept method the arguments used are:

Side PX, the complement of the declination.

Angle P, derived by assuming a longitude which is applied to the GHA to find LHA.

Side PZ, derived by assuming a latitude and subtracting it from  $90^\circ$ .

The solution is made for ZX, the zenith distance and Z, the azimuth or bearing. In order to find LHA and the declination an

accurate Greenwich time of observation to the nearest second is required. This has traditionally been taken from a chronometer keeping UT, but the importance of chronometers has been reduced by the high quality of modern personal time pieces, and any good watch can be used. The important thing is that the error in the watch is regularly monitored by time signal and any error to the nearest second applied. Chronometers are normally kept on UT but if a deck watch is used the correction from the ship's time being kept by the watch to UT must also be made.

The solution gives the zenith distance and bearing which would have been observed at the time of the observation if the observer were in the assumed latitude and longitude. Remember from Module 2.5 that the zenith distance defines a position circle centred upon the geographical position of the body observed.

On the assumption that the true position is somewhere near the assumed position then the bearing calculated can be taken to be of sufficient accuracy. The calculated zenith distance however gives a position circle at right angles to the bearing passing through the assumed position. The true zenith distance derived from the observation will show whether the observer is further away from or closer to the geographical position of the body than the assumed position. The difference between the calculated and the true zenith distances is called the intercept, and named either towards or away depending on whether the true zenith distances is less than or greater than the calculated zenith distance. The true position circle will pass through the end of the intercept. (Intercept Terminal Position or ITP.) Thus one position line is defined by the direction of the position line (at right angles to the bearing), and a position through which it passes (the ITP). Two such calculations yielding two position lines will define the vessel's position.

#### Calculation of the zenith distance

This is best done by the use of the spherical cosine formula if a calculator is being used. This states that in the PZX triangle:

$$\cosine ZX = \cosine PZ \cosine PX + \sine PZ \sine PX \cosine P$$

and

$$\cosine Z = \frac{\cosine PX - \cosine PZ \cosine ZX}{\sine PZ \sine ZX}$$

This can be modified by substituting complements. Thus cosine PX becomes sine declination and cosine PZ becomes sine latitude. Sine PX becomes cosine declination and sine PZ becomes cosine declination. Thus

$$\cos ZX = \sin \text{lat} \sin \text{dec} + \cos \text{lat} \cos \text{dec} \cos P$$

Care should be taken if complements are substituted. By convention P is always the elevated pole and therefore PZ will always be less than  $90^\circ$ , but if declination is opposite to latitude PX will be over  $90^\circ$  and its cosine will be negative. In this case cosine PX becomes  $-\text{sine declination}$ . The equation is therefore best remembered as

$$\cos ZX = \cos \text{lat} \cos \text{dec} \cos P + \sin \text{lat} \sin \text{dec} \quad (\text{lat and dec same name})$$

$$\cos ZX = \cos \text{lat} \cos \text{dec} \cos P - \sin \text{lat} \sin \text{dec} \quad (\text{lat and dec opposite name})$$

The advantage of using the formula without substituting complements is that the calculator will itself insert the correct signs and the correct answer will result without the navigator having to remember them.

The cosine formula is very easily solved with a suitable calculator. It is however unsuitable for logarithmic solution because of the multiple changes between natural and logarithmic functions. Because of this the haversine formula was developed from the cosine formula and was in general use before the availability of hand held calculators. Logarithms are rarely used now and the haversine formula naturally has fallen into disuse. It is however given here as an alternative to the cosine formula for those who still prefer to use a logarithmic solution but all examples given use the cosine formula. The versine is  $(1 - \cosine)$  and the haversine is  $\frac{1}{2}(1 - \cosine)$ .

Derived from the cosine formula the haversine formula states:

$$\text{haversine ZX} = (\text{haversine P sine PZ sine PX}) + \text{haversine (PZ} \sim \text{PX)}$$

#### Procedure

1. From the chronometer reading, deduce the UT. The chronometer may need 12 hours to be added to it. This can be decided by applying the longitude in time to the approximate local time to

find the approximate UT. It may be that the UT is on the following or the preceding date. The date given in any problem will, as in practice, be the date at the ship.

2. With the UT extract the GHA and declination of the body observed.

3. Apply longitude to the GHA to find LHA and hence angle P in the PZX triangle. P is equal to LHA if the body is to the west of the observer and  $(360 - \text{LHA})$  if the body is to the east of the observer.

4. Apply the cosine formula to solve for calculated zenith distance (CZX).

5. Correct the sextant altitude and obtain the true zenith distance (TZX).

6. Take the difference between CZX and TZX to be the intercept and name.

7. Calculate the bearing by ABC tables or cosine formula to give the direction of the position line.

#### Example 1

On 30th September at about 0900 at the ship in DR position  $41^\circ 15' \text{N } 175^\circ 30' \text{W}$ , when a chronometer correct on UT showed 08h 25m 15s, the sextant altitude of the sun's lower limb was  $28^\circ 46.7'$ . Index error  $0.4'$  off the arc. Height of eye 15.8 metres. Find the direction of the position line and a position through which it passes.

approximate LMT	30th 09h 00m		
longitude W	<u>11h 42m</u>		
approximate UT	30th 20h 42m		
UT	20h 25m 15s 30th		
			(12 hours added to the chronometer)
declination	$2^\circ 52.5' \text{S}$	sextant altitude	$28^\circ 46.7'$
'd'	<u>0.4'</u>	index error	<u>+0.4'</u>
declination	$2^\circ 52.9' \text{S}$	observed alt.	$28^\circ 47.1'$
		dip	<u>-7.0'</u>
GHA 20th	$122^\circ 30.1'$	apparent alt.	$28^\circ 40.1'$
increment	<u>6 18.8'</u>	total corr	<u>+14.3'</u>
GHA	$128^\circ 48.9'$	true alt.	$28^\circ 54.4'$
	<u>360^\circ</u>	true ZX	$61^\circ 05.6'$
	$488^\circ 48.9'$		
longitude	<u>175^\circ 30.0' \text{W}</u>		
LHA	$313^\circ 18.9'$		
angle P	$46^\circ 41.1'$		



by cosine formula

$$\begin{aligned}\cosine ZX &= \cosine PZ \cosine PX + \sine PZ \sine PX \cosine P \\ \cosine ZX &= \cosine 48^\circ 45' \cosine 92^\circ 52.9' + \sine 48^\circ 45' \\ &\quad \sine 92^\circ 52.9' \cosine 46^\circ 41.1' \\ &= -0.03315 + 0.51512 \\ &= 0.48197\end{aligned}$$

Calculated ZX	61° 11.2'
True ZX	61° 05.6'
intercept	5.6' towards

A 0.827 S		
B 0.069 S		
C 0.896 S	Azimuth	S 56.0° E or 124° T

From Figure 2.7.2 which shows a plot of the intercept and position line the ITP can be calculated if required. This is the position through which the position line passes which is asked for in the original question.

$$d'lat = 3.1' S \quad \text{departure} = 4.6' E \quad d'long = 4.6 \sec 41^\circ 15' = 6.1' E$$

DR Position	41° 15.0' N	d'long	175° 30.0' W
d'lat	3.1' S		6.1' E
ITP	41° 11.9' N		175° 23.9' W

position line runs 034°/214° through 41° 11.9' N 175° 23.9' W

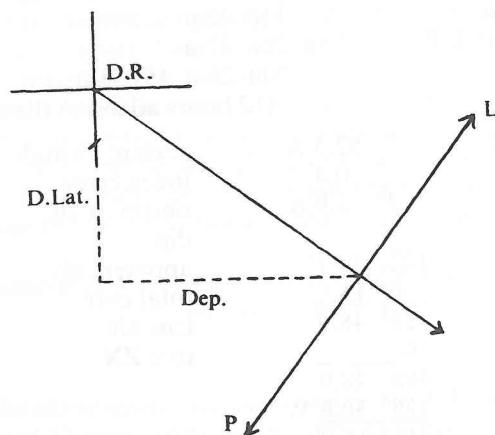


FIG. 2.7.2

Notes:

1. Intermediate steps have been shown in solving the cosine formula equations. These can be dispensed with by a navigator who is proficient with his calculator.

2. The cosine formula to solve for zenith distance may be manipulated by using complements. Thus:

$$\cosine ZX = \cosine PZ \cosine PX + \sine PZ \sine PX \cosine P$$

is equivalent to:

$$\cos ZX = \cos lat \cos dec \cos P + \sin lat \sin dec$$

(if declination is opposite name to latitude then PX is over 90 and cosine PX = -sine dec. It must be remembered that a negative sign is applied to sine dec in this case).

$$\begin{aligned}\cos ZX &= \cos 41^\circ 15' \cos 2^\circ 52.9' \cos 46^\circ 41.1' - \sin 41^\circ 15' \sin 2^\circ 52.9' \\ \cos ZX &= 0.51512 - 0.03317 \\ ZX &= 61^\circ 11.2'\end{aligned}$$

3. The azimuth in the above example was found by using ABC tables. It could equally well be calculated by the cosine formula which states:

$$\cosine Z = \frac{\cosine PX - \cosine PZ \cosine ZX}{\sine PZ \sine ZX}$$

or

$$\begin{aligned}\cosine Z &= \frac{\cosine 92^\circ 52.9' - \cosine 48^\circ 45' \cosine 61^\circ 05.6'}{\sine 48^\circ 45' \sine 61^\circ 05.6'} \\ &= -0.56068 \\ &= N 124.1^\circ E \quad \text{or} \quad 124^\circ T\end{aligned}$$

### EXERCISE 2.7.1

1. On 27th June at about 0900 at the ship in DR position 29° 30' S 121° 20' W, when a chronometer which was correct on UT showed 05h 05m 20s. The sextant altitude of the sun's lower limb was observed to be 21° 11.9'. Sextant index error 1.6' on the

arc. Height of eye 12.0 metres. Find the direction of the position line and a position through which it passes.

2. On 8th January at about 1510 at the ship in DR position  $32^{\circ} 15' S 48^{\circ} 16' W$ , when a chronometer which was correct on UT showed 06h 21m 24s. The sextant altitude of the sun's upper limb was observed to be  $48^{\circ} 59.9'$ . Sextant index error  $0.4'$  on the arc. Height of eye 11.0 metres. Find the direction of the position line and a position through which it passes.

3. On 19th September at about 1547 at the ship in DR position  $00^{\circ} 00' 160^{\circ} 55' W$ , when a chronometer which was correct on UT showed 02h 29m 15s. The sextant altitude of the sun's lower limb was observed to be  $31^{\circ} 46.9'$ . Sextant index error  $0.6'$  off the arc. Height of eye 12.5 metres. Find the direction of the position line and a position through which it passes.

4. On 18th December at about 0846 at the ship in DR position  $43^{\circ} 12' N 38^{\circ} 25' W$ , when a chronometer which was 02m 21s fast on UT showed 11h 21m 52s. The sextant altitude of the sun's lower limb was observed to be  $10^{\circ} 23.9'$ . Sextant index error  $1.6'$  off the arc. Height of eye 11.5 metres. Find the direction of the position line and a position through which it passes.

5. On 30th September at the ship in DR position  $44^{\circ} 05' N 27^{\circ} 41' W$ , at UT 09h 26m 02s. The sextant altitude of the sun's lower limb was observed to be  $16^{\circ} 26.8'$ . Sextant index error  $1.4'$  on the arc. Height of eye 9.0 metres. Find the direction of the position line and a position through which it passes.

**Example 2**

On 9th January at approximate ship's time 1940 in assumed position of  $35^{\circ} 10' S 127^{\circ} 50' E$  the sextant altitude of the star Sirius was observed to be  $37^{\circ} 07.3'$ . Sextant index error  $0.4'$  on the arc. Height of eye 15 metres. A chronometer which was correct on UT showed 11h 15m 10s. Find the direction of the position line and a position through which it passes.

approximate LMT	9th 19h 40m
longitude W	<u>08h 31m</u>
approximate UT	9th 11h 09m
UT	11h 15m 10s 9th

declination	$16^{\circ} 43.2' S$	sextant altitude	$37^{\circ} 07.3'$
GHA $\gamma$ 11h	$273^{\circ} 34.2'$	index error	<u><math>-0.4'</math></u>
increment	$3^{\circ} 48.1'$	observed alt.	$37^{\circ} 06.9'$
GHA $\gamma$	$277^{\circ} 22.3'$	dip	<u><math>-6.8'</math></u>
SHA Sirius	$258^{\circ} 40.7'$	apparent alt.	$37^{\circ} 00.1'$
GHA Sirius	$536^{\circ} 03.0'$	total corr	<u><math>-1.3'</math></u>
	<u><math>360^{\circ}</math></u>	true alt.	$36^{\circ} 58.8'$
GHA Sirius	$176^{\circ} 03.0'$	true ZX	$53^{\circ} 01.2'$
longitude	$127^{\circ} 50.0' E$		
LHA Sirius	$303^{\circ} 53.0'$		
angle P	$56^{\circ} 07.0'$		

by cosine formula

$$\begin{aligned} \cosine ZX &= \cosine PZ \cosine PX + \sine PZ \sine PX \cosine P \\ \cosine ZX &= \cosine 54^{\circ} 50' \cosine 73^{\circ} 16.8' + \sine 54^{\circ} 50' \\ &\quad \sine 73^{\circ} 16.8' \cosine 56^{\circ} 07' \\ &= 0.16570 + 0.43648 \\ ZX &= 52^{\circ} 58.4' \end{aligned}$$

or

$$\begin{aligned} \cos ZX &= \cos \text{lat} \cos \text{dec} \cos P + \sin \text{lat} \sin \text{dec} \\ \cos ZX &= \cos 35^{\circ} 10' \cos 16^{\circ} 43.2' \cos 56^{\circ} 07' + \sin 35^{\circ} 10' \\ &\quad \sin 16^{\circ} 43.2' \\ \cos ZX &= 0.43648 + 0.16570 \\ ZX &= 52^{\circ} 58.4' \end{aligned}$$

Calculated ZX	$52^{\circ} 58.4'$	A	0.473 N
True ZX	<u><math>53^{\circ} 01.2'</math></u>	B	0.362 S
intercept	$2.8'$ away	C	0.111 N Azimuth N $84.8^{\circ} E$ or $085^{\circ} T$

From Figure 2.7.3 d'lat =  $0.3' S$

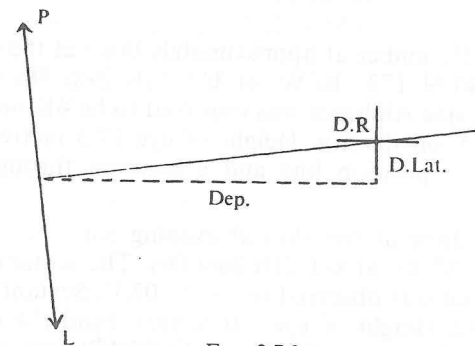


FIG. 2.7.3



$$\text{departure} = 2.8' \text{ W d'long} = 2.8 \sec 35^\circ 10' = 3.4' \text{ W}$$

DR position	35° 10.0' S		127° 50.0' E
d'lat	0.3' S	d'long	3.4' W
ITP	35° 10.3' S		127° 46.6' E

position line runs 355°/175° through 35° 10.3' N 127° 46.6' E

### EXERCISE 2.7.2

1. On 19th September at approximate ship's time 1800 in DR position 24° 30' N 145° 10' E, at UT 08h 19m 50s. The sextant altitude of the star Arcturus was observed to be 40° 07.7'. Sextant index error 0.8' on the arc. Height of eye 12.0 metres. Find the direction of the position line and a position through which it passes.

2. On 30th September at approximate ship's time 0600 ship in DR position 43° 05' N 177° 16' W, at UT 17h 01m 44s. The sextant altitude of the star Schedar was observed to be 41° 54.4'. Sextant index error 0.2' off the arc. Height of eye 13.2 metres. Find the direction of the position line and a position through which it passes.

3. On 19th September at the ship in assumed position 17° 53.6' N 47° 30.0' W, when the chronometer, which was 04m 53s slow on UT, showed 08h 10m 23s. The sextant altitude of the star Alphard during morning twilight was observed to be 18° 06.5'. Sextant index error 0.5' on the arc. Height of eye 18.6 metres. Find the direction of the position line and a position through which it passes.

4. On 18th December at approximately 0600 at the ship in DR position 42° 40' N 172° 10' W, at UT 17h 29m 30s the sextant altitude of the star Alphecca was observed to be 41° 46.7'. Sextant index error 1.3' on the arc. Height of eye 17.5 metres. Find the direction of the position line and a position through which it passes.

5. On 27th June at the ship at evening stars in DR position 40° 59.5' S 56° 57' W, at UT 21h 26m 00s. The sextant altitude of the star Procyon was observed to be 15° 03.1'. Sextant index error 0.6' off the arc. Height of eye 9.0 metres. Find the direction of the position line and a position through which it passes.

### Example 3

On 30th September at approximate ship's time 1319 in assumed position of 14° 38' S 54° 14' W the sextant altitude of the moon's lower limb was observed to be 44° 37.4'. Sextant index error nil. height of eye 12 metres. A chronometer which was correct on UT showed 04h 25m 14s. Find the direction of the position line and a position through which it passes.

approximate LMT	30th 13h 19m	chron.	04h 25m 14s
longitude W	54° 14.0' W	UT	16h 25m 14s 30th
approximate UT	30th 16h 56m		
declination	23° 22.5' S	sextant altitude	44° 37.4'
'd'	+3.7'	index error	—
declination	23° 26.2' S	observed alt.	44° 37.4'
		dip	-6.1'
GHA 16th	1° 53.1'	apparent alt.	44° 31.3'
increment	6° 01.3'	main corr	+50.8'
'v'	2.3'	2nd corr	+7.1'
GHA	7° 56.7'	true altitude	45° 29.2'
longitude	54° 14.0' W	zenith dist.	44° 30.8'
LHA	313° 42.7'		
angle P	46° 17.3'		

by cosine formula

$$\begin{aligned} \cos ZX &= \cos PZ \cos PX + \sin PZ \sin PX \cos P \\ \cos ZX &= \cos 75^\circ 22' \cos 66^\circ 33.8' + \sin 75^\circ 22' \\ &\quad \sin 66^\circ 33.8' \cos 46^\circ 17.3' \\ &= 0.10048 + 0.61345 \\ ZX &= 44^\circ 26.6' \end{aligned}$$

or

$$\begin{aligned} \cos ZX &= \cos \text{lat} \cos \text{dec} \cos P + \sin \text{lat} \sin \text{dec} \\ \cos ZX &= \cos 14^\circ 38' \cos 23^\circ 26.2' \cos 46^\circ 17.3' + \sin 14^\circ 38' \\ &\quad \sin 23^\circ 26.2' \\ \cos ZX &= 0.61345 + 0.10048 \\ ZX &= 44^\circ 26.6' \end{aligned}$$

Calculated ZX	44° 26.6'
True ZX	44° 30.8'
intercept	4.2' away

A 0.250 N

B 0.600 S

C 0.350 S

Azimuth

S 71.3° E or 108.7° T

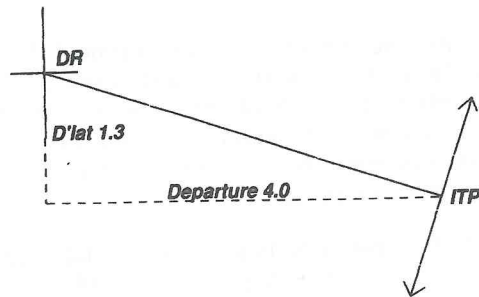


FIG. 2.7.4

From Figure 2.7.4

$$d'lat = 1.3' \text{ N} \quad \text{departure} = 4.0' \text{ W} \quad d'long = 4.0 \sec 14^\circ 38' = 4.1' \text{ W}$$

DR position	14° 38.0' S		54° 14.0' W
d'lat	1.3' N	d'long	4.1' W
ITP	14° 36.7' S		54° 18.1' W

position line runs 018.7°/198.7° through 14° 36.7' S 54° 18.1' W

### EXERCISE 2.7.3

1. On 28th June at approximately 0620 at a ship in assumed position 42° 50' N 41° 30' W the sextant altitude of the moon's lower limb was 31° 51.8'. A chronometer which was correct on UT showed 09h 10m 02s. Index error 2.0' off the arc. Height of eye 10 metres. Find the direction of the position line and a position through which it passes.

2. On 9th January at approximately 1550 hrs at a ship in assumed position 25° 30' N 175° 00' E the sextant altitude of the moon's upper limb was 55° 29.4'. A chronometer which was slow on UT by 1m 24s showed 04h 06m 41s. Index error 2.0' on the arc. Height of eye 7.2 metres. Find the direction of the position line and a position through which it passes.

### Longitude by chronometer

In this method a latitude is assumed. This is used in the PZX triangle with declination and the true zenith distance to solve for angle P and hence Local Hour Angle and longitude. This longitude

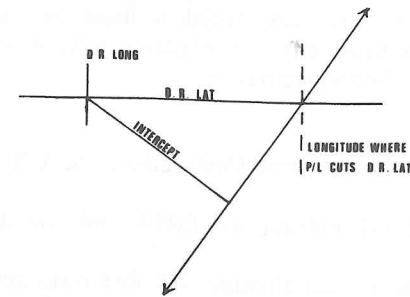


FIG. 2.7.5

will be correct only if the assumed latitude was correct and thus the assumed latitude and calculated longitude give a position through which the position line passes. The direction of the position line must be found as before.

For any one observation there obviously is only one position line regardless of the method used to reduce the observation. The intercept method and the longitude method however result in different positions through which the position line is drawn. Figure 2.7.5 shows the relationship between the information gained from the two methods.

The arguments used to solve the PZX triangle in the longitude by chronometer method are:

1. PZ. This is the complement of the latitude.
2. PX. This is the complement of the declination.
3. ZX. This is the zenith distance or complement of the true altitude.

By cosine formula:

$$\cosine P = \frac{\cosine ZX - \cosine PZ \cosine PX}{\sine PZ \sine PX}$$

or

$$\cosine P = \frac{\cosine ZX - \sin lat \sin dec}{\cos lat \cos dec} \quad (\text{lat and dec same name})$$

$$\cosine P = \frac{\cosine ZX + \sin lat \sin dec}{\cos lat \cos dec} \quad (\text{lat and dec opposite names})$$



If complements are substituted it must be remembered that sine declination must carry a negative sign if the latitude and declination are of opposite names.

*Procedure*

1. From the chronometer time deduce the UT and the date at Greenwich.
2. Using the UT extract the GHA and the declination from the almanac.
3. Correct the sextant altitude and obtain the zenith distance.
4. Solve the cosine formula for angle P and hence the LHA.
5. Apply GHA to LHA to obtain the longitude.
6. Find the true bearing and the direction of the position line.

This method is not suitable for bodies which are close to the meridian. As a rule of thumb it may be said that the body should be at least two hours from its meridian passage. It is particularly suitable for observations of the sun in the forenoon which are going to be run up to noon and combined with a latitude by meridian altitude.

**Example 4**

On 30th September at about 0900 at the ship in DR position 41° 15' N 175° 30' W, when a chronometer correct on UT showed 08h 25m 15s, the sextant altitude of the sun's lower limb was 28° 46.7'. Index error 0.4' off the arc. Height of eye 15.8 metres. Find the direction of the position line and a position through which it passes.

approximate LMT 30th 09h 00m  
 longitude W 11h 42m  
 approximate UT 30th 20h 42m

UT 20h 25m 15s 30th

GHA 20h	122° 30.1'	sextant altitude	28° 46.7'
increment	6° 18.8'	index error	+0.4'
GHA	<u>128° 48.9'</u>	observed alt.	28° 47.1'
		dip	-7.0'
declination	2° 52.5' S	apparent alt.	28° 40.1'
'd' corr	+0.4'	total corr	+14.3'
declination	<u>2° 52.9' S</u>	true altitude	28° 54.4'
		zenith dist.	61° 05.6'

$$\cosine P = \frac{\cosine ZX - \cosine PZ \cosine PX}{\sine PZ \sine PX}$$

or

$$\cosine P = \frac{\cosine ZX + \sin lat \sin dec}{\cos lat \cos dec}$$

$$\begin{aligned} \cosine P &= \frac{\cosine 61^\circ 05.6' + \sin 41^\circ 15' \sin 2^\circ 52.9'}{\cos 41^\circ 15' \cos 2^\circ 52.9'} \\ &= \frac{0.48338 + 0.03315}{0.75089} \end{aligned}$$

P =	46° 32.2'	A	0.831S
LHA	313° 27.8'	B	0.069 S
GHA	<u>128° 48.9'</u>	C	0.900 S
longitude	175° 21.1'	Azimuth	S 55.9° E or 124.1° T

Position line runs 034.1°/214.1° through 41° 15' N 175° 21.1' W

**EXERCISE 2.7.4**

1. On 28th June at approximately 1600 at the ship in DR position 10° 25' N 71° 00' E, when the chronometer, which was fast on UT by 4m 27s, showed 11h 19m 53s, the sextant altitude of the sun's lower limb was 31° 33.3'. Index error 1.2' on the arc. Height of eye 17.0 metres. Find the direction of the position line and the longitude in which it cuts the parallel of the DR latitude.

2. On 19th September at approximately 0730 at the ship in DR position 18° 44' N 127° 00' W when the chronometer, which was correct on UT, showed 04h 01m 42s, the sextant altitude of the sun's upper limb was 24° 34.5'. Index error 0.6' off the arc. Height of eye 18.0 metres. Find the direction of the position line and the longitude in which it cuts the parallel of the DR latitude.

3. On 20th December during the forenoon at the ship in DR position 35° 24' S 171° 15' E, when the chronometer, which was slow on UT by 1m 17s, showed 09h 00m 35s, the sextant altitude of the sun's lower limb was 43° 09.7'. Index error 0.4' on the arc. Height of eye 14.5 metres. Find the direction of the position line and the longitude in which it cuts the parallel of the DR latitude.

4. On 4th January during the forenoon at the ship in DR position 0° 30' S, 0° 04' E when the chronometer, which was correct

on UT, showed 08h 15m 35s, the sextant altitude of the sun's upper limb was  $30^{\circ} 27.1'$ . Index error  $1.4'$  on the arc. Height of eye 19.5 metres. Find the direction of the position line and the longitude in which it cuts the parallel of the DR latitude.

5. On 30th September at approximately 0800 at the ship in DR position  $44^{\circ} 05' N 20^{\circ} 05' W$  at UT 09h 11m 02s, the sextant altitude of the sun's lower limb was  $18^{\circ} 57.5'$ . Index error  $1.4'$  on the arc. Height of eye 9.0 metres. Find the direction of the position line and the longitude in which it cuts the parallel of the DR latitude.

#### Noon position by longitude by chronometer and meridian altitude

A standard method of obtaining a noon position when there is only the sun available for observation is to observe the sun when it is bearing close to east in the forenoon and transfer the position line calculated by longitude by chronometer to the time of noon, that is meridian passage of the sun. The transferred position line can then be crossed with a position line obtained from a latitude by meridian altitude. The noon position can be found without any plotting.

Figure 2.7.6 represents such a morning position line which has been run up to give a noon DR position. The transferred position line through this DR is shown with double arrows. The figure shows that if the noon latitude gives a latitude to the south of the DR then the ship's position must be to the west. If the noon latitude

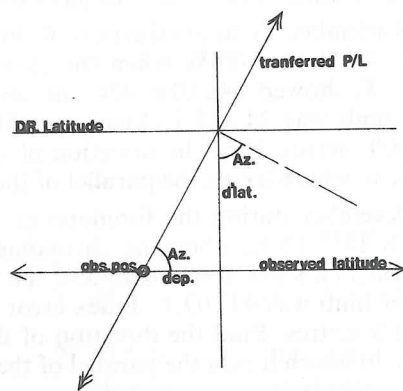


FIG. 2.7.6

is to the north of the DR then the position must be to the east. The amount by which the longitude differs from the DR longitude is given by the number of minutes the noon latitude differs from the DR latitude multiplied by the value 'C' which will have been obtained when working the azimuth at the forenoon sight.

Thus the value 'C' in this respect can be taken as the error in the longitude caused by an error of 1 minute in the latitude.

#### Example 5

On 19th December at approximate ship's time 0810 in assumed position  $25^{\circ} 50' N 50^{\circ} 00' W$  an observation of the sun's lower limb gave a sextant altitude of  $15^{\circ} 47.5'$ . Index error was  $3.0'$  on the arc and height of eye 13.6 metres. The chronometer showed 11h 26m 04s at the time and was slow on UT by 1m 03s. The ship then steamed  $210^{\circ} T$  for 55 miles, when a meridian altitude of the sun's lower limb was  $41^{\circ} 19.8'$  south of the observer. Find the ship's position at noon.

Approximate ship's time	0810
longitude in time	0349
approximate UT	1159 19th

chronometer	11h 26m 04s	sextant altitude	$15^{\circ} 47.5'$
error	$1m 03s$	index error	$-3.0'$
UT	11h 27m 07s 19th	observed alt.	$15^{\circ} 44.5'$
		dip	$-6.5'$
GHA 11h	$345^{\circ} 46.7'$	apparent alt.	$15^{\circ} 38.0'$
increment	$6^{\circ} 46.8'$	total corr	$+12.9'$
GHA	$352^{\circ} 33.5'$	true altitude	$15^{\circ} 50.9'$
		zenith dist.	$74^{\circ} 09.1'$

declination  $23^{\circ} 24.5' S$

$$\cosine P = \frac{\cosine ZX - \sin lat \sin dec}{\cos lat \cos dec}$$

$$\begin{aligned} \cosine P &= \frac{\cosine 74^{\circ} 09.1' + \sin 25^{\circ} 50' \sin 23^{\circ} 24.5'}{\cos 25^{\circ} 50' \cos 23^{\circ} 24.5'} \\ &= \frac{0.27309 + 0.17312}{0.82599} \end{aligned}$$



P = 57° 18.1' A 0.311 S  
 LHA 302° 41.9' B 0.515 S  
 GHA 352° 33.5' C 0.826 S azimuth S 53.2° E  
 longitude 49° 51.6' pos line runs 036.8°/216.8°

DR at forenoon sight 25° 50.0' N 49° 51.6' W  
 run 210° T × 55 miles 47.6' S 30.5' W  
 noon DR 25° 02.4' N 50° 22.1' W

**meridian altitude**

mer. pass.	1157	sextant altitude	41° 19.8'
longitude	<u>0322</u>	index error	<u>-3.0'</u>
UT mer. pass.	1519	observed alt.	41° 16.8'
		dip	<u>-6.5'</u>
declination	23° 24.8'	apparent alt.	41° 10.3'
		total corr	<u>+15.2'</u>
		true altitude	41° 25.5'
		zenith dist.	48° 34.5'
		declination	<u>23° 24.8' S</u>
		latitude	25° 09.7' N
		DR lat.	<u>25° 02.4' N</u>
		difference	7.3' N
		'C'	<u>0.826</u>
		long error	6.0' E

noon DR long 50° 22.1' W  
 long correction 6.0' E  
 noon longitude 50° 16.1' W

noon position 25° 09.7' N 50° 16.1' W

**EXERCISE 2.7.5**

1. On 30th September during the forenoon in assumed position 46° 17' S 157° 20' W an observation of the sun's lower limb gave a sextant altitude of 32° 15'. Index error was 3.0' off the arc and height of eye 11 metres. The chronometer showed 07h 24m 51s at the time and was correct on UT. The ship then steamed 300° T for 45 miles, when a meridian altitude of the sun's lower limb was 46° 47.9' north of the observer. Find the ship's position at noon.

2. On 28th June during at approximate ship's time 0919 in assumed position 38° 15' S 168° 15' E an observation of the sun's lower limb gave a sextant altitude of 17° 18.2'. Index error was 1.0' on the arc and height of eye 8.0 metres. The chronometer showed 10h 05m 17s at the time and was correct on UT. The ship then steamed 045° T for 40 miles, when a meridian altitude of the sun's lower limb was 28° 39.4' north of the observer. Find the ship's position at noon.

## MODULE 2.8

## Latitude by Pole Star

The altitude of the celestial pole is equal to the observer's latitude. Unfortunately the exact position of the pole is not marked and cannot be observed. However the star Polaris has a declination in excess of  $89^\circ$ , so that it describes daily a circle around the pole of radius less than one degree. As it is so near the pole it is referred to as the pole star and its altitude can be observed and small adjustments made to the altitude to give an easy derivation of the latitude.

Figure 2.8.1 represents the daily path of Polaris around the pole. Its polar distance has been exaggerated. If the star is at  $X_1$  the angular distance  $PX_1$ , the polar distance, must be subtracted from the altitude  $NX_1$  to obtain the altitude of the pole, or the latitude. Similarly if the star is at  $X_2$  then the polar distance must be added to the altitude of the star to give that of the pole. At all other times the correction will be the arc  $PY$  in Figure 2.8.1 and this may be

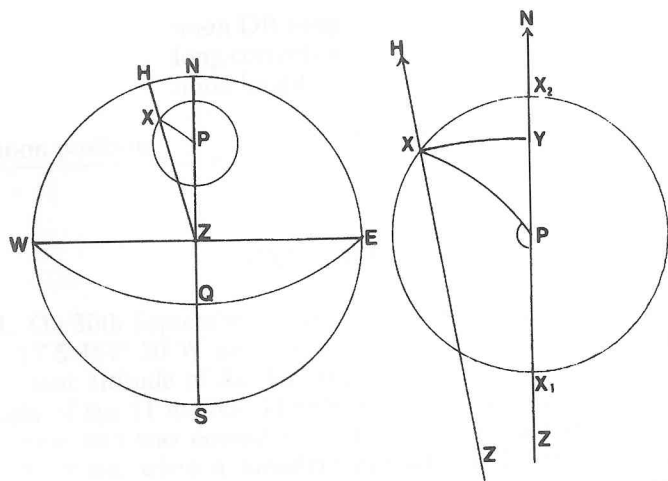


FIG. 2.8.1

positive as shown or negative. The solution of the triangle  $XPY$  for  $PY$  is tabulated in the Nautical Almanac under the title 'Pole Star Tables'. These are found in the back of the almanac.

The solution is arranged in three separate quantities  $a^0$ ,  $a^1$  and  $a^2$ . To each is added a constant, and the sum of the three constants is  $1^\circ$ , which must be subtracted at the end of the calculation. This is done to ensure that all corrections are always positive.

The correction depends upon the LHA of the star. As the SHA can be considered constant for the year it is preferable to tabulate against the argument LHA  $\gamma$ .

*Procedure*

1. From the UT of observation find the GHA  $\gamma$  and apply the DR longitude to get LHA  $\gamma$ .
2. Correct the sextant altitude to obtain true altitude.
3. Using LHA  $\gamma$ , enter the pole star tables and find the column which is headed by the value of LHA  $\gamma$ . There is one column for each 10 degrees of LHA. The three corrections will be found in the same vertical column, which is divided into three sections.

The top section is tabulated against each degree of LHA within the  $10^\circ$  range and  $a^0$  can be extracted with some simple interpolation if necessary.

The middle section is tabulated against latitude and  $a^1$  can be read against the latitude and no interpolation is necessary.

The lower section is tabulated against the month and  $a^2$  can be read off against the correct month without interpolation.

4. The altitude of the pole is given by (true altitude of Polaris  $+a^0 + a^1 + a^2 - 1$ ).

5. Read off the bearing of the star against the latitude from the azimuth table at the foot of the column.

Note: The pole star will not always bear due north and therefore the position line will not be exactly along a parallel. The bearing however will be so close to north that it is usually assumed that the position line does coincide with the observer's parallel. Strictly speaking the latitude derived together with the DR longitude used give a position through which the position line passes with a direction which may be up to 1.7 degrees from east/west.

**Example**

On 21st September in DR position  $37^\circ 58' N 52^\circ 30' E$  at 01h 10m 24s UT an observation of Polaris gave sextant altitude  $38^\circ 40.4'$ . Index error 2.2' off the arc. Height of eye 11.7m. Find the direction of the position line and a position through which it passes.



UT. 01h 10m 24s 21st

GHA $\Upsilon$ 01h	14° 30.0'	sextant altitude	38° 40.4'
increment	<u>2° 36.4'</u>	index error	<u>+2.2'</u>
GHA $\Upsilon$	17° 06.4'	observed alt.	38° 42.6'
longitude E	<u>52° 30.0'</u>	dip	<u>-6.0'</u>
LHA $\Upsilon$	69° 36.4'	apparent alt.	38° 36.6'
		total corr	<u>-1.2'</u>
		true altitude	38° 35.4'
		a <sup>0</sup>	0° 21.7'
		a <sup>1</sup>	0.6'
		a <sup>2</sup>	<u>0.3'</u>
		total	38° 58.0'
			<u>1°</u>
		latitude	37° 58.0' N
		bearing	359.6° T

position line runs 269.6°/089.6° through 37° 58.0' N 52° 30' E

## EXERCISE 2.8.1

1. On 8th January at 19h 25m 22s UT in DR position 49° 20' N 36° 20.4' W the sextant altitude of Polaris was 50° 09.4'. The sextant index error was 1.6' off the arc and the height of eye 12.8 metres. Find the direction of the position line and a position through which it passes.

2. On 20th September at 21h 15m 40s UT in DR position 35° 25' N 36° 25' W the sextant altitude of Polaris was 35° 15.8'. The sextant index error was 0.8' on the arc and the height of eye 11.5 metres. Find the direction of the position line and a position through which it passes.

3. On 27th June at 13h 26m 44s UT in DR position 47° 15' N 158° 40' W the sextant altitude of Polaris was 47° 42.0'. The sextant index error was 1.4' off the arc and the height of eye 6.0 metres. Find the direction of the position line and a position through which it passes.

4. On 30th September at about 0520 local time in DR position 50° 40' N 162° 10.8' E the sextant altitude of Polaris was 51° 10.8'. The chronometer which was 02m 08s slow on UT showed 06h 13m 17s. The sextant index error was 1.2' off the arc and the height

of eye 14.0 metres. Find the direction of the position line and a position through which it passes.

## REVISION EXERCISES

## Paper 1

**Chart: Lands End to Falmouth** Use variation  $5^{\circ}$  W throughout

Use the deviation card in Figure Module 1.3

1. At a time 5 hours after high water Dover on spring tides a vessel was in a position with Lizard Lt. bearing  $000^{\circ}$  T distant 5 miles. Find the compass course to steer to pass 3 miles to the south of Wolf Rock Light, making allowance for any tide you may expect. Estimate the sailing time to the position off Wolf Rock. Vessel's log speed is 12 knots.

2. From a vessel to the south of Mount's Bay steering  $091^{\circ}$  C speed 8 knots Black Head was observed in transit with Lizard lighthouse bearing  $051^{\circ}$  C. After maintaining this course for one hour Lizard Lt. hse. bore  $309^{\circ}$  C. If a current set  $070^{\circ}$  T at 1.5 knots in the interval find the position of the ship at the time of the second observation.

3. It is required to round Lizard point maintaining a distance off Men Hyr Rocks of 1.5 miles. What would be the vertical sextant angle to set on a sextant to observe Lizard light hse.?

4. A vessel steering  $110^{\circ}$  C speed 10 knots observed Longships Lt. bearing  $345^{\circ}$  C and Tater Du Lt. hse. bearing  $035^{\circ}$  C. 1.5 hours later Lizard Point Lt. hse. was bearing  $065^{\circ}$  C while Mullion Island was bearing  $029^{\circ}$  C. Find the set and the drift of the tide in the interval.

5. Find by plane sailing the vessel's position at the end of the third course.

Initial position	$49^{\circ} 30' N$	$8^{\circ} 00' W$
1st course	$261^{\circ} T$	distance 70 miles
2nd course	$210^{\circ} T$	distance 72 miles
3rd course	$166^{\circ} T$	distance 65 miles

6. Find by plane sailing the course and distance between the following positions.

$50^{\circ} 15' N$	$5^{\circ} 25' W$
$52^{\circ} 10' N$	$7^{\circ} 05' W$

7. From the following information find the compass error and the deviation for the ship's head.

Date June 27th	DR position $50^{\circ} 30' N$ $6^{\circ} 30' W$
sun rose bearing $053^{\circ} C$	Variation $8^{\circ} W$

## Paper 2

**Chart: Falmouth to Plymouth** Use  $5^{\circ}$  W variation throughout

Use the deviation card in Module 1.3

1. From a position where Eddystone Rock Lt. bears  $000^{\circ}$  T distant 3 miles find the compass course to steer to a position where Dodman Point bears  $307^{\circ}$  T distant 2.4 miles, in order to counteract a tide estimated to set  $133^{\circ}$  T at 2 knots and allowing for a  $10^{\circ}$  leeway due to a SW'y wind. Ships speed by log 8 knots.

2. The following compass bearings were obtained from a vessel at anchor in Mevagissey Bay:

Chapel Point	$238^{\circ} C$
Black Head	$001^{\circ} C$
Gribbin Head daymark	$056^{\circ} C$

Find the latitude and longitude of the vessel's position and the compass course to steer to arrive at a position where Rame Head chapel ruins is bearing  $000^{\circ}$  T by 3 miles.

3. A vessel steering  $330^{\circ}$  C has the buoy (FL R 10 sec) ( $50^{\circ} 07' N$   $4^{\circ} 30' W$  approximately) bearing  $015^{\circ}$  C distant 1.2 miles. After steaming for 40 minutes at 12 knots the vessel's position was fixed by three bearings:

Gribbin Head	$003^{\circ} C$
Chapel Point	$320^{\circ} C$

Find the set and rate of the current, the course and speed made good.

4. Find the rising and dipping distance of Eddystone Light from a vessel with height of eye 12.5 metres.

5. Find by mercator sailing the position at the end of the run.

Initial position	$55^{\circ} 55' N$	$7^{\circ} 18' E$
Course	$257^{\circ} C$	Variation $8^{\circ} W$ Deviation $3^{\circ} E$
Distance run	120 miles	

6. From the following information find the compass error and the deviation for the ship's head.



Time at ship 1608 29th September. DR position  $43^{\circ} 30' N$   
 $9^{\circ} 40' W$   
 Bearing of the sun by compass  $262^{\circ}$ . Chronometer 05h  
 08m 02s.  
 Chronometer error 2m 18s slow on UT. Variation  $6^{\circ} W$ .

**Paper 3**

**Chart: Lands End to Falmouth** Use variation  $6^{\circ} W$  throughout

**Use the deviation card in Module 3**

1. At 0800 hrs in poor visibility, from a vessel steering  $181^{\circ}$  by gyro, speed 5 knots, the Longships lighthouse bore  $148^{\circ} G$ . Gyro error  $1^{\circ}$  High. The vessel continued on this course and at 0915 Wolf Rock Lt. was observed to bear  $238^{\circ} G$ . If a tide set  $127^{\circ} T$  at 2 knots throughout find the vessels position at 0915.

2. From a position with Wolf Rock Lt. bearing  $350^{\circ} T$  distance 2.4 miles, find the course and distance to a position  $49^{\circ} 46' N$   $5^{\circ} 26.6' W$ . Find also the compass course to steer to counteract a tide setting  $084^{\circ} T$  at 3 knots and 6 degrees leeway due to a SW'y wind, if the vessel's speed by log is 6 knots. What will be the steaming time to the position given.

3. On a vessel at anchor off Falmouth the following compass bearings were taken:

Manacle Point	$226^{\circ} C$
Rosemullion Head	$280^{\circ} C$
St Anthony Head Lt.	$010^{\circ} C$

Find the vessel's position and the error of the compass.

4. At 1000 hrs, the Runnel Stone buoy was observed in transit with Longships lighthouse bearing  $318^{\circ} C$ . At the same time Wolf Rock bore  $251^{\circ} C$ . Find the vessel's position. If the course is now set  $095^{\circ} C$  and 20 minutes later Tater Du Lt. bore  $321^{\circ} C$  and St Michael's Mount bore  $014^{\circ} C$ , estimate the set and the drift of the tide if the distance run by log in the interval was 5 miles.

5. Find the times and heights of high and low waters at Sharpness Dock on 14th January.

**Paper 4**

1. From the following information find the direction of the position line and a position through which it passes:

Time at ship 0825 20th September  
 DR position  $5^{\circ} 58' S$   $126^{\circ} 03' E$   
 Sextant altitude Saturn  $50^{\circ} 39.2'$   
 Index error  $1.5'$  off the arc  
 Ht of eye 14.5 metres  
 Chronometer 00h 27m 38s (correct on UT)

2. Find the GMT and LMT of meridian passage of the star Vega and the setting to put on a sextant to observe this passage:

Date at ship 19th September  
 DR position  $13^{\circ} 00' S$   $138^{\circ} 55' E$   
 Index error  $1.8'$  Off the arc  
 Height of eye 17.0 metres

3. Find by Mercator sailing the course and distance from  $48^{\circ} 11' S$   $169^{\circ} 50' E$  to  $23^{\circ} 36' S$   $161^{\circ} 42' W$ .

4. From the following information find the compass error and the deviation for the ship's head:

Time at ship 1004 18th December  
 DR position  $55^{\circ} 08' N$   $5^{\circ} 13' E$   
 Sun bore  $162^{\circ}$  by compass  
 Chronometer 10h 02m 17s  
 Chronometer error 1m 40s fast on UT  
 Variation  $7^{\circ} W$

**Paper 5**

1. From the following information find the direction of the position line and a position through which it passes:

Time at ship 1930 28th June  
 DR position  $33^{\circ} 05' N$   $131^{\circ} 18' W$   
 Sextant altitude Regulus  $34^{\circ} 54.4'$   
 Index error  $1.0'$  on the arc  
 Ht of eye 16.7 metres  
 Chronometer 04h 12m 13s  
 Chronometer error 1m 03s fast on UT

2. From the following information find the direction of the position line and a position through which it passes:

Time at ship 1210 7th January  
 DR position  $26^{\circ} 17' N$   $48^{\circ} 11' W$   
 Sextant altitude Sun LL  $41^{\circ} 16.9'$   
 Index error  $2.0'$  on the arc  
 Ht of eye 13.2 metres

Chronometer 03h 18m 06s  
Chronometer error 7m 14s fast on UT

3. From the following observation of Polaris during evening twilight find the direction of the position line and a position through which it passes:

Date at ship 27th June  
DR position  $21^{\circ} 03' N 153^{\circ} 16' W$   
Sextant altitude  $20^{\circ} 15'$   
Index error  $2.0'$  on the arc  
Height of eye 11.5 metres  
Chronometer 05h 27m 42s  
Chronometer error 1m 29s slow on UT

4. From the following sights find the position of the ship at the time of the second observation:

Assumed position  $40^{\circ} 12' S 94^{\circ} 30' E$   
Observed longitude  $94^{\circ} 33' E$   
Bearing  $079^{\circ} T$   
Run 3.5 hours at 16 knots  
Course  $352^{\circ} T$   
Current  $260^{\circ} T 2$  knots  
Using assumed position run up intercept  $3.0'$  Towards bearing  $012^{\circ} T$

#### Paper 6

1. From the following information find the direction of the position line and a position through which it passes:

Time at ship 1429 29th September  
DR position  $47^{\circ} 30' N 45^{\circ} 20' W$   
Sextant altitude Sun LL  $29^{\circ} 14.3'$   
Index error  $2.0'$  on the arc  
Ht of eye 6.2 metres  
Chronometer 05h 29m 13s  
Chronometer error 1m 03s fast on UT

2. From the following meridian observation find the latitude and state the direction of the position line:

Date at ship 9th January  
DR position  $51^{\circ} 28' S 136^{\circ} 30' E$   
Sextant altitude Moon's LL  $40^{\circ} 15.7'$   
Index error nil  
Height of eye 16.3 metres

3. Find by Mercator sailing the arrival position:

Initial position  $46^{\circ} 45' N 45^{\circ} 00' W$   
Course  $337^{\circ} T$  distance 245 miles

4. From the following information find the error of the compass and the deviation for the ship's head:

Date at ship 29th September  
DR position  $10^{\circ} 50' N 157^{\circ} 17' W$   
Sun bore  $273^{\circ}$  by compass when setting  
Variation  $4^{\circ} E$

#### Paper 7

1. From the following information find the direction of the position line and a position through which it passes:

Time at ship 1407 9th January  
DR position  $12^{\circ} 10' N 50^{\circ} 05' W$   
Sextant altitude Moon UL  $37^{\circ} 46.1'$   
Index error  $1.0'$  on the arc  
Ht of eye 6.2 metres  
Chronometer 17h 25m 01s  
Chronometer error 0m 48s slow on UT

2. From the following information find the direction of the position line and a position through which it passes:

Time at ship 0508 20th September  
DR position  $38^{\circ} 40' S 138^{\circ} 46' E$   
Sextant altitude Bellatrix  $44^{\circ} 50.0'$   
Index error  $3.0'$  off the arc  
Ht of eye 9.9 metres  
Chronometer 08h 12m 19s  
Chronometer error 2m 18s fast on UT

3. From the following meridian observation find the latitude and state the direction of the position line:

Date at ship 20th September  
DR position  $26^{\circ} 00' N 116^{\circ} 30' W$   
Sextant altitude Sun LL  $64^{\circ} 45.0'$   
Index error  $1.5'$  on the arc  
Height of eye 17.9 metres

4. From the following sights find the position of the ship at the time of the second observation:



Time 1300  
 Assumed position  $23^{\circ} 57' N 92^{\circ} 07' W$   
 Intercept  $3.0'$  Towards Brg  $287^{\circ} T$   
 Run 95 miles  
 Course  $147^{\circ} T$   
 Time 1830  
 Using assumed position run up intercept  $5.0$  Away bearing  
 $030^{\circ} T$

### Paper 8

1. From the following information find the direction of the position line and the longitude in which it cuts the DR latitude:

Time at ship 0840 29th September  
 DR position  $30^{\circ} 40' N 175^{\circ} 18' E$   
 Sextant altitude Sun LL  $34^{\circ} 35.0'$   
 Index error  $1.0'$  off the arc  
 Ht of eye 10.3 metres  
 Chronometer 09h 01m 13s  
 Chronometer error nil

2. From the following meridian observation find the latitude and state the direction of the position line:

Date at ship 6th January  
 DR longitude  $96^{\circ} 35' E$   
 Sextant altitude Sun UL bearing south  $41^{\circ} 25.0'$   
 Index error  $2.0'$  on the arc  
 Height of eye 11.5 metres

3. From the following observation of Polaris during morning twilight find the direction of the position line and a position through which it passes:

Date at ship 27th June  
 DR position  $47^{\circ} 15' N 125^{\circ} 40' W$   
 Sextant altitude  $47^{\circ} 52'$   
 Index error  $0.5'$  off the arc  
 Height of eye 6.1 metres  
 Chronometer 11h 01m 44s  
 Chronometer error nil

4. From the following sights worked using the DR position given, find the ship's position at 1746:

Course  $071^{\circ} T$  speed 20 knots  
 DR position  $42^{\circ} 11' S 161^{\circ} 17' E$

Time 1731  
 Time 1737  
 Time 1746

Intercept  $5.8'$  Towards bearing  $026^{\circ} T$   
 Intercept  $2.9'$  Away bearing  $272^{\circ} T$   
 Intercept  $1.7'$  Towards bearing  $319^{\circ} T$

## ANSWERS TO EXERCISES

### Exercise 1.1.1

- |            |         |             |         |
|------------|---------|-------------|---------|
| 1. 425' N  | 709' W  | 2. 910' N   | 635' E  |
| 3. 930' S  | 741' W  | 4. 2026' N  | 522' E  |
| 5. 741' N  | 1278' W | 6. 1005' S  | 300' E  |
| 7. 995' N  | 3712' W | 8. 2910' N  | 4425' E |
| 9. 1508' N | 8226' W | 10. 2983' N | 3516' E |

### Exercise 1.1.2

- |                |              |                |              |
|----------------|--------------|----------------|--------------|
| 1. 12° 24.0' N | 165° 34.0' W | 2. 43° 37.0' N | 17° 46.0' E  |
| 3. 42° 08.2' N | 34° 14.4' W  | 4. 17° 45.1' S | 170° 59.5' E |

### Exercise 1.3.1

- |          |          |         |         |          |
|----------|----------|---------|---------|----------|
| 1. 1° E  | 2. 14° E | 3. 5° E | 4. 1° W | 5. 17° W |
| 6. 12° E | 7. 2° W  | 8. 1° W |         |          |

### Exercise 1.3.2

- |             |           |             |             |             |
|-------------|-----------|-------------|-------------|-------------|
| 1. 217.5° T | 2. 004° T | 3. 004° T   | 4. 264.5° T | 5. 042.5° T |
| 6. 333° T   | 7. 353° T | 8. 093.5° T |             |             |

### Exercise 1.3.3

- |             |           |             |           |             |
|-------------|-----------|-------------|-----------|-------------|
| 1. 240° C   | 2. 008° C | 3. 355.5° C | 4. 260° C | 5. 033.5° C |
| 6. 325.5° C | 7. 079° C | 8. 246.5° C |           |             |

### Exercise 1.3.4

- |             |             |             |           |           |
|-------------|-------------|-------------|-----------|-----------|
| 1. 351.5° T | 2. 347.5° T | 3. 160.5° T | 4. 253° T | 5. 234° T |
| 6. 059° T   | 7. 085° T   | 8. 200° T   |           |           |

### Exercise 1.4.1

- |         |         |         |         |          |
|---------|---------|---------|---------|----------|
| 1. 057° | 2. 125° | 3. 247° | 4. 322° | 5. 113°  |
| 6. 091° | 7. 000° | 8. 194° | 9. 240° | 10. 269° |

### Exercise 1.4.2

- |           |            |           |            |           |           |
|-----------|------------|-----------|------------|-----------|-----------|
| 1. 152° T | 19.6 knots | 2. 296° T | 13.3 knots | 3. 292° T | 2.8 knots |
| 4. 343° T |            | 5. 177° T | 14.3 knots |           |           |

### Exercise 1.5.1

- |   |                           |
|---|---------------------------|
| 1. 9.7 miles                            | 2. 7.05 miles             |
| 3. Compass error 3° E. Bearing 057° T   | 4. 49° 54.2' N 5° 46.7' W |
| 5. 49° 57.0' N 5° 45.5' W               | 6. 49° 50.0' N 5° 43.8' W |
| 7. 49° 58.5' N 7° 35.7' W. PL 035°/215° |                           |

### Exercise 1.6.1

- |                               |                           |
|-------------------------------|---------------------------|
| 1. 41° 24.6' N or S           | 2. 70° 31.7' N or S       |
| 3. 9° 22'                     | 4. 348.5 miles            |
| 5. 57° 24.6' N or 59° 04.6' S | 6. 31° 42' N 23° 07.8' W  |
| 7. 50° 20.1' N or S           | 8. 6° 15.1'               |
| 9. 48° 11.3' N or S           | 10. 39° 00' N 50° 19.4' W |

### Exercise 1.6.2

- |                            |                |
|----------------------------|----------------|
| 1. 11° 08.9'               | 2. 49.8 miles  |
| 3. 51° 19.1' N 28° 57.2' N | 4. 574.5 knots |
| 5. 6° 02.2'                | 6. 594.9 miles |
| 7. 20m 23.6s               |                |

### Exercise 1.6.3

- |  |                             |
|--|-----------------------------|
| 1. Course N 63.9' W distance 259 miles       | 2. 39° 31.5' N 166° 11.3' W |
| 3. Course S 59° 465' E distance 2620.2 miles | 4. 35° 04.7' S 176° 04.5' W |

### Exercise 1.6.4

- |   |           |           |           |
|---|-----------|-----------|-----------|
| 1. a. 848.9                                 | b. 1862.0 | c. 2244.1 | d. 3962.7 |
| 2. Course S 30.3° W distance 2212.0 miles   |           |           |           |
| 3. Course S 14.2° W distance 1851.2 miles   |           |           |           |
| 4. Course S 60.6° E distance 6000.0 miles   |           |           |           |
| 5. 18° 40.5' N 155° 30.7' E                 |           |           |           |
| 6. 11° 24.3' N distance 1355.5 miles        |           |           |           |
| 7. 28° 51.4' S 00° 35.5' E                  |           |           |           |
| 8. 33° 13.8' N 150° 07.2' W                 |           |           |           |
| 9. Course S 47° 28' E distance 2633.1 miles |           |           |           |
| 10. 894.5 miles                             |           |           |           |

### Exercise 1.6.5

- |  |             |        |                      |
|--|-------------|--------|----------------------|
| 1. Initial course S 50° 39.5' E distance 5038.6 miles  |             |        |                      |
| positions  | 45° 10.7' S | 90° W  | course S 55.9° E     |
|  | 51° 52.4' S | 110° W | S 71.0° E            |
|  | 54° 14.1' S | 130° W | N 87.0° E            |
|  | 53° 09.9' S | 150° W | N 76.8° E            |
|  | 48° 15.5' S | 170° W | N 61.2° E            |
| 2. Distance 4638.8 miles. Initial course S 33° 29.7' W. Position of Vertex 68° 33.0' N 58° 28.0' E |             |        |                      |
| 3. Initial course N 77° 37.7' W. Final course S 33° 29.7' W. Distance 1732.3 miles                 |             |        |                      |
| 4. Initial course S 67° 30.3' E. Vertex 40° 44.8' S 20° 17' W. Distance 3599 miles                 |             |        |                      |
| 5. Great circle distance 5190.4. Mercator distance 5594.1. Saving 403.7 miles                      |             |        |                      |
| 6. Initial course N 61° 50.5' W. Vertex 54° 10.4' N 160° 19.7' W. Distance 4076.7 miles            |             |        |                      |
| positions  | 52° 24.4' N | 140° W | course N 73° 38.4' W |
|  | 54° 10.3' N | 160° W | N 89° 44.0' W        |
|  | 52° 31.4' N | 180°   | S 74° 09.7' W        |
|  | 46° 50.1' N | 160° E | S 58° 49.7' W        |



**Exercise 1.6.6**

1. Initial course S 54° 46.3' E. Distance 5484.6 miles. Vertices 70° 54.9' E and 116° 05.2' E
2. Initial course S 73° 56.6' E. Distance 3613.4 miles
3. Initial course S 52° 00.4' E. Distance 5279.6 miles
4. Initial course S 69° 23.8' W. Distance 4804.0 miles
5. Distance 6630.6. Course at equator S 48° E

**Exercise 1.6.7 (Numerical answers only are given)**

1. 090° or 270°
2. Vertices 42° N 40° E and 42° S 140° W Conv. 42°
4. GC Dist 3539.8m Dep 3856.7m Difference 316.9
5. Approx 085°

**Exercise 1.7.1**

1. LW 0135 1.2 metres, HW 0709 13.7 metres, LW 1407 0.9 metres, HW 1938 13.8 metres
2. HW 2122 14.1 metres, interval -0407, 3.05 metres
3. HW 0837 14.1 metres, interval +0247, 4.2 metres
4. 9.9 metres will not dry
5. Ht of tide 6.0 metres, interval -0330, 0822 hrs
6. Ht of tide 9.0 metres, interval -0132, 1434 hrs
7. Interval +0241 Ht of tide 8.0 metres, 53.2 metres above water

**Exercise 1.7.2**

1. LW 0447 0.6 metres, HW 0810 9.5 metres, LW 1715 0.6 metres, HW 2037 9.5 metres
2. HW 1931 8.2 metres, 10.7 metres
3. HW 0624 12.2 metres, LW 1231 0.4 metres, interval +0406, 2.0 metres
4. HW 0914 12.8 metres, LW 1523 0.6 metres, interval +0246, 8.3 metres
5. Ht of tide 8.0 metres, HW 1108 10.8 metres, LW 0521 1.8 metres, interval -0220, 0848 hrs
6. Ht of tide 5.5 metres, HW 2001 11.2 metres, LW 0152 1.4 metres, interval +0320, 2321 hrs
7. HW 0823 11.3 metres, LW 1609 1.2 metres, interval +0637, 1.2 metres

**Exercise 2.1.1**

1. GHA 333° 28.2' Declination 22° 23.8' S
2. GHA 49° 02.2' Declination 1° 29.0' N
3. GHA 350° 23.0' Declination 23° 24.5' S
4. GHA 81° 20.3' Declination 23° 16.5' N
5. GHA 246° 23.6' Declination 2° 37.2' S

**Exercise 2.1.2**

1. GHA 144° 13.9' Declination 8° 30.0' S
2. GHA 30° 37.1' Declination 26° 43.3' N
3. GHA 335° 49.3' Declination 9° 34.4' S
4. GHA 341° 54.5' Declination 0° 44.0' S
5. GHA 346° 20.4' Declination 16° 17.8' S
6. GHA 271° 57.0' Declination 16° 45.6' N

**Exercise 2.1.3**

- |                   |                   |                   |
|-------------------|-------------------|-------------------|
| 1. LHA 72° 20.2'  | 2. LHA 68° 59.6'  | 3. LHA 267° 05.4' |
| 4. LHA 342° 14.7' | 5. LHA 143° 07.3' | 6. LHA 294° 22.9' |
| 7. LHA 199° 59.2' | 8. LHA 63° 39.6'  |                   |

**Exercise 2.3.1**

- |                   |                   |                  |               |             |
|-------------------|-------------------|------------------|---------------|-------------|
| 1. LHA 305° 26.1' | Angle P 54° 33.9' | T. Brg S 65.3° E | Error 9.3° W  | Dev 3.3° W  |
| 2. LHA 25° 09.5'  | Angle P 25° 09.5' | T. Brg N 46.7° W | Error 2.3° E  | Dev 5.3° E  |
| 3. LHA 319° 24.0' | Angle P 40° 36.0' | T. Brg S 37.3° E | Error 15.3° W | Dev 19.3° W |
| 4. LHA 302° 54.2' | Angle P 57° 05.8' | T. Brg N 51.2° E | Error 7.8° W  | Dev 5.8° W  |
| 5. LHA 51° 35.0'  | Angle P 51° 35.0' | T. Brg S 77.2° W | Error 5.3° W  |             |

**Exercise 2.3.2**

- |                   |                    |                  |               |             |
|-------------------|--------------------|------------------|---------------|-------------|
| 1. LHA 69° 32.4'  | Angle P 69° 32.4'  | T. Brg S 69.4° W | Error 19.4° E | Dev 23.4° E |
| 2. LHA 51° 23.7'  | Angle P 51° 23.7'  | T. Brg S 74.8° W | Error 7.8° E  | Dev 1.3° E  |
| 3. LHA 332° 14.5' | Angle P 27° 45.5'  | T. Brg S 42.1° E | Error 2.9° E  | Dev 3.9° E  |
| 4. LHA 66° 02.0'  | Angle P 66° 02'    | T. Brg N 50.6° W | Error 6.6° W  | Dev 0.4° E  |
| 5. LHA 105° 44.9' | Angle P 105° 44.9' | T. Brg S 33.9° W | Error 6.1° W  | Dev 2.1° W  |

**Exercise 2.3.3**

1. Amplitude E 3° 00.4' S. Compass error 4° E
2. Amplitude E 2° 12.3' N. Compass error 2.8° E. Deviation 2.2° W
3. Amplitude W 31.3° N. Compass error 0.3° E. Deviation 6.3° E
4. Amplitude E 30.5° S. Compass error 5.5° W
5. Amplitude W 35.9° S. Compass error 0.9° High
6. Amplitude E 32.4° N. Compass error 2.4° High

**Exercise 2.4.1**

- |                            |                            |                            |
|----------------------------|----------------------------|----------------------------|
| 1. True altitude 52° 39.6' | 2. True altitude 33° 20.1' | 3. True altitude 71° 33.2' |
| 4. True altitude 27° 24.1' | 5. True altitude 62° 47.1' | 6. True altitude 55° 33.6' |

**Exercise 2.4.2**

- |                             |                            |                            |
|-----------------------------|----------------------------|----------------------------|
| 1. True altitude 47° 21.8'  | 2. True altitude 32° 17.0' | 3. True altitude 21° 05.5' |
| 4. True altitude 47° 06.6'  | 5. True altitude 37° 02.3' | 6. True altitude 12° 08.0' |
| 7. True altitude 53° 14.0'  | 8. True altitude 23° 08.1' | 9. True altitude 51° 47.5' |
| 10. True altitude 14° 26.2' |                            |                            |

**Exercise 2.4.3**

- |                            |                            |                            |
|----------------------------|----------------------------|----------------------------|
| 1. True altitude 63° 52.0' | 2. True altitude 35° 10.9' | 3. True altitude 58° 23.3' |
| 4. True altitude 77° 43.0' | 5. True altitude 22° 32.5' | 6. True altitude 39° 15.0' |
| 7. True altitude 51° 27.6' | 8. True altitude 44° 08.0' |                            |

**Exercise 2.4.4**

- |                            |                            |                            |
|----------------------------|----------------------------|----------------------------|
| 1. True altitude 52° 39.4' | 2. True altitude 33° 20.2' | 3. True altitude 71° 33.3' |
| 4. True altitude 27° 24.2' | 5. True altitude 62° 46.9' | 6. True altitude 55° 33.5' |

**Exercise 2.4.5**

1. True altitude 47° 21.8'
2. True altitude 32° 17.1'
3. True altitude 21° 05.5'
4. True altitude 47° 06.6'
5. True altitude 37° 02.2'
6. True altitude 12° 08.0'
7. True altitude 53° 14.2'
8. True altitude 23° 08.1'
9. True altitude 51° 47.6'
10. True altitude 14° 26.3'

**Exercise 2.4.6**

1. True altitude 63° 52.0'
2. True altitude 35° 10.8'
3. True altitude 58° 22.9'
4. True altitude 77° 42.5'
5. True altitude 22° 32.6'
6. True altitude 39° 15.6'
7. True altitude 51° 27.1'
8. True altitude 44° 07.9'

**Exercise 2.5.1**

- |                 |              |                 |              |
|-----------------|--------------|-----------------|--------------|
| 1. 46° 55.2' N  | 6° 45.6' W   | 2. 36° 10.1' S  | 122° 33.6' E |
| 3. 9° 27.3' N   | 177° 47.5' E | 4. 52° 11.7' N  | 164° 15.2' W |
| 5. 34° 14.6' N  | 40° 28.3' W  | 6. 10° 14.9' S  | 25° 46.2' W  |
| 7. 15° 13.8' S  | 159° 17.5' W | 8. 36° 48.6' N  | 147° 08.1' E |
| 9. 23° 45.3' N  | 51° 57.4' W  | 10. 7° 00.6' S  | 41° 55.0' W  |
| 11. 41° 23.4' S | 114° 36.0' E | 12. 19° 34.7' N | 161° 10.8' W |
| 13. 52° 37.5' N | 135° 56.8' W | 14. 52° 12.6' N | 164° 33.5' W |
| 15. 50° 21.8' N | 23° 45.4' W  | 16. 5° 55.8' N  | 88° 52.9' E  |
| 17. 30° 30.0' N | 46° 13.6' W  | 18. 32° 06.2' S | 115° 27.3' E |

**Exercise 2.6.1**

1. TZX 18° 42.8' Latitude 35° 13.9' N
2. TZX 62° 03.1' Latitude 0° 19.5' S
3. TZX 61° 52.7' Latitude 49° 55.5' S
4. TZX 18° 44.6' Latitude 26° 56.2' S
5. TZX 56° 02.2' Latitude 0° 05.4' S

**Exercise 2.6.2**

1. TZX 23° 41.4' Latitude 0° 17.6' N
2. TZX 48° 20.8' Latitude 25° 04.3' S
3. TZX 28° 59.0' Latitude 51° 27.7' S
4. TZX 39° 38.0' Latitude 37° 04.1' N
5. TZX 53° 12.4' Latitude 51° 31.1' S

**Exercise 2.6.3**

1. Decl. 20° 13.8' S T. Alt. 41° 11.8' Latitude 28° 34.4' N
2. Decl. 26° 52.1' N T. Alt. 30° 54.3' Latitude 32° 13.6' S
3. Decl. 7° 40.9' S T. Alt. 70° 28.1' Latitude 27° 12.8' S
4. Decl. 23° 21.4' S T. Alt. 68° 51.5' Latitude 2° 12.9' S

**Exercise 2.6.4**

1. True altitude 22° 08.6' Latitude 50° 25.0' N
2. True altitude 12° 14.9' Latitude 52° 57.5' N
3. True altitude 21° 40.0' Latitude 55° 06.6' N
4. True altitude 19° 24.3' Latitude 49° 53.4' S
5. True altitude 12° 48.6' Latitude 45° 35.7' S

**Exercise 2.7.1**

1. LHA 314° 14.9' Angle P 45° 45.1' Decl. 23° 19.2' N T. Alt. 21° 17.8' CZX 68° 43.8' Int. 1.6 T. Brg. N 44.9° E ITP 29° 28.9' S 121° 18.7' W P/L 134.9°/314.9°

2. LHA 45° 24.6' Angle P 45° 24.6' Decl. 22° 13.4' S T. Alt. 48° 36.8' CZX 41° 17.1' Int. 6.1 A. Brg. N 87.7° W ITP 32° 15.2' S 48° 08.8' W P/L 002.3°/182.3°
3. LHA 57° 58.5' Angle P 57° 58.5' Decl. 1° 18.1' N T. Alt. 31° 55.8' CZX 57° 59.1' Int. 5.1 A. Brg. N 88.5° W ITP 00° 00.1' S 160° 49.9' W P/L 001.5°/181.5°
4. LHA 312° 21.9' Angle P 47° 38.1' Decl. 23° 23.0' S T. Alt. 10° 30.6' CZX 79° 40.6' Int. 11.2 T. Brg. S 43.6° E ITP 43° 03.9' N 38° 14.4' W P/L 046.4°/226.4°
5. LHA 296° 17.3' Angle P 63° 42.7' Decl. 2° 42.2' S T. Alt. 16° 32.9' CZX 73° 26.5' Int. 0.6 A. Brg. S 69.1° E ITP 44° 05.2' N 27° 41.8' W P/L 020.9°/200.9°

**Exercise 2.7.2**

1. LHA 54° 00.3' Angle P 54° 00.3' Decl. 19° 10.0' N T. Alt. 39° 59.6' CZX 50° 06.6' Int. 6.2 T. Brg. N 84.9° W ITP 24° 30.6' N 145° 03.2' E P/L 005.1°/185.1°
2. LHA 77° 00.8' Angle P 77° 00.8' Decl. 56° 33.5' N T. Alt. 41° 47.1' CZX 48° 40.0' Int. 27.1 T. Brg. N 45.7° W ITP 43° 23.9' N 177° 42.6' W P/L 224.3°/044.3°
3. LHA 292° 12.5' Angle P 67° 47.5' Decl. 8° 40.2' S T. Alt. 17° 55.4' CZX 71° 59.1' Int. 5.5 A. Brg. S 74.3° E ITP 17° 55.1' N 47° 35.6' W P/L 015.7°/195.7°
4. LHA 303° 25.0' Angle P 56° 35.0' Decl. 26° 42.0' N T. Alt. 41° 36.9' CZX 48° 13.1' Int. 10.0 A. Brg. S 89.8° E ITP 42° 40.0' N 172° 23.6' W P/L 000.2°/180.2°
5. LHA 65° 15.7' Angle P 65° 15.7' Decl. 5° 13.1' N T. Alt. 14° 54.8' CZX 75° 13.9' Int. 8.7 T. Brg. N 69.3° W ITP 40° 56.4' S 57° 07.8' W P/L 200.7°/020.7°

**Exercise 2.7.3**

1. LHA 292° 34.2' Angle P 67° 25.8' Decl. 24° 59.2' N T. Alt. 32° 48.1' CZX 57° 09.6' Int. 2.3 A. Brg. N 85° E ITP 42° 49.8' N 41° 33.1' W P/L 355°/175°
2. LHA 340° 17.2' Angle P 19° 42.8' Decl. 2° 54.8' S T. Alt. 55° 38.3' CZX 34° 14.2' Int. 7.5 A. Brg. S 36.8° E ITP 25° 36.0' N 174° 55.0' E P/L 053°/233°

**Exercise 2.7.4**

1. GHA 348° 04.1' TZX 58° 20.8' LHA 59° 53.0' Longitude 71° 48.9' E Brg N 69° W PL 201°/011°
2. GHA 61° 58.0' TZX 65° 50.3' LHA 295° 03.9' Longitude 126° 54.1' W Brg S 82.9° E PL 007°/187°
3. GHA 136° 11.6' TZX 46° 42.2' LHA 307° 31.3' Longitude 171° 19.7' E Brg N 90° E PL 000°/180°
4. GHA 302° 42.6' TZX 59° 59.8' LHA 302° 35.3' Longitude 0° 07.3' W Brg S 63.8° E PL 026.2°/206.2°
5. GHA 320° 13.3' TZX 70° 56.0' LHA 300° 03.7' Longitude 20° 09.6' W Brg S 66.2° E PL 023.8°/203.8°

**Exercise 2.7.5**

1. GHA 113° 42.7' TZX 57° 33.3' LHA 314° 27.7' Forenoon longitude 157° 15.0' W Brg N 54.6° E PL 144.6°/324.6°. Noon DR 45° 54.5' S 158° 11.2'. Longitude correction 0.2' E. Noon position 45° 54.7' S 158° 11.0' W
2. GHA 150° 33.6' TZX 72° 34.9' LHA 319° 00.0' Forenoon longitude 168° 26.4' W Brg N 39.1° E PL 129.1°/309.1°. Noon DR 37° 46.7' S 169° 02.3'. Longitude correction 11.3' E. Noon position 37° 53.9' S 169° 13.6' E



**Exercise 2.8.1**

1. LHA  $\Upsilon$  2° 55.9' Position 49° 29.1' N 36° 20.4' W PL 090.6°/270.6°
2. LHA  $\Upsilon$  281° 50.8' Position 35° 27.6' N 36° 25' W PL 090.9°/270.9°
3. LHA  $\Upsilon$  318° 15.7' Position 47° 31.1' N 158° 40' W PL 091.1°/271.1°
4. LHA  $\Upsilon$  84° 07.7' Position 50° 34.1' N 162° 10.8' W PL 089.2°/269.2°

**Paper 1**

1. 281° C, 1h 42m
2. 49° 53.7' N 5° 05.7' W
3. 1° 27'
4. Second position 49° 54.6' N 5° 20.4' W, tide 330° 1.7 knots
5. 47° 03.5' N 10° 14.3' W
6. Course N 28½° W, distance 131.0 miles
7. Compass error 1.5° W, deviation 6.5° E

**Paper 2**

1. 282½°
2. 50° 16.3' N 4° 44.6' W, 094½° C
3. Tide 221° 1.5 knots, course and speed made good 315° 11.8 knots
4. 20.65 miles
5. 55° 17.9' N 3° 56.1' E
6. Compass error 7½° W, deviation 1½° W

**Paper 3**

1. 49° 58.5' N 5° 44.0' W
2. Course and distance 121° T 16.2 miles. 134½°. Steaming time 1h 58m
3. 50° 07.1' N 5° 00.5' W, 20° W
4. 49° 59.6' N 5° 37.9' W, tide 349° 2.1 knots
5. LW 0500 0.6m, HW 0824 8.7m, LW 1720 0.6m, HW 2046 8.5m

**Paper 4**

1. LHA 28° 24.2', CZX 39° 33.0', TZX 39° 26.8', intercept 6.2' towards, brg N 43.8° W ITP 5° 53.5' S 125° 58.7' E 226.2°/046.2°
2. UT 0929, LMT 1841 19th. 38° 19.3'
3. Course N 42° 50.3' E, distance 2011.5 miles
4. LHA 336° 16.7' Error 4° W, Deviation 3° E

**Paper 5**

1. LHA 56° 11.7', CZX 55° 18.7', TZX 55° 15.2', intercept 3.5' towards, brg 261½° ITP 33° 04.5' N 131° 22.1' W, PL 171½°/351½°
2. LHA 357° 58.9', CZX 48° 41.5', TZX 48° 36.3', intercept 5.2' towards, brg 177½°, ITP 26° 11.8' N 48° 10.7' W, PL 267½°/087½°
3. LHA  $\Upsilon$  204° 56.0', latitude 20° 46.8' N, PL 269.8°/089.8°
4. 39° 15.1' S 94° 13.2' E

**Paper 6**

1. LHA 39° 07.0', CZX 60° 30.8', TZX 60° 37.8', intercept 7.0' away, brg S 46.4° W ITP 47° 34.8' N 45° 12.5' W, PL 136½°/316½°
2. Declination 1° 59.7' S, latitude 51° 25.7' N
3. 50° 30.5' N 47° 24.5' W
4. Declination 2° 38.0' S, error 6° W, deviation 10° W

**Paper 7**

1. LHA 309° 13.6', CZX 51° 48.9', TZX 51° 52.4', intercept 3.5' away, brg 099.8°, ITP 12° 10.6' N 50° 08.5' W, PL 189.8°/009.8°
2. LHA 358° 15.5', CZX 45° 03.1', TZX 45° 13.5', intercept 10.4' away, brg N 2½° E ITP 38° 50.4' S 138° 45.4' E, PL 272½°/092½°
3. Declination 1° 01.4' N, latitude 26° 09.8' N, PL 090°/270°
4. 22° 33.9' N 91° 15.1' W

**Paper 8**

1. LHA 312° 56.7', CZX 55° 28.3', TZX 55° 15.0', intercept 13.3' towards, brg S 62.6° E, ITP 30° 33.9' N 175° 31.7' E, PL 207½°/027½°
2. Declination 22° 32.5' S, latitude 26° 27.6' N, PL 090°/270°
3. LHA  $\Upsilon$  314° 54.8', latitude 47° 42.7' N, PL 091.1°/271.1°
4. 42° 03.5' S 161° 25.0' E

**Extracts from  
the  
Nautical Almanac 2003**

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A2 ALTITUDE CORRECTION TABLES 10°-90°—SUN, STARS, PLANETS

OCT.—MAR. SUN			APR.—SEPT.			STARS AND PLANETS				DIP			
App. Alt.	Lower Limb	Upper Limb	App. Alt.	Lower Limb	Upper Limb	App. Alt.	Corr <sup>n</sup>	App. Alt.	Additional Corr <sup>n</sup>	Ht. of Eye	Corr <sup>n</sup>	Ht. of Eye	Ht. of Corr <sup>n</sup>
9 34	+10.8	-21.5	9 39	+10.6	-21.2	9 56	-5.3		<b>2003</b>	m		ft.	m
9 45	+10.9	-21.4	9 51	+10.7	-21.1	10 08	-5.2		<b>VENUS</b>	2.4	-2.8	8.0	1.0 - 1.8
9 56	+11.0	-21.3	10 03	+10.8	-21.0	10 20	-5.1		Jan. 1-Feb. 20	2.6	-2.9	8.6	1.5 - 2.2
10 08	+11.1	-21.2	10 15	+10.9	-20.9	10 33	-5.0		0	2.8	-3.0	9.2	2.0 - 2.5
10 21	+11.2	-21.1	10 27	+11.0	-20.8	10 46	-4.9		0	3.0	-3.1	9.8	2.5 - 2.8
10 34	+11.3	-21.0	10 40	+11.1	-20.7	11 00	-4.8		41 +0.2	3.2	-3.2	10.5	3.0 - 3.0
10 47	+11.4	-20.9	10 54	+11.2	-20.6	11 14	-4.7		76 +0.1	3.4	-3.3	11.2	
11 01	+11.5	-20.8	11 08	+11.3	-20.5	11 29	-4.6		Feb. 21-Dec. 31	3.6	-3.4	11.9	See table
11 15	+11.6	-20.7	11 23	+11.4	-20.4	11 45	-4.5		0	3.8	-3.4	12.6	←
11 30	+11.7	-20.6	11 38	+11.5	-20.3	12 01	-4.5		0 +0.1	4.0	-3.6	13.3	m
11 46	+11.8	-20.5	11 54	+11.6	-20.2	12 18	-4.4		60	4.3	-3.6	14.1	20 - 7.9
12 02	+11.9	-20.4	12 10	+11.7	-20.1	12 35	-4.2		<b>MARS</b>	4.5	-3.7	14.9	22 - 8.3
12 19	+12.0	-20.3	12 28	+11.8	-20.0	12 54	-4.2		Jan. 1-May 2	4.7	-3.9	15.7	24 - 8.6
12 37	+12.1	-20.2	12 46	+11.9	-19.9	13 13	-4.0		Dec. 17-Dec. 31	5.0	-3.9	16.5	26 - 9.0
12 55	+12.2	-20.1	13 05	+12.0	-19.8	13 33	-3.9		0	5.2	-4.0	17.4	28 - 9.3
13 14	+12.3	-20.0	13 24	+12.1	-19.7	13 54	-3.8		0 +0.1	5.5	-4.1	18.3	
13 35	+12.4	-19.9	13 45	+12.2	-19.6	14 16	-3.7		60	5.8	-4.2	19.1	30 - 9.6
14 18	+12.5	-19.8	14 07	+12.3	-19.5	14 40	-3.6		May 3-June 26	6.1	-4.3	20.1	32 - 10.0
14 42	+12.6	-19.7	14 30	+12.4	-19.4	15 04	-3.5		Oct. 26-Dec. 16	6.3	-4.4	21.0	34 - 10.3
15 06	+12.7	-19.6	15 19	+12.5	-19.3	15 30	-3.4		0	6.6	-4.5	22.0	36 - 10.6
15 32	+12.8	-19.5	15 46	+12.6	-19.2	15 57	-3.3		41 +0.2	6.9	-4.6	22.9	38 - 10.8
15 59	+12.9	-19.4	16 14	+12.7	-19.1	16 26	-3.2		76 +0.1	7.2	-4.7	23.9	
16 28	+13.0	-19.3	16 44	+12.8	-19.0	16 56	-3.1		June 27-Aug. 1	7.5	-4.9	24.9	40 - 11.1
16 59	+13.1	-19.2	17 15	+13.0	-18.8	17 28	-3.0		Sept. 23-Oct. 25	7.9	-4.9	26.0	42 - 11.4
17 32	+13.2	-19.1	17 48	+13.1	-18.7	18 02	-2.9		0	8.2	-5.0	27.1	44 - 11.7
18 06	+13.3	-19.0	18 24	+13.2	-18.6	18 38	-2.8		34 +0.3	8.5	-5.1	28.1	46 - 11.9
18 42	+13.4	-18.9	19 01	+13.3	-18.5	19 17	-2.7		60 +0.2	8.8	-5.2	29.2	48 - 12.2
19 21	+13.5	-18.8	19 42	+13.4	-18.4	19 58	-2.6		80 +0.1	9.2	-5.3	30.4	ft.
20 03	+13.6	-18.7	20 25	+13.5	-18.3	20 42	-2.5		Aug. 2-Sept. 22	9.5	-5.4	31.5	2 - 1.4
20 48	+13.8	-18.5	21 11	+13.6	-18.2	21 28	-2.4		0	9.9	-5.5	32.7	4 - 1.9
21 35	+13.9	-18.4	22 00	+13.7	-18.1	22 19	-2.3		29 +0.4	10.3	-5.6	33.9	6 - 2.4
22 26	+14.0	-18.3	22 54	+13.8	-18.0	23 13	-2.2		51 +0.3	10.6	-5.7	35.1	8 - 2.7
23 22	+14.1	-18.2	23 51	+13.9	-17.9	24 11	-2.1		68 +0.2	11.0	-5.9	36.3	10 - 3.1
24 21	+14.2	-18.1	24 53	+14.0	-17.8	25 14	-2.0		83 +0.1	11.4	-6.0	37.6	See table
25 26	+14.3	-18.0	26 00	+14.1	-17.7	26 22	-2.0		0	11.8	-6.1	38.9	←
26 36	+14.4	-17.9	27 13	+14.2	-17.6	27 36	-1.9		26 22	12.2	-6.2	40.1	ft.
27 52	+14.5	-17.8	28 33	+14.3	-17.5	28 56	-1.8		27 36	12.6	-6.2	41.5	70 - 8.1
29 15	+14.6	-17.7	30 00	+14.4	-17.4	30 24	-1.7		30 24	13.0	-6.3	42.8	75 - 8.4
30 46	+14.7	-17.6	31 35	+14.5	-17.3	32 00	-1.6		32 00	13.4	-6.4	44.2	80 - 8.7
32 26	+14.8	-17.5	33 20	+14.6	-17.2	33 45	-1.5		33 45	13.8	-6.5	45.5	85 - 8.9
34 17	+14.9	-17.4	35 17	+14.7	-17.1	35 40	-1.4		35 40	14.2	-6.6	46.9	90 - 9.2
36 20	+15.0	-17.3	37 26	+14.8	-17.0	37 48	-1.3		37 48	14.7	-6.7	48.4	95 - 9.5
38 36	+15.1	-17.2	39 50	+14.9	-16.9	40 08	-1.2		40 08	15.1	-6.8	49.8	
41 08	+15.2	-17.1	42 31	+15.0	-16.8	42 44	-1.1		42 44	15.5	-6.9	51.3	100 - 9.7
43 59	+15.3	-17.0	45 31	+15.1	-16.7	45 36	-1.0		45 36	16.0	-7.0	52.8	105 - 9.9
47 10	+15.4	-16.9	48 55	+15.2	-16.6	48 47	-0.9		48 47	16.5	-7.1	54.3	110 - 10.2
50 46	+15.5	-16.8	52 44	+15.3	-16.5	52 18	-0.8		52 18	16.9	-7.2	55.8	115 - 10.4
54 49	+15.6	-16.7	57 02	+15.4	-16.4	56 11	-0.7		56 11	17.4	-7.3	57.4	120 - 10.6
59 23	+15.7	-16.6	61 51	+15.5	-16.3	60 28	-0.6		60 28	17.9	-7.4	58.9	125 - 10.8
64 30	+15.8	-16.5	67 17	+15.6	-16.2	65 08	-0.5		65 08	18.4	-7.5	60.5	
70 12	+15.9	-16.4	73 16	+15.7	-16.1	70 11	-0.4		70 11	18.8	-7.6	62.1	130 - 11.1
76 26	+16.0	-16.3	79 43	+15.8	-16.0	75 34	-0.3		75 34	19.3	-7.7	63.8	135 - 11.3
83 05	+16.1	-16.2	86 32	+15.9	-15.9	81 13	-0.2		81 13	19.8	-7.8	65.4	140 - 11.5
90 00						87 03	-0.1		87 03	20.4	-7.9	67.1	145 - 11.7
						90 00	0.0		90 00	20.9	-8.0	68.8	150 - 11.9
										21.4	-8.1	70.5	155 - 12.1

App. Alt. = Apparent altitude = Sextant altitude corrected for index error and dip.



UT	ARIES			VENUS -4.5			MARS +1.5			JUPITER -2.5			SATURN -0.4			STARS							
	d	h	GHA	GHA	Dec	S15	S17	S30.1	GHA	Dec	N16	N22	N22.2	GHA	Dec	N22	N22.2	Name	SHA	Dec			
																					SHA	Dec	SHA
4 00	103	11.4	228	06.3	S15	53.9	233	55.9	S17	30.1	323	52.3	N16	36.0	19	25.9	N22	02.2	Acamar	315	24.3	S40	17.8
01	118	13.9	243	06.3	54.4	248	56.8	30.5	338	55.0	36.1	34	28.6	02.2	Acchernar	335	32.6	S57	13.7				
02	133	16.4	258	06.3	55.0	263	57.6	30.9	353	57.7	36.2	49	31.2	02.2	Acruz	173	18.7	S63	06.6				
03	148	18.8	273	06.3	55.5	278	58.4	31.4	9	00.4	36.3	64	33.9	02.2	Adhara	255	18.6	S28	58.5				
04	163	21.3	288	06.4	56.0	293	59.3	31.8	24	03.1	36.3	79	36.6	02.2	Aldebaran	290	58.6	N16	30.9				
05	178	23.7	303	06.4	56.6	309	00.1	32.3	39	05.8	36.4	94	39.2	02.2									
06	193	26.2	318	06.4	S15	57.1	324	01.0	S17	32.7	54	08.4	N16	36.5	109	41.9	N22	02.2	Alioth	166	27.7	N55	56.4
07	208	28.7	333	06.4	57.7	339	01.8	33.1	69	11.1	36.6	124	44.6	02.2	Alkaid	153	05.4	N49	17.7				
08	223	31.0	348	06.4	58.2	354	02.6	33.6	84	13.8	36.7	139	47.2	02.2	Al Na'ir	27	54.2	S46	57.1				
09	238	33.6	3	06.5	58.8	9	03.5	34.0	99	16.5	36.7	154	49.9	02.2	Anilam	275	54.4	S	1	12.0			
10	253	36.1	18	06.5	59.3	24	04.3	34.0	114	19.2	36.8	169	52.6	02.2	Alphard	218	03.9	S	8	40.2			
11	268	38.5	33	06.5	59.8	39	05.1	34.9	129	21.9	36.9	184	55.2	02.2									
12	283	41.0	48	06.5	S16	00.4	54	06.0	S17	35.3	144	24.6	N16	37.0	199	57.9	N22	02.2	Alphecca	126	18.2	N26	42.1
13	298	43.5	63	06.5	00.9	69	06.8	35.8	159	27.3	37.1	215	00.6	02.2	Alpheratz	357	52.2	N29	06.5				
14	313	45.9	78	06.5	01.5	84	07.7	36.2	174	30.0	37.1	230	03.2	02.2	Alnilam	62	16.6	N	8	52.5			
15	328	48.4	93	06.5	02.0	99	08.5	36.6	189	32.7	37.2	245	05.9	02.2	Ankaa	353	23.7	S42	17.7				
16	343	50.9	108	06.5	02.5	114	09.3	37.1	204	35.4	37.3	260	08.6	02.2	Antares	112	36.7	S26	26.3				
17	358	53.3	123	06.5	03.1	129	10.2	37.5	219	38.1	37.4	275	11.2	02.2									
18	13	55.8	138	06.5	S16	03.6	144	11.0	S17	37.9	234	40.8	N16	37.5	290	13.9	N22	02.2	Arcturus	146	03.3	N19	09.9
19	28	58.2	153	06.6	04.2	159	11.8	38.4	249	43.5	37.5	305	16.6	02.2	Atria	107	46.5	S69	01.8				
20	44	00.7	168	06.6	04.7	174	12.7	38.8	264	46.2	37.6	320	19.2	02.2	Avior	234	20.9	S59	31.0				
21	59	03.2	183	06.6	05.3	189	13.5	39.2	279	48.9	37.7	335	21.9	02.2	Belatrix	278	40.5	N	6	21.1			
22	74	05.6	198	06.6	05.8	204	14.3	39.7	294	51.6	37.8	350	24.6	02.2	Betelgeuse	271	09.9	N	7	24.5			
23	89	08.1	213	06.6	06.3	219	15.0	40.1	309	54.3	37.9	379	27.2	02.2									
5 00	104	10.6	228	06.6	S16	06.9	234	16.0	S17	40.5	324	57.0	N16	37.9	20	29.9	N22	02.2	Canopus	263	59.3	S52	41.8
01	119	13.0	243	06.6	07.4	249	16.8	41.0	339	59.7	38.0	35	32.6	02.2	Capella	280	46.2	N46	00.2				
02	134	15.5	258	06.6	08.0	264	17.7	41.4	355	02.4	38.1	50	35.2	02.2	Deneb	49	37.6	N45	17.5				
03	149	18.0	273	06.6	08.5	279	18.5	41.8	10	05.1	38.2	65	37.9	02.2	Denebola	182	41.9	N14	33.3				
04	164	20.4	288	06.6	09.0	294	19.3	42.3	25	07.8	38.3	80	40.5	02.2	Diphda	349	04.1	S17	58.4				
05	179	22.9	303	06.6	09.6	309	20.2	42.7	40	10.5	38.3	95	43.2	02.2									
06	194	25.4	318	06.5	S16	10.1	324	21.0	S17	43.1	55	13.2	N16	38.4	110	45.9	N22	02.2	Dubhe	194	01.2	N61	43.9
07	209	27.8	333	06.5	10.7	339	21.8	43.6	70	15.9	38.0	125	48.5	02.2	El Nath	278	42.3	S	67	56.8			
08	224	30.3	348	06.5	11.2	354	22.7	44.0	85	18.6	38.6	140	51.2	02.2	Eltanin	90	50.5	N51	29.2				
09	239	32.7	3	06.5	11.7	9	23.5	44.4	100	21.3	38.7	155	53.9	02.2	Enif	33	55.5	N	9	53.2			
10	254	35.2	18	06.5	12.3	24	24.3	44.9	115	24.0	38.8	170	56.5	02.2	Fomalhaut	15	33.2	S29	36.7				
11	269	37.7	33	06.5	12.8	39	25.2	45.3	130	26.7	38.8	185	59.2	02.2									
12	284	40.1	48	06.5	S16	13.4	54	26.0	S17	45.7	145	29.4	N16	38.9	201	01.9	N22	02.2	Gacrux	172	10.3	S57	07.4
13	299	42.6	63	06.5	13.9	69	26.8	46.1	160	32.1	39.0	216	04.5	02.2	Gienah	176	00.8	S17	33.4				
14	314	45.1	78	06.5	14.4	84	27.7	46.6	175	34.8	39.1	231	07.2	02.2	Hadar	149	00.0	S60	22.9				
15	329	47.5	93	06.4	15.0	99	28.5	47.0	190	37.6	39.2	246	09.9	02.2	Hamal	328	10.0	S23	28.6				
16	344	50.0	108	06.4	15.5	114	29.3	47.4	205	40.3	39.2	261	12.5	02.2	Kaus Aust.	83	55.1	S34	23.0				
17	359	52.5	123	06.4	16.1	129	30.2	47.9	220	43.0	39.3	276	15.2	02.2									
18	14	54.9	138	06.4	S16	16.6	144	31.0	S17	48.3	235	45.7	N16	39.4	291	17.8	N22	02.2	Kochab	137	20.0	N74	08.3
19	29	57.4	153	06.4	17.1	159	31.8	48.7	250	48.4	39.5	306	20.5	02.2	Markab	13	46.7	N15	13.2				
20	44	59.9	168	06.4	17.7	174	32.7	49.2	265	51.1	39.6	321	23.2	02.2	Merikar	314	23.5	N	4	06.0			
21	60	02.3	183	06.3	18.2	189	33.5	49.6	280	53.8	39.6	336	25.8	02.1	Mikant	148	17.5	S36	22.9				
22	75	04.8	198	06.3	18.7	204	34.3	50.0	295	56.5	39.7	351	28.5	02.1	Miaplacidus	221	40.9	S69	43.5				
23	90	07.2	213	06.3	19.3	219	35.2	50.4	310	59.2	39.8	6	31.2	02.1									
6 00	105	09.7	228	06.3	S16	19.8	234	36.0	S17	50.9	326	01.9	N16	39.9	21	33.8	N22	02.1	Mirfak	308	51.9	N49	52.5
01	120	12.2	243	06.2	20.4	249	36.8	51.3	341	04.6	40.0	36	36.5	02.1	Nunki	76	08.9	S26	17.7				
02	135	14.6	258	06.2	20.9	264	37.7	51.7	356	07.3	40.1	51	39.2	02.1	Peacock	53	32.6	S56	43.7				
03	150	17.1	273	06.2	21.4	279	38.5	52.2	11	10.0	40.1	66	41.8	02.1	Pollux	243	37.4	N28	01.1				
04	165	19.6	288	06.2	22.0	294	39.3	52.6	26	12.7	40.2	81	44.5	02.1	Procyon	245	08.0	N	5	13.1			
05	180	22.0	303	06.1	22.5	309	40.2	53.0	41	15.4	40.3	96	47.1	02.1									
06	195	24.5	318	06.1	S16	23.0	324	41.0	S17	53.4	56	18.1	N16	40.4	111	49.8	N22	02.1	Rasalhague	96	14.4	N12	33.4
07	210	27.0	333	06.1	23.6	339	41.8	53.9	71	20.9	40.5	126	52.5	02.1	Regulus	201	52						



UT	ARIES			VENUS -4.5			MARS +1.5			JUPITER -2.5			SATURN -0.4			STARS		
	GHA	GHA	Dec	GHA	Dec	GHA	Dec	GHA	Dec	GHA	Dec	GHA	Dec	Name	SHA	Dec		
700	106 08.8	228 05.4	S16 32.7	234 55.9	S18 01.1	327 06.9	N16 41.9	22 37.7	N22 02.1	315 24.3	S40 17.8	Acamar	315 24.3	S40 17.8	17.8			
01	121 11.3	243 05.3	33.2	249 56.7	01.5	342 09.7	42.0	37 40.4	02.1	335 32.6	S57 13.7	Achernar	335 32.6	S57 13.7	13.7			
02	136 13.8	258 05.3	33.8	264 57.6	01.9	357 12.4	42.1	52 43.0	02.1	173 18.7	S63 06.6	Acruz	173 18.7	S63 06.6	6.6			
03	151 16.2	273 05.2	34.3	279 58.4	02.3	372 15.1	42.1	67 45.7	02.1	255 18.6	S28 58.5	Adhara	255 18.6	S28 58.5	58.5			
04	166 18.7	288 05.2	34.8	284 59.2	02.8	387 17.8	42.2	82 48.4	02.1	290 58.6	N16 30.9	Aldebaran	290 58.6	N16 30.9	30.9			
05	181 21.2	303 05.1	35.4	310 00.1	03.2	402 20.5	42.3	97 51.0	02.1									
06	196 23.6	318 05.1	S16 35.9	325 00.9	S18 03.6	412 23.2	N16 42.4	112 53.7	N22 02.1	166 27.7	N55 56.4	Alioth	166 27.7	N55 56.4	56.4			
07	211 26.1	333 05.0	36.4	340 01.7	04.0	425 25.9	42.5	127 56.3	02.1	153 05.3	N49 17.7	Alkaid	153 05.3	N49 17.7	17.7			
08	226 28.6	348 04.9	37.0	355 02.5	04.5	447 28.6	42.6	142 59.0	02.1	27 54.2	S46 57.1	Al Na'ir	27 54.2	S46 57.1	57.1			
09	241 31.0	3 04.9	37.5	10 03.4	04.9	102 31.4	42.6	158 01.7	02.1	275 54.4	S 1 12.0	Anihim	275 54.4	S 1 12.0	12.0			
10	256 33.5	18 04.8	38.0	25 04.2	05.3	117 34.1	42.7	173 04.3	02.1	218 03.9	S 8 40.2	Alphard	218 03.9	S 8 40.2	40.2			
11	271 36.0	33 04.8	38.6	40 05.0	05.7	132 36.8	42.8	188 07.0	02.1									
12	286 38.4	48 04.7	S16 39.1	55 05.9	S18 06.1	147 39.5	N16 42.9	203 09.6	N22 02.1	126 18.2	N26 42.1	Alphecca	126 18.2	N26 42.1	42.1			
13	301 40.9	63 04.6	39.6	70 06.7	06.6	162 42.2	43.0	218 12.3	02.1	357 52.2	N29 06.5	Alpheratz	357 52.2	N29 06.5	6.5			
14	316 43.3	78 04.6	40.2	85 07.5	07.0	177 44.9	43.1	233 15.0	02.1	62 16.6	N 8 52.5	Alhair	62 16.6	N 8 52.5	52.5			
15	331 45.8	93 04.5	40.7	100 08.3	07.4	192 47.7	43.1	248 17.6	02.1	153 23.8	S42 17.7	Ankaa	153 23.8	S42 17.7	17.7			
16	346 48.3	108 04.5	41.2	115 09.2	07.8	207 50.4	43.2	263 20.3	02.1	352 36.7	S26 26.3	Antares	352 36.7	S26 26.3	26.3			
17	1 50.7	123 04.4	41.8	130 10.0	08.2	222 53.1	43.3	278 22.9	02.1									
18	16 53.2	138 04.3	S16 42.3	145 10.8	S18 08.7	237 55.8	N16 43.4	293 25.6	N22 02.1	146 03.3	N19 09.9	Arcturus	146 03.3	N19 09.9	9.9			
19	31 55.7	153 04.3	42.8	160 11.6	09.1	252 58.5	43.5	308 28.3	02.1	107 46.5	S69 01.0	Atria	107 46.5	S69 01.0	1.0			
20	46 58.1	168 04.2	43.3	175 12.5	09.5	268 01.2	43.6	323 30.9	02.1	234 20.9	S59 31.0	Avior	234 20.9	S59 31.0	31.0			
21	62 00.6	183 04.1	43.9	190 13.3	09.9	283 04.0	43.7	338 33.6	02.1	278 40.5	N 6 21.1	Bellatrix	278 40.5	N 6 21.1	21.1			
22	77 03.1	198 04.0	44.4	205 14.1	10.3	298 06.7	43.7	353 36.2	02.1	271 09.9	N 7 24.5	Betelgeuse	271 09.9	N 7 24.5	24.5			
23	92 05.5	213 04.0	44.9	220 14.9	10.7	313 09.4	43.8	368 39.9	02.1									
800	107 08.0	228 03.9	S16 45.5	235 15.8	S18 11.2	328 12.1	N16 43.9	23 41.5	N22 02.1	263 59.3	S52 41.9	Canopus	263 59.3	S52 41.9	41.9			
01	122 10.4	243 03.8	46.0	250 16.6	11.6	343 14.8	44.0	38 44.2	02.1	280 46.2	N46 00.2	Capella	280 46.2	N46 00.2	0.2			
02	137 12.9	258 03.8	46.5	265 17.4	12.0	358 17.5	44.1	53 46.9	02.1	49 37.6	N45 17.4	Deneb	49 37.6	N45 17.4	17.4			
03	152 15.4	273 03.7	47.1	280 18.2	12.4	373 20.3	44.2	68 49.5	02.1	182 41.9	N14 33.3	Denebola	182 41.9	N14 33.3	33.3			
04	167 17.8	288 03.6	47.6	295 19.1	12.8	388 23.0	44.3	83 52.2	02.1	349 04.1	S17 58.4	Diphda	349 04.1	S17 58.4	58.4			
05	182 20.3	303 03.5	48.1	310 19.9	13.2	403 25.7	44.3	98 54.8	02.1									
06	197 22.8	318 03.5	S16 48.6	325 20.7	S18 13.7	418 28.4	N16 44.4	113 57.5	N22 02.1	194 01.1	N61 43.9	Dubhe	194 01.1	N61 43.9	43.9			
07	212 25.2	333 03.4	49.2	340 21.5	14.1	433 31.1	44.5	129 00.1	02.1	207 01.8	S15 7	El Nath	207 01.8	S15 7	7			
08	227 27.7	348 03.3	49.7	355 22.4	14.5	448 33.9	44.6	144 02.8	02.1	90 50.5	N51 29.2	Eltanin	90 50.5	N51 29.2	29.2			
09	242 30.2	3 03.2	50.2	10 23.2	14.9	103 36.6	44.7	159 05.5	02.1	23 55.5	N 9 53.2	Enif	23 55.5	N 9 53.2	53.2			
10	257 32.6	18 03.1	50.8	25 24.0	15.3	118 39.3	44.8	174 08.1	02.0	15 33.2	S29 36.7	Fomalhaut	15 33.2	S29 36.7	36.7			
11	272 35.1	33 03.0	51.3	40 24.8	15.7	133 42.0	44.9	189 10.8	02.0									
12	287 37.6	48 03.0	S16 51.8	55 25.7	S18 16.1	148 44.8	N16 44.9	204 13.4	N22 02.1	172 10.2	S57 07.5	Garxur	172 10.2	S57 07.5	7.5			
13	302 40.0	63 02.9	52.3	70 26.5	16.6	163 47.5	45.0	219 16.1	02.0	176 00.7	S17 33.4	Gienah	176 00.7	S17 33.4	33.4			
14	317 42.5	78 02.8	52.9	85 27.3	17.0	178 50.2	45.1	234 18.7	02.0	149 00.0	S60 22.9	Hadar	149 00.0	S60 22.9	22.9			
15	332 44.9	93 02.7	53.4	100 28.1	17.4	193 52.9	45.2	249 21.4	02.0	328 10.0	N23 28.6	Hamal	328 10.0	N23 28.6	28.6			
16	347 47.4	108 02.6	53.9	115 29.0	17.8	208 55.6	45.3	264 24.1	02.0	83 55.1	S34 23.0	Kaus Aust.	83 55.1	S34 23.0	23.0			
17	2 49.9	123 02.5	54.4	130 29.8	18.2	223 58.4	45.4	279 26.7	02.0									
18	17 52.3	138 02.4	S16 55.0	145 30.6	S18 18.6	239 01.1	N16 45.5	294 29.4	N22 02.1	137 19.9	N74 08.3	Kochab	137 19.9	N74 08.3	8.3			
19	32 54.8	153 02.3	55.5	160 31.4	19.0	254 03.8	45.5	309 32.0	02.0	13 46.7	N15 13.2	Markab	13 46.7	N15 13.2	13.2			
20	47 57.3	168 02.3	56.0	175 32.3	19.5	269 06.5	45.6	324 34.7	02.0	314 23.5	N 4 06.0	Menkar	314 23.5	N 4 06.0	6.0			
21	62 59.7	183 02.2	56.6	190 33.1	19.9	284 09.3	45.7	339 37.3	02.0	148 17.5	S36 22.9	Menkent	148 17.5	S36 22.9	22.9			
22	78 02.2	198 02.1	57.1	205 33.9	20.3	299 12.0	45.8	354 40.0	02.0	221 40.8	S69 43.5	Miaplacidus	221 40.8	S69 43.5	43.5			
23	93 04.7	213 02.0	57.6	220 34.7	20.7	314 14.7	45.9	369 42.7	02.0									
900	108 07.1	228 01.9	S16 58.1	235 35.5	S18 21.1	329 17.4	N16 46.0	24 45.3	N22 02.1	308 52.0	N49 52.5	Miraf	308 52.0	N49 52.5	52.5			
01	123 09.6	243 01.8	58.2	250 36.4	21.5	344 20.1	46.1	39 48.0	02.0	76 08.9	S26 17.7	Nunki	76 08.9	S26 17.7	17.7			
02	138 12.1	258 01.7	59.2	265 37.2	21.9	359 22.9	46.1	54 50.6	02.0	53 32.6	S56 43.7	Peacock	53 32.6	S56 43.7	43.7			
03	153 14.5	273 01.6	16 59.7	280 38.0	22.3	374 25.6	46.2	69 53.3	02.0	243 37.4	N28 01.1	Pollux	243 37.4	N28 01.1	1.1			
04	168 17.0	288 01.5	17 00.2	295 38.8	22.7	389 28.3	46.3	84 55.9	02.0	245 08.0	N 5 13.1	Procyon	245 08.0	N 5 13.1	13.1			
05	183 19.4	303 01.4	00.7	310 39.7	23.2	404 31.0	46.4	99 58.6	02.0									
06	198 21.9	318 01.3	S17 01.3	325 40.5	S18 23.6	419 33.8	N16 46.5	115 01.2	N22 02.1	96 14.4	N12 33.4	Rasalhague	96 14.4	N12 33.4	33.4			
07	213 24.4	333 01.2	01.8	340 41.3	24.0	434 36.5	46.6	130 03.9	02.0	207 52.0	N11 57.2	Regulus	207 52.0	N11 57.2	57.2			
08	228 26.8	348 01.1	02.3	355 42.1	24.4	449 39.2	46.7	145 06.5	02.0	281 19.7	S 8 11.9	Rigel	281 19.7	S 8 11.9	11.9			
09	243 29.3	3 01.0	02.8	10 42.9	24.8	104 42.0	46.8	160 09.2	02.0	140 03.5	S60 50.5	Rigel Kent.	140 03.5	S60 50.5	50.5			
10	258 31.8	18 00.9	03.4	25 43.8	25.2	119 44.7	46.8	175 11.5	02.0	102 22.3	S15 43.7	Sabik	102 22.3	S15 43.7	43.7			
11	273 34.2	33 00.8	03.9	40 44.6	25.6	134 47.4	46.9	190 14.5	02.0									
12	288 36.7	48 00.7	S17 04.4	55 45.4	S18 26.0	149 50.1	N16 47.0	205 17.2	N22 02.1	349 50.2	N56 33.4	Schedar	349 50.2	N56 33.4	33.4			
13	303 39.2	63 00.5	04.9	70 46.2	26.4	164 52.9	47.1	220 19.8	02.0	96 33.5	S37 06.3	Shaula	96 33.5	S37 06.3	6.3			
14	318 41.6	78 00.4	05.5	85 47.0	26.8	179 55.6	47.2	235 22.5	02.0	258 40.7	S16 43.2	Sirius	258 40.7	S16 43.2	43.2			



UT	ARIES		VENUS -4.0		MARS +0.5		JUPITER -2.3		SATURN +0.1		STARS		
	GHA	Dec	GHA	Dec	GHA	Dec	GHA	Dec	GHA	Dec	Name	SHA	Dec
29 00 01	185 59.1	212 13.4 S11 35.9	259 22.3	S23 07.7	55 12.3	N19 05.0	103 17.7	N22 16.1	103 17.7	N22 16.1	Acamar	315 24.7	S40 17.7
01	201 01.6	227 12.9	34.9	274 23.0	07.6	70 14.8	05.1	118 20.0	16.1	16.1	Achernar	335 33.1	S57 13.4
02	216 04.0	242 12.5	34.0	289 23.8	07.5	85 17.4	05.1	133 22.2	16.1	16.1	Acrux	173 18.0	S63 07.0
03	231 06.5	257 12.1	33.0	304 24.6	07.4	100 19.9	05.1	148 24.6	16.1	16.1	Adhara	255 18.9	S28 58.8
04	246 08.9	272 11.6	32.0	319 25.3	07.2	115 22.4	05.1	163 26.9	16.1	16.1	Aldebaran	290 58.8	N16 30.9
05	261 11.4	287 11.2	31.1	334 26.1	07.1	130 24.9	05.1	178 29.2	16.2	16.2			
06	276 13.9	302 10.8	S11 30.1	349 26.9	S23 07.0	145 27.4	N19 05.1	193 31.5	N22 16.2	16.2	Alioth	166 27.0	N55 56.5
07	291 16.3	317 10.3	29.2	4 27.7	06.9	160 29.9	05.1	208 33.8	16.2	16.2	Alkaid	153 04.6	N49 17.7
08	306 18.8	332 09.9	28.2	19 28.4	06.8	175 32.4	05.1	223 36.1	16.2	16.2	Al Nair	27 54.0	S46 56.8
09	321 21.3	347 09.4	27.2	34 29.2	06.6	190 34.9	05.1	238 38.4	16.2	16.2	Alnilam	275 54.6	S 1 12.1
10	336 23.7	2 09.0	26.3	49 30.0	06.5	205 37.5	05.1	253 40.7	16.3	16.3	Alphard	218 03.8	S 8 40.4
11	351 26.2	17 08.6	25.3	64 30.7	06.4	220 40.0	05.2	268 43.0	16.3	16.3			
12	6 28.7	32 08.1	S11 24.4	79 31.5	S23 06.3	235 42.5	N19 05.2	283 45.3	N22 16.2	16.2	Alphecca	126 17.5	N26 42.0
13	21 31.1	47 07.7	23.4	94 32.3	06.1	250 45.0	05.2	298 47.6	16.3	16.3	Alpheratz	357 52.3	N29 06.3
14	36 33.6	62 07.3	22.4	109 33.0	06.0	265 47.5	05.2	313 49.9	16.3	16.3	Altair	62 16.2	N 8 52.3
15	51 36.0	77 06.8	21.5	124 33.8	05.9	280 50.0	05.2	328 52.2	16.3	16.3	Ankaa	353 23.9	S42 17.5
16	66 38.5	92 06.4	20.5	139 34.6	05.8	295 52.5	05.2	343 54.5	16.3	16.3	Antares	112 36.0	S26 26.4
17	81 41.0	107 06.0	19.5	154 35.3	05.6	310 55.0	05.2	358 56.8	16.4	16.4			
18	96 43.4	122 05.5	S11 18.6	169 36.1	S23 05.5	325 57.5	N19 05.2	383 59.8	N22 16.2	16.2	Arcturus	146 02.7	N19 09.8
19	111 45.9	137 05.1	17.6	184 36.9	05.4	341 00.0	05.2	29 01.3	16.4	16.4	Atria	107 45.0	S69 01.8
20	126 48.4	152 04.7	16.6	199 37.9	05.3	356 02.6	05.2	44 03.6	16.4	16.4	Avior	234 21.2	S59 31.4
21	141 50.8	167 04.2	15.7	214 38.4	05.1	11 05.1	05.2	59 05.9	16.4	16.4	Bellatrix	278 40.8	N 6 21.1
22	156 53.3	182 03.8	14.7	229 39.2	05.0	26 07.6	05.3	74 08.2	16.4	16.4	Beletgeuse	171 10.1	N 7 6.2
23	171 55.8	197 03.4	13.7	244 40.0	04.9	41 10.1	05.3	89 10.5	16.5	16.5			
30 00 01	186 58.2	212 02.9	S11 12.8	259 40.7	S23 04.8	56 12.6	N19 05.3	104 12.8	N22 16.2	16.2	Canopus	263 59.8	S52 42.1
02	202 00.7	227 02.5	11.8	274 41.5	04.6	71 15.1	05.3	119 15.1	16.5	16.5	Capella	280 46.6	N46 00.2
03	217 03.2	242 02.1	10.8	289 42.3	04.5	86 17.6	05.3	134 17.4	16.5	16.5	Deneb	49 37.3	N45 17.1
04	232 05.6	257 01.6	09.8	304 43.0	04.4	101 20.1	05.3	149 19.7	16.5	16.5	Denebola	182 41.5	N14 33.2
05	247 08.1	272 01.2	08.9	319 43.8	04.3	116 22.6	05.3	164 22.0	16.5	16.5	Diphda	349 04.2	S17 58.3
06	262 10.5	287 00.8	07.9	334 44.6	04.1	131 25.1	05.3	179 24.3	16.6	16.6			
07	277 13.0	302 00.3	S11 06.9	349 45.3	S23 04.0	146 27.6	N19 05.3	194 26.6	N22 16.2	16.2	Dubhe	194 00.6	N61 44.2
08	292 15.5	316 59.9	06.0	4 46.1	03.9	161 30.1	05.3	209 28.9	16.6	16.6	Elnath	278 22.9	N28 36.7
09	307 17.9	331 59.5	05.0	19 46.9	03.7	176 32.6	05.3	224 31.2	16.6	16.6	Enif	33 55.3	N 9 53.1
10	322 20.4	346 59.0	04.0	34 47.7	03.6	191 35.1	05.3	239 33.5	16.6	16.6	Fomalhaut	15 33.1	S29 36.5
11	337 22.9	1 58.6	03.0	49 48.4	03.5	206 37.6	05.4	254 35.8	16.6	16.6			
12	352 25.3	16 58.2	02.1	64 49.2	03.4	221 40.1	05.4	269 38.0	16.6	16.6			
13	7 27.8	31 57.8	S11 01.1	79 50.0	S23 03.2	236 42.6	N19 05.4	284 40.3	N22 16.7	16.7	Gacrux	172 09.6	S57 07.9
14	22 30.3	46 57.3	11 00.1	94 50.7	03.1	251 45.1	05.4	299 42.6	16.7	16.7	Giannih	176 00.3	S17 33.6
15	37 32.7	61 56.9	10 59.1	109 51.3	03.0	266 47.6	05.4	314 44.9	16.7	16.7	Hadar	148 59.0	S60 23.2
16	52 35.2	76 56.5	09.8	124 52.3	02.8	281 50.1	05.4	329 47.2	16.7	16.7	Hamal	328 10.2	N23 28.5
17	67 37.7	91 56.0	08.7	139 53.1	02.7	296 52.6	05.4	344 49.5	16.7	16.7	Kaus Aust.	83 54.5	S34 23.0
18	82 40.1	106 55.6	07.6	154 53.8	02.6	311 55.1	05.4	359 51.8	16.7	16.7			
19	97 42.6	121 55.2	S10 55.2	169 54.6	S23 02.4	326 57.6	N19 05.4	14 54.1	N22 16.8	16.8	Kochab	137 18.3	N74 08.3
20	112 45.0	136 54.8	04.6	184 55.4	02.3	342 00.1	05.4	29 56.4	16.8	16.8	Markab	13 46.7	N15 13.1
21	127 47.5	151 54.3	03.3	199 56.1	02.2	357 02.6	05.4	44 58.7	16.8	16.8	Menkar	314 23.8	N 4 06.0
22	142 50.0	166 53.9	02.3	214 56.9	02.1	12 05.1	05.4	60 01.0	16.8	16.8	Menkent	148 16.8	S36 23.1
23	157 52.4	181 53.5	01.3	229 57.7	01.9	27 07.6	05.4	75 03.3	16.8	16.8	Miaplacidus	221 41.1	S69 44.0
31 00 01	172 54.9	196 53.1	00.3	244 58.5	01.8	42 10.1	05.4	90 05.5	16.8	16.8			
02	187 57.4	211 52.6	S10 49.3	259 59.2	S23 01.6	57 12.6	N19 05.4	105 07.8	N22 16.9	16.9	Miraf	308 52.4	N49 52.4
03	202 59.8	226 52.2	48.3	275 00.0	01.5	72 15.1	05.5	120 10.1	16.9	16.9	Nunki	76 08.2	S26 17.6
04	218 02.3	241 51.8	47.4	290 00.8	01.4	87 17.6	05.5	135 12.4	16.9	16.9	Peacock	53 32.0	S56 43.4
05	233 04.8	256 51.4	46.4	305 01.6	01.2	102 20.1	05.5	150 14.7	16.9	16.9	Pollux	243 37.4	N28 01.2
06	248 07.2	271 50.9	45.4	320 02.3	01.1	117 22.6	05.5	165 17.0	16.9	16.9	Procyon	245 08.1	N 5 13.0
07	263 09.7	286 50.5	44.4	335 03.1	01.0	132 25.1	05.5	180 19.3	16.9	16.9			
08	278 12.1	301 50.1	S10 43.4	350 03.9	S23 00.8	147 27.6	N19 05.5	195 21.6	N22 17.0	17.0	Rasalhague	96 13.8	N12 33.2
09	293 14.6	316 49.7	42.4	5 04.7	00.7	162 30.1	05.5	210 23.9	17.0	17.0	Regulus	207 51.8	N11 57.1
10	308 17.1	331 49.2	41.5	20 05.4	00.6	177 32.6	05.5	225 26.1	17.0	17.0	Rigel	281 19.9	S 8 12.0
11	323 19.5	346 48.8	40.5	35 06.2	00.4	192 35.1	05.5	240 28.4	17.0	17.0	Rigel Kent.	140 02.5	S60 50.8
12	338 22.0	1 48.4	39.5	50 07.0	00.3	207 37.6	05.5	255 30.7	17.0	17.0	Sabik	102 21.7	S15 43.8
13	353 24.5	16 48.0	38.5	65 07.8	00.2	222 40.1	05.5	270 33.0	17.0	17.0			
14	8 26.9	31 47.6	S10 37.5	80 08.5	S23 00.0	237 42.6	N19 05.5	285 35.3	N22 17.0	17.0	Schedar	349 50.6	N56 33.2
15	23 29.4	46 47.1	36.5	95 09.3	00.0	252 45.1	05.5	300 37.6	17.1	17.1	Shaula	96 32.8	S37 06.3
16	38 31.9	61 46.7	35.5	110 10.1	00.0	267 47.6	05.5	315 39.9	17.1	17.1	Sirius	258 40.9	S16 43.3
17	53 34.3	76 46.3	34.5	125 10.9	00.0	282 50.1	05.5	330 42.2	17.1	17.1	Spica	158 59.5	S11 10.7
18	68 36.8	91 45.9	33.5	140 11.6	00.0	297 52.6	05.5	345 44.5	17.1	17.1	Suhail	222 58.2	S43 26.9
19	83 39.3	106 45.5	32.5	155 12.4	00.0	312 55.1	05.5	0 46.7	17.1	17.1			
20	98 41.7	121 45.0	S10 31.6	170 13.2	S22 59.2	327 57.6	N19 05.5	15 49.0	N22 17.1	17.1	Vega	80 44.4	N38 46.8
21	113 44.2	136 44.6	30.6	185 14.0	00.0	343 00.1	05.6	30 51.3	17.2	17.2	Zuben'ubi	137 14.1	S16 03.4
22	128 46.6	151 44.2	29.6	200 14.7	00.0	358 02.5	05.6	45 53.6	17.2	17.2			
23	143 49.1	166 43.8	28.6	215 15.5	00.0	13 05.0	05.6	60 55.9	17.2	17.2			
24	158 51.6	181 43.4	27.6	230 16.3	00.0	28 07.5	05.6	75 58.2	17.2	17.2			
25	173 54.0	196 42.9	26.6	245 17.1	00.0	43 10.0	05.6	91 00.5	17.2	17.2			
h m		v -0.4	d 1.0	v 0.8	d 0.1								



UT	ARIES		VENUS -3.9		MARS -1.4		JUPITER -1.8		SATURN +0.0		STARS			
	GHA	Dec	GHA	Dec	GHA	Dec	GHA	Dec	GHA	Dec	Name	SHA	Dec	
27 00	274 41.6	194 56.9 N22 40.8	297 23.7 S13 53.3	134 48.5 N16 26.8	181 29.3 N22 36.5	Acamar	315 24.5 S40 17.3							
01	289 44.1	209 56.1 41.1	312 25.3 53.1	149 50.5 26.7	196 31.4 36.5	Achernar	335 32.6 S57 12.9							
02	304 46.5	224 55.3 41.4	327 26.8 52.9	164 52.5 26.6	211 33.5 36.5	Achernar	173 18.4 S63 07.9							
03	319 49.0	239 54.5 41.7	342 28.4 52.7	179 54.5 26.4	226 35.6 36.5	Adhara	255 19.1 S28 58.5							
04	334 51.5	254 53.6 42.0	357 29.9 52.5	194 56.5 26.3	241 37.7 36.5	Aldebaran	290 58.7 N16 31.0							
05	349 53.9	269 52.8 42.4	12 31.5 52.3	209 58.5 26.1	256 39.8 36.5									
06	4 56.4	284 52.0 N22 42.7	27 33.1 S13 52.1	225 00.5 N16 26.0	271 41.9 N22 36.5	Alloth	166 27.3 N55 56.8							
07	19 58.8	299 51.1 43.0	42 34.6 51.9	240 02.5 25.8	286 44.1 36.5	Alkaid	153 04.7 N49 18.1							
08	35 01.3	314 50.3 43.3	57 36.2 51.7	255 04.5 25.7	301 46.2 36.5	Al Na'ir	27 53.1 S46 56.5							
09	50 03.8	329 49.5 43.6	72 37.8 51.5	270 06.5 25.6	316 48.3 36.5	Ankara	275 54.7 S 1 11.9							
10	65 06.2	344 48.6 43.9	87 39.3 51.4	285 08.5 25.4	331 50.4 36.5	Alphard	218 04.1 S 8 40.3							
11	80 08.7	359 47.8 44.2	102 40.9 51.2	300 10.5 25.3	346 52.5 36.5									
12	95 11.2	14 47.0 N22 44.5	117 42.5 S13 51.0	315 12.5 N16 25.1	1 54.6 N22 36.5	Alphecca	126 17.3 N26 42.3							
13	110 13.6	29 46.1 44.8	132 44.1 50.8	330 14.5 25.0	16 56.7 36.5	Alpheratz	257 51.7 N29 06.3							
14	125 16.1	44 45.3 45.1	147 45.6 50.6	345 16.5 24.8	31 58.8 36.5	Alhair	62 15.6 N 8 52.6							
15	140 18.6	59 44.5 45.4	162 47.2 50.4	0 18.5 24.7	47 00.9 36.5	Ankaa	353 23.3 S42 17.1							
16	155 21.0	74 43.6 45.7	177 48.8 50.2	15 20.5 24.6	62 03.1 36.5	Antares	112 35.6 S26 26.5							
17	170 23.5	89 42.8 46.0	192 50.3 51.0	30 22.5 24.4	77 05.2 36.5									
18	185 26.0	104 42.0 N22 46.3	207 51.9 S13 49.9	45 24.5 N16 24.3	92 07.3 N22 36.5	Arcturus	146 02.7 N19 10.0							
19	200 28.4	119 41.1 46.6	222 53.5 49.7	60 26.4 24.1	107 09.4 36.5	Atria	177 44.1 S69 02.2							
20	215 30.9	134 40.3 46.9	237 55.1 49.5	75 28.4 24.0	122 11.5 36.4	Avior	234 22.0 S59 31.3							
21	230 33.3	149 39.5 47.2	252 56.7 49.3	90 30.4 23.8	137 13.6 36.4	Bellatrix	278 40.8 N 6 21.2							
22	245 35.8	164 38.6 47.5	267 58.2 49.1	105 32.4 23.7	152 15.7 36.4	Betelgeuse	271 10.2 N 7 24.5							
23	260 38.3	179 37.8 47.8	282 59.8 48.9	120 34.4 23.5	167 17.8 36.4									
28 00	275 40.7	194 37.0 N22 48.1	298 01.4 S13 48.8	135 36.4 N16 23.4	182 20.0 N22 36.4	Canopus	264 00.2 S52 41.8							
01	290 43.2	209 36.1 48.4	313 03.0 48.6	150 38.4 23.3	197 22.1 36.4	Capella	280 46.6 N46 00.1							
02	305 45.7	224 35.3 48.7	328 04.6 48.4	165 40.4 23.1	212 24.2 36.4	Deneb	49 36.5 N45 17.3							
03	320 48.1	239 34.5 48.9	343 06.1 48.2	180 42.4 23.0	227 26.3 36.4	Denebola	182 41.7 N14 33.3							
04	335 50.6	254 33.6 49.2	358 07.7 48.0	195 44.4 22.8	242 28.4 36.4	Diphda	349 03.8 S17 58.0							
05	350 53.1	269 32.8 49.5	13 09.3 47.8	210 46.4 22.7	257 30.5 36.4									
06	5 55.5	284 31.9 N22 49.8	28 10.9 S13 47.7	225 48.4 N16 22.5	272 32.6 N22 36.4	Dubhe	194 01.3 N61 44.3							
07	20 58.0	299 31.1 50.1	43 12.5 47.5	240 50.4 22.4	287 34.7 36.4	Elnath	278 23.0 N28 36.6							
08	36 00.4	314 30.3 50.4	58 14.1 47.3	255 52.4 22.2	302 36.8 36.4	Eltanin	90 49.3 N51 29.3							
09	51 02.9	329 29.4 50.6	73 15.6 47.1	270 54.4 22.1	317 39.0 36.4	Enif	33 54.6 N 9 53.3							
10	66 05.4	344 28.6 50.9	88 17.2 46.9	285 56.4 22.0	332 41.1 36.4	Fomalhaut	15 32.4 S29 36.2							
11	81 07.8	359 27.8 51.2	103 18.8 46.7	300 58.4 21.8	347 43.2 36.4									
12	96 10.3	14 26.9 N22 51.5	118 20.4 S13 46.6	316 00.4 N16 21.7	2 45.3 N22 36.4	Gacrux	172 09.9 S57 08.2							
13	111 12.8	29 26.1 51.8	133 22.0 46.3	331 02.4 21.5	17 47.4 36.4	Gienah	176 00.5 S17 33.7							
14	126 15.2	44 25.2 52.0	148 23.6 46.2	346 04.4 21.4	32 49.5 36.4	Hadar	148 59.0 S60 23.6							
15	141 17.7	59 24.4 52.3	163 25.2 46.0	1 06.4 21.2	47 41.6 36.4	Hamal	328 09.9 S23 28.6							
16	156 20.2	74 23.6 52.6	178 26.8 45.8	16 08.4 21.1	62 53.7 36.4	Kaus Aust.	83 53.8 S34 23.0							
17	171 22.6	89 22.7 52.8	193 28.4 45.7	31 10.4 20.9	77 55.9 36.4									
18	186 25.1	104 21.9 N22 53.1	208 30.0 S13 45.5	46 12.4 N16 20.8	92 58.0 N22 36.4	Kochab	137 18.6 N74 08.8							
19	201 27.6	119 21.0 53.4	223 31.6 45.3	61 14.4 20.7	108 00.1 36.3	Markab	13 46.1 N15 13.3							
20	216 30.0	134 20.2 53.7	238 33.2 45.1	76 16.4 20.4	123 02.2 36.3	Menkar	314 23.5 N 4 06.2							
21	231 32.5	149 19.4 53.9	253 34.8 45.0	91 18.4 20.2	138 04.3 36.3	Meikant	148 16.8 S36 23.3							
22	246 34.9	164 18.5 54.2	268 36.4 44.8	106 20.4 20.2	153 06.4 36.3	Miaplacidus	221 42.4 S69 44.0							
23	261 37.4	179 17.7 54.5	283 38.0 44.6	121 22.3 20.1	168 08.5 36.3									
29 00	276 39.9	194 16.8 N22 54.7	298 39.6 S13 44.4	136 24.3 N16 19.9	183 10.6 N22 36.3	Mirafak	308 52.1 N49 52.2							
01	291 42.3	209 16.0 55.0	313 41.2 44.3	151 26.3 19.8	198 12.8 36.3	Nunki	76 07.7 S26 17.6							
02	306 44.8	224 15.1 55.2	328 42.8 44.1	166 28.3 19.6	213 14.9 36.3	Peacock	53 30.9 S56 43.4							
03	321 47.3	239 14.3 55.5	343 44.4 43.9	181 30.3 19.5	228 17.0 36.3	Pollux	243 37.7 N28 01.2							
04	336 49.7	254 13.5 55.8	358 46.0 43.7	196 32.3 19.3	243 19.1 36.3	Procyon	245 08.3 N 5 13.1							
05	351 52.2	269 12.6 56.0	13 47.6 43.6	211 34.3 19.2	258 21.2 36.3									
06	6 54.7	284 11.8 N22 56.3	28 49.2 S13 43.4	226 36.3 N16 19.1	273 23.3 N22 36.3	Rasalhague	96 13.4 N12 33.4							
07	21 57.1	299 10.9 56.5	43 50.8 43.2	241 38.3 18.9	288 25.4 36.3	Regulus	207 52.0 N11 57.2							
08	36 59.6	314 10.1 56.8	58 52.4 43.0	256 40.3 18.8	303 27.5 36.3	Rigel	281 19.9 S 8 11.8							
09	52 02.1	329 09.2 57.0	73 54.0 42.9	271 42.3 18.6	318 29.7 36.3	Rigel Kent.	140 02.4 S60 51.2							
10	67 04.5	344 08.4 57.3	88 55.6 42.7	286 44.3 18.5	333 31.8 36.3	Sabik	102 21.2 S15 43.8							
11	82 07.0	359 07.6 57.5	103 57.2 42.5	301 46.3 18.3	348 33.9 36.3									
12	97 09.4	14 06.7 N22 57.8	118 58.8 S13 42.3	316 48.3 N16 18.2	3 36.0 N22 36.3	Schedar	349 49.8 N56 33.0							
13	112 11.9	29 05.9 58.0	134 00.4 42.2	331 50.3 18.0	18 38.1 36.3	Shaula	96 32.2 S37 06.5							
14	127 14.4	44 05.0 58.3	149 02.0 42.0	346 52.3 17.9	33 40.2 36.3	Sirius	258 41.0 S16 43.2							
15	142 16.8	59 04.2 58.5	164 03.7 41.8	1 54.3 17.7	48 42.3 36.3	Spica	158 39.5 S11 10.8							
16	157 19.3	74 03.2 58.8	179 05.3 41.7	16 56.2 17.6	63 44.4 36.3	Suhail	222 58.7 S43 26.8							
17	172 21.8	89 02.5 59.0	194 06.9 41.5	31 58.2 17.5	78 46.6 36.2									
18	187 24.2	104 01.6 N22 59.3	209 08.5 S13 41.3	47 00.2 N16 17.3	93 48.7 N22 36.2	Vega	80 43.9 N38 47.1							
19	202 26.7	119 00.8 59.5	224 10.1 41.1	62 02.2 17.2	108 50.8 36.2	Zuben'ubi	137 14.0 S16 03.4							
20	217 29.2	133 59.9 59.5	239 11.7 41.0	77 04.2 17.0	123 52.9 36.2									
21	232 31.6	148 59.1 23 00.0	254 13.4 40.8	92 06.2 16.9	138 55.0 36.2									
22	247 34.1	163 58.3 00.2	269 15.0 40.6	107 08.2 16.7	153 57.1 36.2	Venus	278 56.2 11 02							
23	262 36.6	178 57.4 00.5	284 16.6 40.5	122 10.2 16.6	168 59.2 36.2	Mars	22 20.7 4 07							
						Jupiter	219 55.7 14 56							
						Saturn	266 39.2 11 49							

Mer.Pass. 5 36.4 v -0.8 d 0.3 v 1.6 d 0.2 v 2.0 d 0.1 v 2.1 d 0.0



UT	ARIES		VENUS -3.9		MARS -2.4		JUPITER -1.7		SATURN +0.1		STARS		
	d	h	GHA	Dec	GHA	Dec	GHA	Dec	GHA	Dec	Name	SHA	Dec
1900	357	29.3	173 11.2	S 0 29.6	22 49.4	S16 24.3	200 27.7	N10 31.7	254 30.6	N22 09.6	Acamar	315 23.8	S40 17.1
01	12	31.7	188 10.8	30.9	37 52.2	24.2	215 29.7	31.5	269 32.9	09.6	Achernar	335 31.7	S57 12.8
02	27	34.2	203 10.4	32.2	52 55.0	24.1	230 31.6	31.3	284 35.2	09.6	Acruz	173 18.9	S63 07.1
03	42	36.7	218 10.1	33.5	67 57.8	24.1	245 33.6	31.1	299 37.5	09.6	Adhara	255 18.7	S28 58.3
04	57	39.1	233 09.7	34.7	83 00.6	24.0	260 35.6	30.9	314 39.8	09.6	Aldebaran	290 58.1	N16 31.1
05	72	41.6	248 09.3	36.0	98 03.4	23.9	275 37.5	30.7	329 42.1	09.6			
06	87	44.1	263 08.9	S 0 37.3	113 06.2	S16 23.8	290 39.5	N10 30.5	344 44.4	N22 09.6	Alioth	166 27.7	N55 56.6
07	102	46.5	278 08.6	38.6	128 08.9	23.8	305 41.5	30.3	359 46.6	09.5	Alkaid	153 05.2	N49 17.9
08	117	49.0	293 08.2	39.8	143 11.7	23.7	320 43.4	30.2	41 48.9	09.5	Al Nair	27 52.8	S46 56.7
09	132	51.4	308 07.8	41.1	158 14.5	23.6	335 45.4	30.0	29 51.2	09.5	Ainamil	275 54.7	S 11 11.8
10	147	53.9	323 07.5	42.4	173 17.3	23.5	350 47.4	29.8	44 53.5	09.5	Alphard	218 03.9	S 8 40.2
11	162	56.4	338 07.1	43.7	188 20.1	23.4	5 49.3	29.6	59 55.8	09.5			
12	177	58.8	353 06.7	S 0 44.9	203 22.9	S16 23.4	20 51.3	N10 29.4	74 58.1	N22 09.6	Alphecca	126 17.7	N26 42.4
13	193	01.3	8 06.4	46.2	218 25.6	23.3	35 53.2	29.2	90 00.4	09.5	Alpheratz	357 51.2	N29 06.7
14	208	03.8	23 06.0	47.5	233 28.4	23.2	50 55.2	29.0	105 02.7	09.4	Alnilam	62 15.6	N 8 52.7
15	223	06.2	38 05.6	48.8	248 31.2	23.1	65 57.2	28.8	120 05.0	09.4	Ankaa	353 22.7	S42 17.1
16	238	08.7	53 05.2	50.0	263 34.0	23.0	80 59.1	28.6	135 07.3	09.4	Antares	112 35.9	S46 26.5
17	253	11.2	68 04.9	51.3	278 36.8	23.0	96 01.1	28.5	150 09.6	09.4			
18	268	13.6	83 04.5	S 0 52.6	293 39.5	S16 22.9	111 03.1	N10 28.3	165 11.9	N22 09.6	Arcturus	146 03.0	N19 10.0
19	283	16.1	98 04.1	53.9	308 42.3	22.8	126 05.0	28.1	180 14.2	09.4	Atria	107 44.8	S69 02.3
20	298	18.6	113 03.8	55.1	323 45.1	22.7	141 07.0	27.9	195 16.5	09.4	Avior	234 21.7	S59 30.9
21	313	21.0	128 03.4	56.4	338 47.9	22.6	156 09.0	27.7	210 18.8	09.3	Bellatrix	278 40.2	N 6 21.4
22	328	23.5	143 03.0	57.7	353 50.6	22.5	171 10.9	27.5	225 21.0	09.3	Beltegeuse	271 09.6	N 7 24.6
23	343	25.9	158 02.7	0 59.0	8 53.4	22.4	186 12.9	27.3	240 23.3	09.3			
2000	358	28.4	173 02.3	S 1 00.2	23 56.2	S16 22.4	201 14.9	N10 27.1	255 25.6	N22 09.3	Canopus	263 59.7	S52 41.4
01	13	30.9	188 01.9	01.5	38 58.9	22.3	216 16.8	26.9	270 27.9	09.3	Capella	280 45.8	N46 00.0
02	28	33.3	203 01.6	02.8	54 01.7	22.2	231 18.8	26.8	285 30.2	09.3	Deneb	49 36.5	N45 17.8
03	43	35.8	218 01.2	04.1	69 04.5	22.1	246 20.8	26.6	300 32.5	09.3	Denebola	182 41.8	N14 33.3
04	58	38.3	233 00.8	05.3	84 07.2	22.0	261 22.7	26.4	315 34.8	09.3	Diphda	349 03.2	S71 57.9
05	73	40.7	248 00.4	06.6	99 10.0	21.9	276 24.7	26.2	330 37.1	09.2			
06	88	43.2	263 00.1	S 1 07.9	114 12.7	S16 21.8	291 26.7	N10 26.0	345 39.4	N22 09.2	Dubhe	194 01.4	N61 44.0
07	103	45.7	277 59.7	09.2	129 15.5	21.7	306 28.6	25.8	0 41.7	09.2	Elnath	278 22.3	N28 36.7
08	118	48.1	292 59.3	10.4	144 18.3	21.6	321 30.6	25.6	15 44.0	09.2	Eltanin	90 49.7	N51 29.5
09	133	50.6	307 59.0	11.7	159 21.0	21.5	336 32.6	25.4	30 46.3	09.2	Enif	33 54.4	N 9 53.6
10	148	53.0	322 58.6	13.0	174 23.8	21.4	351 34.5	25.3	45 48.6	09.2	Fornahaut	15 32.0	S29 36.2
11	163	55.5	337 58.2	14.3	189 26.5	21.4	6 36.5	25.1	60 50.9	09.2			
12	178	58.0	352 57.8	S 1 15.5	204 29.3	S16 21.3	21 38.5	N10 24.9	75 53.2	N22 09.1	Gacrux	172 10.3	S57 07.9
13	194	00.4	7 57.5	16.8	219 32.0	21.2	36 40.4	24.7	90 55.5	09.1	Genah	176 00.6	S17 33.6
14	209	02.9	22 57.1	18.1	234 34.8	21.1	51 42.4	24.5	105 57.8	09.1	Hadar	148 59.6	S60 23.5
15	224	05.4	37 56.7	19.4	249 37.5	21.0	66 44.4	24.3	121 00.1	09.1	Haus	328 09.2	N23 28.8
16	239	07.8	52 56.4	20.6	264 40.3	20.9	81 46.3	24.1	136 02.4	09.1	Karmel	83 53.9	S34 23.1
17	254	10.3	67 56.0	21.9	279 43.0	20.8	96 48.3	23.9	151 04.7	09.1			
18	269	12.8	82 55.6	S 1 23.2	294 45.8	S16 20.7	111 50.3	N10 23.7	166 07.0	N22 09.1	Kochab	137 20.1	N74 08.7
19	284	15.2	97 55.3	24.5	309 48.5	20.6	126 52.2	23.6	181 09.3	09.1	Markab	13 45.7	N15 13.6
20	299	17.7	112 54.9	25.7	324 51.3	20.5	141 54.2	23.4	196 11.6	09.0	Menkar	314 22.9	N 4 06.4
21	314	20.2	127 54.5	27.0	339 54.0	20.4	156 56.2	23.2	211 13.9	09.0	Menkent	148 17.1	S36 23.3
22	329	22.6	142 54.1	28.3	354 56.7	20.3	171 58.1	23.0	226 16.2	09.0	Miaplacidus	221 42.4	S69 43.6
23	344	25.1	157 53.8	29.6	9 59.5	20.2	187 00.1	22.8	241 18.5	09.0			
2100	359	27.5	172 53.4	S 1 30.8	25 02.2	S16 20.1	202 02.1	N10 22.6	256 20.8	N22 09.0	Miraf	308 51.2	N49 52.4
01	14	30.0	187 53.0	32.1	40 05.0	20.0	217 04.0	22.4	271 23.1	09.0	Nunki	76 07.7	S26 17.6
02	29	32.5	202 52.7	33.4	55 07.7	19.9	222 06.0	22.2	286 25.4	09.0	Peacock	53 30.8	S56 43.6
03	44	34.9	217 52.3	34.7	70 10.4	19.8	247 08.0	22.1	301 27.7	08.9	Pollux	243 37.3	N28 01.1
04	59	37.4	232 51.9	35.9	85 13.2	19.7	262 09.9	21.9	316 30.0	08.9	Procyon	245 07.9	N 5 13.2
05	74	39.9	247 51.5	37.2	100 15.9	19.6	277 11.9	21.7	331 32.3	08.9			
06	89	42.3	262 51.2	S 1 38.5	115 18.6	S16 19.5	292 13.9	N10 21.5	346 34.6	N22 08.9	Rasalhague	96 13.6	N12 33.6
07	104	44.8	277 50.8	39.8	130 21.4	19.4	307 15.8	21.3	361 36.9	08.9	Regulus	207 51.9	N11 57.2
08	119	47.3	292 50.4	41.0	145 24.1	19.3	322 17.8	21.1	376 39.2	08.9	Rigel	281 19.4	S 8 11.6
09	134	49.7	307 50.1	42.3	160 26.8	19.2	337 19.8	20.9	391 41.5	08.9	Fligel Kent.	140 03.1	S60 51.1
10	149	52.7	322 49.7	43.6	175 29.5	19.0	352 21.8	20.7	46 43.8	08.9	Sabik	102 21.4	S15 43.8
11	164	54.7	337 49.3	44.9	190 32.3	18.9	7 23.7	20.6	61 46.1	08.8			
12	179	57.1	352 48.9	S 1 46.1	205 35.0	S16 18.8	22 25.7	N10 20.4	76 48.4	N22 08.8	Schedar	349 49.0	N56 33.4
13	194	59.6	7 48.6	47.4	220 37.7	18.7	37 27.7	20.2	91 50.7	08.8	Shaula	96 32.4	S37 06.5
14	210	02.0	22 48.2	48.7	235 40.4	18.6	52 29.6	20.0	106 53.0	08.8	Sirius	258 40.6	S16 42.9
15	225	04.5	37 47.8	50.0	250 43.1	18.5	67 31.6	19.8	121 55.3	08.8	Spica	158 39.7	S11 10.7
16	240	07.0	52 47.5	51.2	265 45.9	18.4	82 33.6	19.6	136 57.6	08.8	Suhail	222 58.5	S43 26.5
17	255	09.4	67 47.1	52.5	280 48.6	18.3	97 35.5	19.4	151 59.9	08.8			
18	270	11.9	82 46.7	S 1 53.8	295 51.3	S16 18.2	112 37.5	N10 19.2	167 02.2	N22 08.7	Vega	80 44.1	N38 47.4
19	285	14.4	97 46.3	55.1	310 54.0	18.1	127 39.5	19.1	182 04.5	08.7	Zubenubi	137 14.2	S16 03.4
20	300	16.8	112 46.0	56.3	325 56.7	18.0	142 41.4	18.9	197 06.8	08.7			
21	315	19.3	127 45.6	57.6	340 59.4	17.8	157 43.4	18.7	212 09.1	08.7			
22	330	21.8	142 45.2	58.9	356 02.1	17.7	172 45.4	18.5	227 11.4	08.7			
23	345	24.2	157 44.8	S 0 00.2	11 04.9	17.6	187 47.3	18.3	242 13.7	08.7			
			h m								SHA	Mer.Pass.	
			v -0.4	d 1.3	v 2.8	d 0.1	v 2.0	d 0.2	v 2.3	d 0.0			
			Mer.Pass.	0 06.1							Venus	174 33.9	12 28
											Mars	25 27.8	22 20



Table with columns for UT, ARIES, VENUS -3.9, MARS -2.2, JUPITER -1.7, SATURN +0.1, and STARS. It lists celestial objects with their coordinates and magnitudes.

Table with columns for UT, SUN, MOON, Lat., Twilight (Naut., Civil), Sunrise, Moonrise (28, 29, 30, 1), and Moonset (28, 29, 30, 1). It provides detailed astronomical data for the Sun and Moon.



UT	ARIES			VENUS -3.9			MARS -1.2			JUPITER -1.8			SATURN -0.1			STARS			
	GHA	SHA	Dec	GHA	SHA	Dec	GHA	SHA	Dec	GHA	SHA	Dec	GHA	SHA	Dec	Name	SHA	Dec	
31 00	38 53.1	164 51.1	S19 31.0	59 19.1	S11 11.9	234 15.7	N 7 35.8	294 36.3	N22 03.4	Acamar	315 23.6	S40 17.3							
01	53 55.6	179 50.4	31.8	74 20.7	11.4	249 17.8	35.7	309 38.8	03.4	Achernar	335 31.6	S57 13.1							
02	68 58.0	194 49.6	32.7	89 23.3	10.9	264 19.8	35.5	324 41.2	03.4	Acrux	173 18.8	S63 06.9							
03	84 00.5	209 48.9	33.5	104 24.0	10.4	279 21.9	35.4	339 43.7	03.4	Adhara	255 18.4	S28 58.3							
04	99 02.9	224 48.2	34.3	119 25.6	09.9	294 24.0	35.2	354 46.2	03.4	Aldebaran	290 57.8	N16 31.1							
05	114 05.4	239 47.5	35.2	134 27.3	09.4	309 26.1	35.1	9 48.7	03.4										
06	129 07.9	254 46.8	S19 36.0	149 28.9	S11 08.9	324 28.1	N 7 34.9	24 51.2	N22 03.4	Alloth	166 27.6	N55 56.3							
07	144 10.3	269 46.0	36.8	164 30.6	08.4	339 30.2	34.8	39 53.7	03.4	Altohd	153 05.2	N49 17.7							
08	159 12.8	284 45.3	37.6	179 32.2	08.0	354 32.3	34.8	54 56.2	03.4	Al Nair	27 52.9	S46 56.8							
09	174 15.3	299 44.6	38.5	194 33.8	07.5	9 34.4	34.5	69 58.7	03.4	Alnilam	275 53.9	S 1 11.8							
10	189 17.7	314 43.9	39.3	209 35.5	07.0	24 36.4	34.3	85 01.2	03.4	Alphard	218 03.6	S 8 40.2							
11	204 20.2	329 43.2	40.1	224 37.1	06.5	39 38.5	34.2	100 03.7	03.4										
12	219 22.7	344 42.4	S19 40.9	239 38.8	S11 06.0	54 40.6	N 7 34.0	115 06.2	N22 03.4	Alphecca	126 17.8	N26 42.2							
13	234 25.1	359 41.7	41.8	254 40.4	05.5	69 42.7	33.9	130 08.6	03.4	Alpheratz	357 51.2	N29 06.8							
14	249 27.6	374 41.0	42.6	269 42.0	05.0	84 44.8	33.7	145 11.1	03.5	Altair	62 15.7	N 8 52.7							
15	264 30.1	389 40.3	43.4	284 43.7	04.5	99 46.8	33.6	160 13.6	03.5	Ankaa	353 22.2	S24 17.2							
16	279 32.5	404 39.5	44.2	299 45.3	04.0	114 48.9	33.4	175 16.1	03.5	Antares	112 36.0	S26 26.4							
17	294 35.0	59 38.8	45.0	314 46.9	03.5	129 51.0	33.3	190 18.6	03.5										
18	309 37.4	74 38.1	S19 45.8	329 48.6	S11 03.1	144 53.1	N 7 33.1	205 21.1	N22 03.5	Arcturus	146 03.0	N19 09.9							
19	324 39.9	89 37.4	46.7	344 50.2	02.6	159 55.2	33.0	220 23.6	03.5	Atria	107 45.2	S69 02.2							
20	339 42.4	104 36.6	47.5	359 51.8	02.1	174 57.2	32.8	235 26.1	03.5	Avior	234 21.2	S59 30.9							
21	354 44.8	119 35.9	48.3	374 53.5	01.6	189 59.3	32.7	250 28.6	03.5	Bellatrix	278 39.9	N 6 21.3							
22	9 47.3	134 35.2	49.1	29 55.1	01.1	205 01.4	32.5	265 31.1	03.5	Betelgeuse	271 09.3	N 7 24.6							
23	24 49.8	149 34.4	49.9	44 56.7	00.6	220 03.5	32.4	280 33.6	03.5										
1 00	39 52.2	164 33.7	S19 50.7	59 58.4	S11 00.1	235 05.5	N 7 32.2	295 36.1	N22 03.5	Canopus	263 59.2	S52 41.5							
01	54 54.7	179 33.0	51.5	75 00.0	10 51.6	310 07.6	32.1	310 38.6	03.5	Capella	280 55.2	N29 06.8							
02	69 57.2	194 32.3	52.3	90 01.6	59.1	265 09.7	31.9	325 41.1	03.5	Deneb	49 36.8	N45 17.8							
03	84 59.6	209 31.5	53.1	105 03.2	58.6	280 11.8	31.8	340 43.6	03.5	Denobola	182 41.6	N14 33.2							
04	100 02.1	224 30.8	53.9	120 04.9	58.1	295 13.9	31.6	355 46.0	03.5	Diphda	349 03.2	S17 58.0							
05	115 04.5	239 30.1	54.7	135 06.5	57.6	310 15.9	31.5	10 48.5	03.5										
06	130 07.0	254 29.3	S19 55.6	150 08.1	S10 57.1	325 18.0	N 7 31.3	25 51.0	N22 03.5	Dubhe	194 01.0	N61 43.7							
07	145 09.5	269 28.6	56.6	165 09.7	56.6	340 20.1	31.2	40 53.5	03.5	Elmath	278 22.0	N28 36.7							
08	160 11.9	284 27.9	57.2	180 11.4	56.2	355 22.2	31.0	55 56.0	03.5	Eltanin	90 50.0	N51 29.5							
09	175 14.4	299 27.1	58.0	195 13.0	55.7	10 24.3	30.9	70 58.5	03.5	Enif	33 54.5	N 9 53.6							
10	190 16.9	314 26.4	58.8	210 14.6	55.2	25 26.3	30.7	86 01.0	03.5	Fomalhaut	15 32.0	S29 36.3							
11	205 19.3	329 25.7	59 59.6	225 16.2	54.7	40 28.4	30.6	101 03.5	03.5										
12	220 21.8	344 24.9	S20 00.4	240 17.9	S10 54.2	55 30.5	N 7 30.4	116 06.0	N22 03.5	Gacrux	172 10.2	S57 07.8							
13	235 24.3	359 24.2	01.2	255 19.5	53.7	70 32.6	30.3	131 08.5	03.5	Gienah	176 00.5	S17 33.5							
14	250 26.7	374 23.4	02.0	270 21.1	53.2	85 34.7	30.1	146 11.0	03.5	Hadar	148 59.6	S60 23.3							
15	265 29.2	389 22.7	02.7	285 22.7	52.7	100 36.8	30.0	161 13.5	03.5	Hamil	348 09.1	N23 28.9							
16	280 31.7	404 22.0	03.5	300 24.3	52.2	115 38.8	29.8	176 16.0	03.5	Kaus Aust.	83 54.1	S34 23.1							
17	295 34.4	59 21.2	04.3	315 26.0	51.7	130 40.9	29.7	191 18.5	03.6										
18	310 36.6	74 20.5	S20 05.1	330 27.6	S10 51.2	145 43.0	N 7 29.5	206 21.0	N22 03.6	Kochab	137 20.5	N74 08.4							
19	325 39.0	89 19.8	05.9	345 29.0	50.7	160 45.1	29.4	221 23.5	03.6	Markab	13 45.8	N15 13.6							
20	340 41.5	104 19.0	06.7	0 30.8	50.2	175 47.2	29.2	236 26.0	03.6	Menkar	314 22.7	N 4 06.4							
21	355 44.0	119 18.3	07.5	15 32.4	49.7	190 49.3	29.1	251 28.5	03.6	Menkent	148 17.1	S36 23.2							
22	10 46.4	134 17.5	08.3	30 34.0	49.2	205 51.3	28.9	266 31.0	03.6	Miaplacidus	221 41.7	S69 43.5							
23	25 48.9	149 16.8	09.1	45 35.6	48.7	220 53.4	28.8	281 33.5	03.6										
2 00	40 51.4	164 16.1	S20 09.9	60 37.2	S10 48.2	235 55.5	N 7 28.6	296 36.0	N22 03.6	Mirafak	308 50.9	N49 52.5							
01	55 53.8	179 15.3	10.7	75 38.9	47.7	250 57.6	28.5	311 38.5	03.6	Nunki	76 07.9	S26 17.7							
02	70 56.3	194 14.6	11.4	90 40.5	47.2	265 59.7	28.3	326 41.0	03.6	Peacock	53 31.1	S56 43.7							
03	85 58.8	209 13.8	12.2	105 42.1	46.7	281 01.8	28.2	341 43.5	03.6	Pollux	243 36.9	N28 01.1							
04	101 01.2	224 13.1	13.0	120 43.7	46.2	296 03.8	28.0	356 46.0	03.6	Procyon	245 07.6	N 5 13.1							
05	116 03.7	239 12.3	13.8	135 45.3	45.7	311 05.9	27.9	11 48.5	03.6										
06	131 06.2	254 11.6	S20 14.6	150 46.9	S10 45.2	326 08.0	N 7 27.7	26 51.0	N22 03.6	Rasalhague	96 13.8	N12 33.5							
07	146 08.6	269 10.8	15.3	165 48.5	44.7	341 10.1	27.6	41 53.5	03.6	Regulus	207 51.7	N11 57.1							
08	161 11.1	284 10.1	16.1	180 50.1	44.2	356 12.2	27.4	56 56.0	03.6	Rigel	281 19.1	S 8 11.6							
09	176 13.5	299 09.3	16.9	195 51.7	43.7	11 14.3	27.3	71 58.5	03.6	Rigil Kent.	140 03.2	S60 51.0							
10	191 16.0	314 08.6	17.7	210 53.3	43.2	26 16.3	27.1	87 01.0	03.6	Sabik	102 21.6	S15 43.8							
11	206 18.5	329 07.9	18.5	225 54.9	42.7	41 18.4	27.0	102 03.5	03.6										
12	221 20.9	344 07.1	S20 19.2	240 56.5	S10 42.2	56 20.5	N 7 26.8	117 06.0	N22 03.6	Schedar	349 49.0	N56 33.6							
13	236 23.4	359 06.4	20.0	255 58.1	41.7	71 22.6	26.7	132 08.5	03.6	Shaula	96 32.6	S37 06.5							
14	251 25.9	374 05.6	20.8	270 59.7	41.2	86 24.7	26.5	147 11.0	03.6	Sirius	258 40.3	S16 43.0							
15	266 28.3	389 04.9	21.6	286 01.3	40.7	101 26.8	26.4	162 13.5	03.6	Spica	158								



UT	ARIES			VENUS -4.0			MARS +0.0			JUPITER -2.1			SATURN -0.4			STARS		
	GHA	SHA	Dec	GHA	SHA	Dec	GHA	SHA	Dec	GHA	SHA	Dec	GHA	SHA	Dec	Name	SHA	Dec
1800	86 11.8	147 53.2	S22 41.9	85 18.4	N 03.0	03.0	276 22.3	N 5 37.4	344 25.0	N22 18.2	344 25.0	N22 18.2	344 25.0	N22 18.2	344 25.0	Acamar	315 23.6	S40 17.5
01	101 14.2	162 52.4	41.4	100 19.6	03.7	03.7	291 24.6	37.4	359 27.7	18.2	359 27.7	18.2	359 27.7	18.2	359 27.7	Achernar	335 31.8	S57 13.3
02	116 16.7	177 51.6	40.8	115 20.7	04.3	04.3	306 27.0	37.4	340 30.4	18.2	340 30.4	18.2	340 30.4	18.2	340 30.4	Acrux	173 18.2	S63 06.9
03	131 19.2	192 50.7	40.3	130 21.9	05.0	05.0	321 29.3	37.2	29 33.1	18.3	29 33.1	18.3	29 33.1	18.3	29 33.1	Adhara	255 18.1	S28 58.5
04	146 21.6	207 49.9	39.7	145 21.6	05.6	05.6	336 31.6	37.2	44 35.7	18.3	44 35.7	18.3	44 35.7	18.3	44 35.7	Aldebaran	290 57.7	N16 31.1
05	161 24.1	222 49.1	39.2	160 24.2	06.3	06.3	351 34.0	37.2	59 38.4	18.3	59 38.4	18.3	59 38.4	18.3	59 38.4			
06	176 26.6	237 48.3	S22 38.6	175 25.4	N 06.9	06.9	6 36.3	N 5 37.2	74 41.1	N22 18.3	74 41.1	N22 18.3	74 41.1	N22 18.3	74 41.1	Alioth	166 27.2	N55 56.1
07	191 29.0	252 47.4	38.1	190 26.5	07.5	07.5	21 38.6	37.1	89 49.8	18.3	89 49.8	18.3	89 49.8	18.3	89 49.8	Alkaid	153 04.9	N49 17.4
08	206 31.5	267 46.6	37.5	205 27.7	08.2	08.2	36 41.0	37.1	104 46.4	18.4	104 46.4	18.4	104 46.4	18.4	104 46.4	Alnilam	275 53.6	S46 56.8
09	221 33.9	282 45.8	36.9	220 28.8	08.8	08.8	51 43.3	37.0	119 49.1	18.4	119 49.1	18.4	119 49.1	18.4	119 49.1	Alphard	218 03.3	S 40.4
10	236 36.4	297 45.0	36.4	235 30.0	09.5	09.5	66 45.7	37.0	134 51.8	18.4	134 51.8	18.4	134 51.8	18.4	134 51.8			
11	251 38.9	312 44.1	35.2	250 31.2	10.1	10.1	81 48.0	37.0	149 54.5	18.4	149 54.5	18.4	149 54.5	18.4	149 54.5			
12	266 41.3	327 43.3	S22 35.2	265 32.3	N 10.8	10.8	96 50.3	N 5 36.9	164 57.1	N22 18.4	164 57.1	N22 18.4	164 57.1	N22 18.4	164 57.1	Alphecca	126 17.6	N26 42.0
13	281 43.8	342 42.5	34.7	280 33.5	11.4	11.4	111 52.7	36.9	179 59.8	18.5	179 59.8	18.5	179 59.8	18.5	179 59.8	Alpheratz	357 51.3	N29 06.8
14	296 46.3	357 41.7	34.1	295 34.6	12.1	12.1	126 55.0	36.8	195 02.5	18.5	195 02.5	18.5	195 02.5	18.5	195 02.5	Altair	62 15.8	N 9 52.7
15	311 48.7	372 40.8	33.5	310 35.8	12.7	12.7	141 57.4	36.8	210 05.2	18.5	210 05.2	18.5	210 05.2	18.5	210 05.2	Ankaa	353 22.8	S42 17.4
16	326 51.2	383 39.0	33.0	325 36.9	13.4	13.4	156 59.7	36.8	225 07.8	18.5	225 07.8	18.5	225 07.8	18.5	225 07.8	Antares	112 35.9	S26 26.4
17	341 53.7	392 39.2	32.4	340 38.1	14.0	14.0	172 02.0	36.7	240 10.5	18.5	240 10.5	18.5	240 10.5	18.5	240 10.5			
18	356 56.1	401 38.4	S22 31.8	355 39.2	N 14.7	14.7	187 04.4	N 5 36.7	255 13.2	N22 18.6	255 13.2	N22 18.6	255 13.2	N22 18.6	255 13.2	Arcturus	146 02.7	N19 09.6
19	11 58.6	72 37.6	31.3	10 40.4	15.3	15.3	202 06.7	36.6	270 15.9	18.6	270 15.9	18.6	270 15.9	18.6	270 15.9	Atria	107 45.1	S69 02.0
20	27 01.1	87 36.7	30.7	25 41.6	15.9	15.9	217 09.1	36.6	285 18.5	18.6	285 18.5	18.6	285 18.5	18.6	285 18.5	Avior	234 20.7	S59 31.0
21	42 03.5	102 35.9	30.1	40 42.7	16.6	16.6	232 11.4	36.6	300 21.2	18.6	300 21.2	18.6	300 21.2	18.6	300 21.2	Beatrix	278 39.7	N 6 21.3
22	57 06.0	117 35.1	29.5	55 43.9	17.2	17.2	247 13.8	36.5	315 23.9	18.6	315 23.9	18.6	315 23.9	18.6	315 23.9	Belelguese	271 09.1	N 7 24.5
23	72 08.4	132 34.3	29.0	70 45.0	17.9	17.9	262 16.1	36.5	330 26.6	18.7	330 26.6	18.7	330 26.6	18.7	330 26.6			
1900	87 10.9	147 33.5	S22 28.8	85 46.2	N 18.5	18.5	277 18.4	N 5 36.4	345 29.2	N22 18.7	345 29.2	N22 18.7	345 29.2	N22 18.7	345 29.2	Canopus	263 58.9	S52 41.7
01	102 13.4	162 32.6	27.4	100 47.3	19.2	19.2	292 20.8	36.4	0 31.9	18.7	0 31.9	18.7	0 31.9	18.7	0 31.9	Capella	280 45.1	N46 00.2
02	117 15.8	177 31.8	27.2	115 48.5	19.8	19.8	307 23.1	36.4	15 34.6	18.7	15 34.6	18.7	15 34.6	18.7	15 34.6	Deneb	49 37.0	N51 17.7
03	132 18.3	192 31.0	26.6	130 49.6	20.5	20.5	322 25.5	36.3	30 37.3	18.7	30 37.3	18.7	30 37.3	18.7	30 37.3	Denebola	182 41.2	N14 33.0
04	147 20.8	207 30.2	26.1	145 50.8	21.1	21.1	337 27.8	36.3	45 39.9	18.8	45 39.9	18.8	45 39.9	18.8	45 39.9	Diphda	349 03.3	S17 58.1
05	162 23.2	222 29.4	25.5	160 51.9	21.8	21.8	352 30.2	36.2	60 42.6	18.8	60 42.6	18.8	60 42.6	18.8	60 42.6			
06	177 25.7	237 28.6	S22 24.9	175 53.1	N 22.4	22.4	7 32.5	N 5 36.2	75 45.3	N22 18.8	75 45.3	N22 18.8	75 45.3	N22 18.8	75 45.3	Dubhe	194 00.4	N61 43.6
07	192 28.2	252 27.7	24.3	190 54.3	23.1	23.1	22 34.8	36.2	90 48.0	18.8	90 48.0	18.8	90 48.0	18.8	90 48.0	Elath	278 21.7	N28 36.7
08	207 30.6	267 26.9	23.7	205 55.4	23.7	23.7	37 37.2	36.1	105 50.6	18.8	105 50.6	18.8	105 50.6	18.8	105 50.6	Eltanin	90 50.2	N51 29.2
09	222 33.1	282 26.1	23.1	220 56.6	24.4	24.4	52 39.5	36.1	120 53.3	18.9	120 53.3	18.9	120 53.3	18.9	120 53.3	Enif	33 54.7	N 9 53.5
10	237 35.6	297 25.3	22.5	235 57.7	25.0	25.0	67 41.9	36.1	135 56.0	18.9	135 56.0	18.9	135 56.0	18.9	135 56.0	Fomalhaut	15 32.2	S29 36.3
11	252 38.0	312 24.5	22.0	250 58.9	25.6	25.6	82 44.2	36.0	150 58.7	18.9	150 58.7	18.9	150 58.7	18.9	150 58.7			
12	267 40.5	327 23.7	S22 21.4	266 00.0	N 26.3	26.3	97 46.6	N 5 36.0	166 01.3	N22 18.9	166 01.3	N22 18.9	166 01.3	N22 18.9	166 01.3	Gacrux	172 09.7	S57 07.8
13	282 42.9	342 22.9	20.8	281 01.2	26.9	26.9	112 48.9	35.9	181 04.0	18.9	181 04.0	18.9	181 04.0	18.9	181 04.0	Gienah	176 00.1	S17 33.6
14	297 45.4	357 21.1	20.2	296 02.3	27.6	27.6	127 51.3	35.9	196 06.7	18.9	196 06.7	18.9	196 06.7	18.9	196 06.7	Hadar	148 59.2	S60 23.2
15	312 47.9	372 12.1	19.6	311 03.5	28.2	28.2	142 53.6	35.9	211 09.4	19.0	211 09.4	19.0	211 09.4	19.0	211 09.4	Hamal	328 09.1	N23 29.1
16	327 50.3	382 10.4	19.0	326 04.6	28.9	28.9	157 56.0	35.8	226 12.1	19.0	226 12.1	19.0	226 12.1	19.0	226 12.1	Kaus Aust.	83 54.1	S34 23.1
17	342 52.8	392 08.4	18.4	341 05.8	29.5	29.5	172 58.3	35.8	241 14.7	19.0	241 14.7	19.0	241 14.7	19.0	241 14.7			
18	357 55.3	401 07.8	S22 17.8	356 06.9	N 30.2	30.2	188 00.7	N 5 35.8	256 17.4	N22 19.0	256 17.4	N22 19.0	256 17.4	N22 19.0	256 17.4	Kochab	137 20.2	N74 08.1
19	12 57.7	72 18.0	17.2	11 08.1	30.8	30.8	203 03.0	35.7	271 20.1	19.0	271 20.1	19.0	271 20.1	19.0	271 20.1	Markab	13 45.9	N15 13.6
20	28 00.2	87 17.2	16.6	26 09.2	31.5	31.5	218 05.4	35.7	286 22.8	19.1	286 22.8	19.1	286 22.8	19.1	286 22.8	Menkar	314 22.6	N 4 06.3
21	43 02.7	102 16.4	16.0	41 10.4	32.1	32.1	233 07.7	35.6	301 25.4	19.1	301 25.4	19.1	301 25.4	19.1	301 25.4	Menkent	148 16.8	S36 23.2
22	58 05.1	117 15.6	15.4	56 11.5	32.8	32.8	248 10.1	35.6	316 28.1	19.1	316 28.1	19.1	316 28.1	19.1	316 28.1	Miaplacidus	221 41.0	S69 43.6
23	73 07.6	132 14.8	14.8	71 12.7	33.4	33.4	263 12.4	35.6	331 30.8	19.1	331 30.8	19.1	331 30.8	19.1	331 30.8			
2000	88 10.0	147 14.0	S22 14.2	86 13.8	N 34.1	34.1	278 14.8	N 5 35.5	346 33.5	N22 19.1	346 33.5	N22 19.1	346 33.5	N22 19.1	346 33.5	Mirafak	308 50.8	N49 52.7
01	103 12.5	162 13.2	13.6	101 15.0	34.7	34.7	293 17.1	35.5	1 36.1	19.2	1 36.1	19.2	1 36.1	19.2	1 36.1	Nunki	76 07.9	S26 17.6
02	118 15.0	177 12.4	13.0	116 16.1	35.3	35.3	308 19.5	35.5	16 38.8	19.2	16 38.8	19.2	16 38.8	19.2	16 38.8	Peacock	53 31.3	S56 43.6
03	133 17.4	192 11.6	12.3	131 17.3	36.0	36.0	323 21.8	35.4	31 41.5	19.2	31 41.5	19.2	31 41.5	19.2	31 41.5	Pollux	243 36.5	N28 01.0
04	148 19.9	207 10.8	11.7	146 18.4	36.6	36.6	33											



POLARIS (POLE STAR) TABLES, 2003  
FOR DETERMINING LATITUDE FROM SEXTANT ALTITUDE AND FOR AZIMUTH

LHA ARIES	0° - 9°	10° - 19°	20° - 29°	30° - 39°	40° - 49°	50° - 59°	60° - 69°	70° - 79°	80° - 89°	90° - 99°	100° - 109°	110° - 119°
0	25.3	21.0	17.9	16.1	15.6	16.4	18.6	21.9	26.4	31.9	38.2	45.2
1	24.8	20.7	17.7	16.0	15.6	16.6	18.8	22.3	26.9	32.5	38.9	45.9
2	24.3	20.3	17.5	15.9	15.7	16.8	19.1	22.7	27.5	33.1	39.6	46.6
3	23.9	20.0	17.3	15.8	15.7	16.9	19.5	23.2	28.0	33.7	40.3	47.3
4	23.4	19.6	17.1	15.8	15.8	17.1	19.8	23.6	28.5	34.4	40.9	48.1
5	23.0	19.3	16.9	15.7	15.9	17.3	20.1	24.1	29.1	35.0	41.6	48.8
6	22.6	19.0	16.7	15.7	15.9	17.6	20.4	24.5	29.6	35.6	42.3	49.5
7	22.2	18.7	16.5	15.6	16.0	17.8	20.8	25.0	30.2	36.3	43.0	50.3
8	21.8	18.5	16.4	15.6	16.2	18.0	21.2	25.5	30.8	36.9	43.7	51.0
9	21.4	18.2	16.2	15.6	16.3	18.3	21.5	25.9	31.3	37.6	44.5	51.8
10	21.0	17.9	16.1	15.6	16.4	18.6	21.9	26.4	31.9	38.2	45.2	52.5
Lat.	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$
0	0.5	0.5	0.6	0.6	0.6	0.6	0.5	0.5	0.4	0.4	0.3	0.3
10	0.5	0.6	0.6	0.6	0.6	0.6	0.5	0.5	0.4	0.4	0.4	0.3
20	0.5	0.6	0.6	0.6	0.6	0.6	0.5	0.5	0.4	0.4	0.4	0.3
30	0.5	0.6	0.6	0.6	0.6	0.6	0.5	0.5	0.4	0.4	0.4	0.3
40	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.5	0.5	0.5	0.5
45	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
50	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
55	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
60	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
62	0.7	0.6	0.6	0.6	0.6	0.6	0.6	0.7	0.7	0.7	0.8	0.8
64	0.7	0.6	0.6	0.6	0.6	0.6	0.6	0.7	0.7	0.7	0.8	0.8
66	0.7	0.6	0.6	0.6	0.6	0.6	0.6	0.7	0.7	0.7	0.8	0.8
68	0.7	0.7	0.6	0.6	0.6	0.6	0.7	0.7	0.8	0.8	0.9	0.9
Month	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$
Jan.	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.6
Feb.	0.6	0.7	0.7	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8
Mar.	0.5	0.5	0.6	0.6	0.7	0.7	0.8	0.8	0.9	0.9	0.9	0.9
Apr.	0.3	0.4	0.5	0.5	0.6	0.6	0.7	0.8	0.8	0.9	0.9	0.9
May	0.2	0.3	0.4	0.4	0.5	0.6	0.6	0.7	0.8	0.8	0.8	0.9
June	0.2	0.2	0.2	0.3	0.3	0.4	0.4	0.5	0.6	0.6	0.7	0.8
July	0.3	0.2	0.2	0.2	0.3	0.3	0.3	0.4	0.4	0.5	0.5	0.6
Aug.	0.4	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.4	0.4	0.4	0.4
Sept.	0.6	0.5	0.5	0.4	0.4	0.3	0.3	0.3	0.3	0.3	0.3	0.3
Oct.	0.8	0.7	0.6	0.6	0.5	0.5	0.4	0.4	0.3	0.3	0.3	0.3
Nov.	0.9	0.9	0.8	0.8	0.7	0.6	0.5	0.4	0.4	0.4	0.3	0.3
Dec.	1.0	1.0	1.0	0.9	0.9	0.8	0.7	0.7	0.6	0.5	0.4	0.4
Lat.	AZIMUTH											
0	0.4	0.3	0.2	0.0	359.9	359.8	359.7	359.6	359.5	359.4	359.3	359.3
20	0.4	0.3	0.2	0.1	359.9	359.8	359.7	359.5	359.4	359.3	359.3	359.3
40	0.5	0.4	0.2	0.1	359.9	359.7	359.6	359.4	359.3	359.2	359.1	359.1
50	0.6	0.5	0.3	0.1	359.9	359.7	359.5	359.3	359.2	359.1	359.0	358.9
55	0.7	0.5	0.3	0.1	359.9	359.6	359.4	359.2	359.1	358.9	358.8	358.8
60	0.8	0.6	0.4	0.1	359.8	359.6	359.4	359.1	358.9	358.8	358.7	358.6
65	1.0	0.7	0.4	0.1	359.8	359.5	359.2	359.0	358.7	358.6	358.4	358.3

Latitude = Apparent altitude (corrected for refraction) -  $1^\circ + a_0 + a_1 + a_2$

The table is entered with LHA Aries to determine the column to be used; each column refers to a range of  $10^\circ$ .  $a_0$  is taken, with mental interpolation, from the upper table with the units of LHA Aries in degrees as argument;  $a_1$ ,  $a_2$  are taken, without interpolation, from the second and third tables with arguments latitude and month respectively.  $a_0$ ,  $a_1$ ,  $a_2$ , are always positive. The final table gives the azimuth of *Polaris*.

POLARIS (POLE STAR) TABLES, 2003  
FOR DETERMINING LATITUDE FROM SEXTANT ALTITUDE AND FOR AZIMUTH

LHA ARIES	120° - 129°	130° - 139°	140° - 149°	150° - 159°	160° - 169°	170° - 179°	180° - 189°	190° - 199°	200° - 209°	210° - 219°	220° - 229°	230° - 239°
0	52.5	00.0	07.5	14.7	21.4	27.4	32.6	36.7	39.7	41.5	42.0	41.2
1	53.3	00.8	08.2	15.4	22.1	28.0	33.1	37.1	40.0	41.6	42.0	41.0
2	54.0	01.5	09.0	16.1	22.7	28.5	33.5	37.4	40.2	41.7	41.9	40.9
3	54.8	02.3	09.7	16.8	23.3	29.1	33.9	37.8	40.4	41.8	41.9	40.7
4	55.5	03.0	10.4	17.5	23.9	29.6	34.4	38.1	40.6	41.9	41.8	40.5
5	56.3	03.8	11.2	18.1	24.5	30.1	34.8	38.4	40.8	41.9	41.8	40.3
6	57.0	04.5	11.9	18.8	25.1	30.6	35.2	38.7	40.9	41.9	41.7	40.1
7	57.8	05.3	12.6	19.5	25.7	31.1	35.6	39.0	41.1	42.0	41.6	39.9
8	58.5	06.0	13.3	20.1	26.3	31.6	36.0	39.2	41.2	42.0	41.5	39.6
9	59.3	06.8	14.0	20.8	26.9	32.1	36.4	39.5	41.4	42.0	41.3	39.4
10	00.0	07.5	14.7	21.4	27.4	32.6	36.7	39.7	41.5	42.0	41.2	39.1
Lat.	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$	$a_1$
0	0.3	0.3	0.3	0.3	0.4	0.4	0.5	0.5	0.6	0.6	0.6	0.6
10	0.3	0.3	0.3	0.3	0.4	0.4	0.5	0.5	0.6	0.6	0.6	0.6
20	0.4	0.4	0.4	0.4	0.5	0.5	0.6	0.6	0.6	0.6	0.6	0.6
30	0.4	0.4	0.4	0.4	0.5	0.5	0.6	0.6	0.6	0.6	0.6	0.6
40	0.5	0.5	0.5	0.5	0.5	0.6	0.6	0.6	0.6	0.6	0.6	0.6
45	0.5	0.5	0.5	0.5	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
50	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
55	0.7	0.7	0.7	0.7	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
60	0.7	0.7	0.7	0.7	0.7	0.7	0.6	0.6	0.6	0.6	0.6	0.6
62	0.8	0.8	0.8	0.8	0.7	0.7	0.6	0.6	0.6	0.6	0.6	0.6
64	0.8	0.8	0.8	0.8	0.8	0.7	0.6	0.6	0.6	0.6	0.6	0.6
66	0.9	0.9	0.9	0.8	0.8	0.7	0.6	0.6	0.6	0.6	0.6	0.6
68	0.9	0.9	0.9	0.9	0.8	0.8	0.7	0.7	0.6	0.6	0.6	0.6
Month	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$	$a_2$
Jan.	0.6	0.6	0.6	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
Feb.	0.8	0.7	0.7	0.7	0.6	0.6	0.6	0.5	0.5	0.5	0.4	0.4
Mar.	0.9	0.9	0.9	0.8	0.8	0.8	0.7	0.7	0.6	0.6	0.5	0.5
Apr.	1.0	1.0	1.0	1.0	0.9	0.9	0.9	0.8	0.7	0.7	0.6	0.6
May	0.9	1.0	1.0	1.0	1.0	1.0	1.0	0.9	0.9	0.8	0.8	0.7
June	0.8	0.9	0.9	0.9	1.0	1.0	1.0	1.0	0.9	0.9	0.9	0.8
July	0.7	0.7	0.8	0.8	0.9	0.9	0.9	1.0	1.0	1.0	0.9	0.9
Aug.	0.5	0.6	0.6	0.7	0.7	0.8	0.8	0.9	0.9	0.9	0.9	0.9
Sept.	0.4	0.4	0.4	0.5	0.5	0.6	0.6	0.7	0.7	0.8	0.8	0.9
Oct.	0.3	0.3	0.3	0.3	0.4	0.4	0.4	0.5	0.6	0.6	0.7	0.7
Nov.	0.2	0.2	0.2	0.2	0.2	0.2	0.3	0.3	0.4	0.4	0.5	0.6
Dec.	0.3	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.3	0.3	0.4
Lat.	AZIMUTH											
0	359.3	359.3	359.3	359.4	359.4	359.5	359.6	359.7	359.8	359.9	0.0	0.0
20	359.2	359.2	359.3	359.3	359.4	359.5	359.6	359.7	359.8	359.9	0.0	0.0
40	359.1	359.1	359.1	359.2	359.2	359.3	359.4	359.5	359.6	359.8	359.9	0.1
50	358.9	358.9	358.9	359.0	359.1	359.2	359.3	359.4	359.6	359.7	359.9	0.1
55	358.7	358.8	358.8	358.9	359.0	359.1	359.2	359.3	359.5	359.7	359.9	0.



**POLARIS (POLE STAR) TABLES, 2003**  
FOR DETERMINING LATITUDE FROM SEXTANT ALTITUDE AND FOR AZIMUTH

LHA ARIES	240° - 249°	250° - 259°	260° - 269°	270° - 279°	280° - 289°	290° - 299°	300° - 309°	310° - 319°	320° - 329°	330° - 339°	340° - 349°	350° - 359°					
	<i>a</i> <sub>0</sub>	<i>a</i> <sub>0</sub>	<i>a</i> <sub>0</sub>	<i>a</i> <sub>0</sub>	<i>a</i> <sub>0</sub>	<i>a</i> <sub>0</sub>	<i>a</i> <sub>0</sub>	<i>a</i> <sub>0</sub>	<i>a</i> <sub>0</sub>	<i>a</i> <sub>0</sub>	<i>a</i> <sub>0</sub>	<i>a</i> <sub>0</sub>					
0	39.1	35.8	31.4	26.1	19.9	13.0	05.7	0	58.2	0	50.7	0	43.5	0	36.7	0	30.5
1	38.8	35.4	30.9	25.5	19.2	12.3	05.0	57.5	50.0	42.8	36.0	30.0					
2	38.6	35.0	30.4	24.9	18.5	11.6	04.2	56.7	49.2	42.1	35.4	29.4					
3	38.3	34.6	29.9	24.3	17.9	10.9	03.5	56.0	48.5	41.4	34.7	28.8					
4	37.9	34.2	29.4	23.7	17.2	10.1	02.7	55.2	47.8	40.7	34.1	28.3					
5	37.6	33.8	28.9	23.1	16.5	09.4	02.0	54.5	47.0	40.0	33.5	27.8					
6	37.3	33.3	28.3	22.4	15.8	08.7	01.2	53.7	46.3	39.3	32.9	27.3					
7	36.9	32.9	27.8	21.8	15.1	07.9	00.5	53.0	45.6	38.6	32.3	26.7					
8	36.6	32.4	27.2	21.2	14.4	07.2	0	52.2	44.9	38.0	31.7	26.2					
9	36.2	31.9	26.6	20.5	13.7	06.5	59.0	51.5	44.2	37.3	31.1	25.7					
10	35.8	31.4	26.1	19.9	13.0	05.7	0	58.2	0	43.5	0	36.7	0	30.5	0	25.3	
Lat.	<i>a</i> <sub>1</sub>	<i>a</i> <sub>1</sub>	<i>a</i> <sub>1</sub>	<i>a</i> <sub>1</sub>	<i>a</i> <sub>1</sub>	<i>a</i> <sub>1</sub>	<i>a</i> <sub>1</sub>	<i>a</i> <sub>1</sub>	<i>a</i> <sub>1</sub>	<i>a</i> <sub>1</sub>	<i>a</i> <sub>1</sub>	<i>a</i> <sub>1</sub>					
0	0.5	0.5	0.4	0.4	0.3	0.3	0.3	0.3	0.3	0.3	0.4	0.4					
10	.5	.5	.5	.4	.4	.3	.3	.3	.3	.4	.4	.5					
20	.6	.5	.5	.4	.4	.4	.4	.4	.4	.4	.5	.5					
30	.6	.5	.5	.5	.5	.4	.4	.4	.4	.5	.5	.5					
40	0.6	0.6	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.6					
45	.6	.6	.6	.6	.6	.6	.5	.5	.6	.6	.6	.6					
50	.6	.6	.6	.6	.6	.6	.6	.6	.6	.6	.6	.6					
55	.6	.6	.6	.6	.7	.7	.7	.7	.7	.7	.6	.6					
60	.6	.7	.7	.7	.7	.7	.7	.7	.7	.7	.7	.7					
62	0.6	0.7	0.7	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.7	0.7					
64	.6	.7	.7	.8	.8	.8	.8	.8	.8	.8	.8	.7					
66	.7	.7	.7	.8	.8	.9	.9	.9	.9	.9	.8	.7					
68	0.7	0.7	0.8	0.8	0.9	0.9	0.9	0.9	0.9	0.9	0.8	0.8					
Month	<i>a</i> <sub>2</sub>	<i>a</i> <sub>2</sub>	<i>a</i> <sub>2</sub>	<i>a</i> <sub>2</sub>	<i>a</i> <sub>2</sub>	<i>a</i> <sub>2</sub>	<i>a</i> <sub>2</sub>	<i>a</i> <sub>2</sub>	<i>a</i> <sub>2</sub>	<i>a</i> <sub>2</sub>	<i>a</i> <sub>2</sub>	<i>a</i> <sub>2</sub>					
Jan.	0.5	0.5	0.5	0.5	0.5	0.6	0.6	0.6	0.6	0.6	0.7	0.7					
Feb.	.4	.4	.4	.4	.4	.4	.4	.5	.5	.5	.6	.6					
Mar.	.4	.4	.3	.3	.3	.3	.3	.3	.3	.4	.4	.4					
Apr.	0.5	0.4	0.4	0.3	0.3	0.3	0.2	0.2	0.2	0.2	0.3	0.3					
May	.6	.6	.5	.4	.4	.3	.3	.2	.2	.2	.2	.2					
June	.8	.7	.6	.6	.5	.4	.3	.3	.2	.2	.2	.2					
July	0.9	0.8	0.8	0.7	0.7	0.6	0.5	0.5	0.4	0.4	0.3	0.3					
Aug.	.9	.9	.9	.8	.8	.8	.7	.6	.6	.5	.5	.4					
Sept.	.9	.9	.9	.9	.9	.9	.8	.8	.8	.7	.7	.6					
Oct.	0.8	0.8	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.8	0.8					
Nov.	.6	.7	.8	.8	.9	.9	1.0	1.0	1.0	1.0	1.0	1.0					
Dec.	0.5	0.5	0.6	0.7	0.8	0.8	0.9	0.9	1.0	1.0	1.0	1.0					
Lat.	AZIMUTH																
0	0.3	0.4	0.5	0.6	0.7	0.7	0.7	0.7	0.7	0.6	0.6	0.5					
20	0.3	0.5	0.6	0.6	0.7	0.7	0.7	0.8	0.8	0.7	0.7	0.5					
40	0.4	0.6	0.7	0.8	0.9	0.9	0.9	0.9	0.9	0.8	0.8	0.7					
50	0.5	0.7	0.8	0.9	1.0	1.1	1.1	1.1	1.1	1.0	0.9	0.8					
55	0.5	0.7	0.9	1.0	1.1	1.2	1.3	1.3	1.2	1.1	1.0	0.9					
60	0.6	0.8	1.0	1.2	1.3	1.4	1.4	1.4	1.4	1.3	1.2	1.0					
65	0.7	1.0	1.2	1.4	1.5	1.6	1.7	1.7	1.6	1.5	1.4	1.2					

$$\text{Latitude} = \text{Apparent altitude (corrected for refraction)} - 1^\circ + a_0 + a_1 + a_2$$

The table is entered with LHA Aries to determine the column to be used; each column refers to a range of 10°. *a*<sub>0</sub> is taken, with mental interpolation, from the upper table with the units of LHA Aries in degrees as argument; *a*<sub>1</sub>, *a*<sub>2</sub> are taken, without interpolation, from the second and third tables with arguments latitude and month respectively. *a*<sub>0</sub>, *a*<sub>1</sub>, *a*<sub>2</sub>, are always positive. The final table gives the azimuth of *Polaris*.

## Increments and Corrections



INCREMENTS AND CORRECTIONS

Table with columns for SUN PLANETS, ARIES, MOON, and three columns for corrections (d, Corr<sup>n</sup>). Rows are numbered 00 to 60.

INCREMENTS AND CORRECTIONS

Table with columns for SUN PLANETS, ARIES, MOON, and three columns for corrections (d, Corr<sup>n</sup>). Rows are numbered 00 to 60.



INCREMENTS AND CORRECTIONS

4	SUN PLANETS			ARIES	MOON			v or Corr <sup>n</sup>			5	SUN PLANETS			ARIES	MOON			v or Corr <sup>n</sup>		
	o	'	"		o	'	"	o	'	"		o	'	"		o	'	"	o	'	"
00	1 000	1 002	0 573	0 0	0 0	6 0	0 5	12 0	0 9	00	1 150	1 152	1 116	0 0	0 0	6 0	0 6	12 0	1 1		
01	1 003	1 004	0 575	0 1	0 0	6 1	0 5	12 1	0 9	01	1 153	1 155	1 118	0 1	0 0	6 1	0 6	12 1	1 1		
02	1 005	1 007	0 577	0 2	0 0	6 2	0 5	12 2	0 9	02	1 155	1 157	1 121	0 2	0 0	6 2	0 6	12 2	1 1		
03	1 008	1 009	0 580	0 3	0 0	6 3	0 5	12 3	0 9	03	1 158	1 160	1 123	0 3	0 0	6 3	0 6	12 3	1 1		
04	1 010	1 012	0 582	0 4	0 0	6 4	0 5	12 4	0 9	04	1 160	1 162	1 125	0 4	0 0	6 4	0 6	12 4	1 1		
05	1 013	1 014	0 585	0 5	0 0	6 5	0 5	12 5	0 9	05	1 163	1 165	1 128	0 5	0 0	6 5	0 6	12 5	1 1		
06	1 015	1 017	0 587	0 6	0 0	6 6	0 5	12 6	0 9	06	1 165	1 167	1 130	0 6	0 1	6 6	0 6	12 6	1 2		
07	1 018	1 019	0 589	0 7	0 1	6 7	0 5	12 7	1 0	07	1 168	1 170	1 133	0 7	0 1	6 7	0 6	12 7	1 2		
08	1 020	1 022	0 592	0 8	0 1	6 8	0 5	12 8	1 0	08	1 170	1 172	1 135	0 8	0 1	6 8	0 6	12 8	1 2		
09	1 023	1 024	0 594	0 9	0 1	6 9	0 5	12 9	1 0	09	1 173	1 175	1 137	0 9	0 1	6 9	0 6	12 9	1 2		
10	1 025	1 027	0 597	1 0	0 1	7 0	0 5	13 0	1 0	10	1 175	1 177	1 140	1 0	0 1	7 0	0 6	13 0	1 2		
11	1 028	1 029	0 599	1 1	0 1	7 1	0 5	13 1	1 0	11	1 178	1 180	1 142	1 1	0 1	7 1	0 7	13 1	1 2		
12	1 030	1 032	1 001	1 2	0 1	7 2	0 5	13 2	1 0	12	1 180	1 182	1 144	1 2	0 1	7 2	0 7	13 2	1 2		
13	1 033	1 034	1 004	1 3	0 1	7 3	0 5	13 3	1 0	13	1 183	1 185	1 147	1 3	0 1	7 3	0 7	13 3	1 2		
14	1 035	1 037	1 006	1 4	0 1	7 4	0 6	13 4	1 0	14	1 185	1 187	1 149	1 4	0 1	7 4	0 7	13 4	1 2		
15	1 038	1 039	1 008	1 5	0 1	7 5	0 6	13 5	1 0	15	1 188	1 190	1 152	1 5	0 1	7 5	0 7	13 5	1 2		
16	1 040	1 042	1 011	1 6	0 1	7 6	0 6	13 6	1 0	16	1 190	1 192	1 154	1 6	0 1	7 6	0 7	13 6	1 2		
17	1 043	1 044	1 013	1 7	0 1	7 7	0 6	13 7	1 0	17	1 193	1 195	1 156	1 7	0 2	7 7	0 7	13 7	1 3		
18	1 045	1 047	1 016	1 8	0 1	7 8	0 6	13 8	1 0	18	1 195	1 197	1 159	1 8	0 2	7 8	0 7	13 8	1 3		
19	1 048	1 049	1 018	1 9	0 1	7 9	0 6	13 9	1 0	19	1 198	1 200	1 161	1 9	0 2	7 9	0 7	13 9	1 3		
20	1 050	1 052	1 020	2 0	0 2	8 0	0 6	14 0	1 1	20	1 200	1 202	1 164	2 0	0 2	8 0	0 7	14 0	1 3		
21	1 053	1 054	1 023	2 1	0 2	8 1	0 6	14 1	1 1	21	1 203	1 205	1 167	2 1	0 2	8 1	0 7	14 1	1 3		
22	1 055	1 057	1 025	2 2	0 2	8 2	0 6	14 2	1 1	22	1 205	1 207	1 168	2 2	0 2	8 2	0 8	14 2	1 3		
23	1 058	1 059	1 028	2 3	0 2	8 3	0 6	14 3	1 1	23	1 208	1 210	1 171	2 3	0 2	8 3	0 8	14 3	1 3		
24	1 060	1 062	1 030	2 4	0 2	8 4	0 6	14 4	1 1	24	1 210	1 212	1 173	2 4	0 2	8 4	0 8	14 4	1 3		
25	1 063	1 064	1 032	2 5	0 2	8 5	0 6	14 5	1 1	25	1 213	1 215	1 175	2 5	0 2	8 5	0 8	14 5	1 3		
26	1 065	1 067	1 035	2 6	0 2	8 6	0 6	14 6	1 1	26	1 215	1 217	1 178	2 6	0 2	8 6	0 8	14 6	1 3		
27	1 068	1 069	1 037	2 7	0 2	8 7	0 7	14 7	1 1	27	1 218	1 220	1 180	2 7	0 2	8 7	0 8	14 7	1 3		
28	1 070	1 072	1 039	2 8	0 2	8 8	0 7	14 8	1 1	28	1 220	1 222	1 183	2 8	0 3	8 8	0 8	14 8	1 4		
29	1 073	1 074	1 042	2 9	0 2	8 9	0 7	14 9	1 1	29	1 223	1 225	1 185	2 9	0 3	8 9	0 8	14 9	1 4		
30	1 075	1 077	1 044	3 0	0 2	9 0	0 7	15 0	1 1	30	1 225	1 227	1 187	3 0	0 3	9 0	0 8	15 0	1 4		
31	1 078	1 079	1 047	3 1	0 2	9 1	0 7	15 1	1 1	31	1 228	1 230	1 190	3 1	0 3	9 1	0 8	15 1	1 4		
32	1 080	1 082	1 049	3 2	0 2	9 2	0 7	15 2	1 1	32	1 230	1 232	1 192	3 2	0 3	9 2	0 8	15 2	1 4		
33	1 083	1 084	1 051	3 3	0 2	9 3	0 7	15 3	1 1	33	1 233	1 235	1 195	3 3	0 3	9 3	0 9	15 3	1 4		
34	1 085	1 087	1 054	3 4	0 3	9 4	0 7	15 4	1 2	34	1 235	1 237	1 197	3 4	0 3	9 4	0 9	15 4	1 4		
35	1 088	1 089	1 056	3 5	0 3	9 5	0 7	15 5	1 2	35	1 238	1 240	1 199	3 5	0 3	9 5	0 9	15 5	1 4		
36	1 090	1 092	1 059	3 6	0 3	9 6	0 7	15 6	1 2	36	1 240	1 242	1 202	3 6	0 3	9 6	0 9	15 6	1 4		
37	1 093	1 094	1 061	3 7	0 3	9 7	0 7	15 7	1 2	37	1 243	1 245	1 204	3 7	0 3	9 7	0 9	15 7	1 4		
38	1 095	1 097	1 063	3 8	0 3	9 8	0 7	15 8	1 2	38	1 245	1 247	1 207	3 8	0 3	9 8	0 9	15 8	1 4		
39	1 098	1 099	1 066	3 9	0 3	9 9	0 7	15 9	1 2	39	1 248	1 250	1 209	3 9	0 4	9 9	0 9	15 9	1 5		
40	1 100	1 102	1 068	4 0	0 3	10 0	0 8	16 0	1 2	40	1 250	1 252	1 211	4 0	0 4	10 0	0 9	16 0	1 5		
41	1 103	1 104	1 070	4 1	0 3	10 1	0 8	16 1	1 2	41	1 253	1 255	1 214	4 1	0 4	10 1	0 9	16 1	1 5		
42	1 105	1 107	1 073	4 2	0 3	10 2	0 8	16 2	1 2	42	1 255	1 257	1 216	4 2	0 4	10 2	0 9	16 2	1 5		
43	1 108	1 109	1 075	4 3	0 3	10 3	0 8	16 3	1 2	43	1 258	1 260	1 218	4 3	0 4	10 3	0 9	16 3	1 5		
44	1 110	1 112	1 078	4 4	0 3	10 4	0 8	16 4	1 2	44	1 260	1 262	1 221	4 4	0 4	10 4	1 0	16 4	1 5		
45	1 113	1 114	1 080	4 5	0 3	10 5	0 8	16 5	1 2	45	1 263	1 265	1 223	4 5	0 4	10 5	1 0	16 5	1 5		
46	1 115	1 117	1 082	4 6	0 3	10 6	0 8	16 6	1 2	46	1 265	1 267	1 226	4 6	0 4	10 6	1 0	16 6	1 5		
47	1 118	1 119	1 085	4 7	0 4	10 7	0 8	16 7	1 3	47	1 268	1 270	1 228	4 7	0 4	10 7	1 0	16 7	1 5		
48	1 120	1 122	1 087	4 8	0 4	10 8	0 8	16 8	1 3	48	1 270	1 272	1 230	4 8	0 4	10 8	1 0	16 8	1 5		
49	1 123	1 124	1 090	4 9	0 4	10 9	0 8	16 9	1 3	49	1 273	1 275	1 233	4 9	0 4	10 9	1 0	16 9	1 5		
50	1 125	1 127	1 092	5 0	0 4	11 0	0 8	17 0	1 3	50	1 275	1 277	1 235	5 0	0 5	11 0	1 0	17 0	1 6		
51	1 128	1 129	1 094	5 1	0 4	11 1	0 8	17 1	1 3	51	1 278	1 280	1 238	5 1	0 5	11 1	1 0	17 1	1 6		
52	1 130	1 132	1 097	5 2	0 4	11 2	0 8	17 2	1 3	52	1 280	1 282	1 240	5 2	0 5	11 2	1 0	17 2	1 6		
53	1 133	1 135	1 099	5 3	0 4	11 3	0 8	17 3	1 3	53	1 283	1 285	1 242	5 3	0 5	11 3	1 0	17 3	1 6		
54	1 135	1 137	1 102	5 4	0 4	11 4	0 9	17 4	1 3	54	1 285	1 287	1 245	5 4	0 5	11 4	1 0	17 4	1 6		
55	1 138	1 140	1 104	5 5	0 4	11 5	0 9	17 5	1 3	55	1 288	1 290	1 247	5 5	0 5	11 5	1 1	17 5	1 6		
56	1 140	1 142	1 106	5 6	0 4	11 6	0 9	17 6	1 3	56	1 290	1 292	1 249	5 6	0 5	11 6	1 1	17 6	1 6		
57	1 143	1 145	1 109	5 7	0 4	11 7	0 9	17 7	1 3	57	1 293	1 295	1 252	5 7	0 5	11 7	1 1	17 7	1 6		
58	1 145	1 147	1 111	5 8	0 4	11 8	0 9	17 8	1 3	58	1 295	1 297	1 254	5 8	0 5	11 8	1 1	17 8	1 6		
59	1 148	1 150	1 113	5 9	0 4	11 9	0 9	17 9	1 3	59	1 298	1 300	1 257	5 9	0 5	11 9	1 1	17 9	1 6		
60	1 150	1 152	1 116	6 0	0 5	12 0	0 9	18 0	1 4	60	1 300	1 302	1 259	6 0	0 6	12 0	1 1	18 0	1 7		

INCREMENTS AND CORRECTIONS

6	SUN PLANETS			ARIES	MOON			v or Corr <sup>n</sup>			7	SUN PLANETS			ARIES	MOON			v or Corr <sup>n</sup>		
	o	'	"		o	'	"	o	'	"		o	'	"		o	'	"	o	'	"
00	1 300	1 302	1 259	0 0	0 0	6 0	0 7	12 0	1 3	00	1 450	1 453	1 402	0 0	0 0	6 0	0 8	12 0	1 5		
01	1 303	1 305	1 261	0 1	0 0	6 1	0 7	12 1	1 3	01	1 453	1 455	1 405	0 1	0 0	6 1	0 8	12 1	1 5		
02	1 305	1 307	1 264	0 2	0 0	6 2	0 7	12 2	1 3	02	1 455	1 458	1 407	0 2	0 0	6 2	0 8	12 2	1 5		
03	1 308	1 310	1 266	0 3	0 0	6 3	0 7	12 3	1 3	03	1 458	1 460	1 409	0 3	0 0	6 3	0 8	12 3	1 5		



INCREMENTS AND CORRECTIONS

Table with columns: SUN PLANETS, ARIES, MOON, and three columns for 'or Corr<sup>n</sup>' (d, h, m). Rows 00-60.

Table with columns: SUN PLANETS, ARIES, MOON, and three columns for 'or Corr<sup>n</sup>' (d, h, m). Rows 00-60.

INCREMENTS AND CORRECTIONS

Table with columns: SUN PLANETS, ARIES, MOON, and three columns for 'or Corr<sup>n</sup>' (d, h, m). Rows 00-60.

Table with columns: SUN PLANETS, ARIES, MOON, and three columns for 'or Corr<sup>n</sup>' (d, h, m). Rows 00-60.



INCREMENTS AND CORRECTIONS

Table with columns for SUN PLANETS, ARIES, MOON, and correction values (v or d, Corr<sup>n</sup>) for rows 00 to 60.

Table with columns for SUN PLANETS, ARIES, MOON, and correction values (v or d, Corr<sup>n</sup>) for rows 00 to 60.

INCREMENTS AND CORRECTIONS

Table with columns for SUN PLANETS, ARIES, MOON, and correction values (v or d, Corr<sup>n</sup>) for rows 00 to 60.

Table with columns for SUN PLANETS, ARIES, MOON, and correction values (v or d, Corr<sup>n</sup>) for rows 00 to 60.



16	SUN PLANETS			ARIES			MOON			v or Corr <sup>n</sup>			17	SUN PLANETS			ARIES			MOON			v or Corr <sup>n</sup>		
	s	'	"	s	'	"	s	'	"	s	'	"		s	'	"	s	'	"	s	'	"	s	'	"
00	4	00	0	4	00	0	4	00	0	0	0	0	0	0	4	00	0	4	00	0	0	0	0	0	
01	4	00	3	4	00	3	4	00	3	4	9	1	0	0	4	00	3	4	00	3	4	9	1	0	0
02	4	00	5	4	00	5	4	00	5	4	9	2	0	0	4	00	5	4	00	5	4	9	2	0	0
03	4	00	8	4	00	8	4	00	8	4	9	5	0	1	4	00	8	4	00	8	4	9	5	0	1
04	4	01	0	4	01	0	4	01	0	4	0	4	0	1	4	01	0	4	01	0	4	0	4	0	1
05	4	01	3	4	01	3	4	01	3	4	0	5	0	1	4	01	3	4	01	3	4	0	5	0	1
06	4	01	5	4	01	5	4	01	5	4	0	6	0	2	4	01	5	4	01	5	4	0	6	0	2
07	4	01	8	4	01	8	4	01	8	4	0	6	7	0	4	01	8	4	01	8	4	0	6	7	0
08	4	02	0	4	02	0	4	02	0	4	0	6	8	0	4	02	0	4	02	0	4	0	6	8	0
09	4	02	3	4	02	3	4	02	3	4	0	6	9	0	4	02	3	4	02	3	4	0	6	9	0
10	4	02	5	4	02	5	4	02	5	4	0	7	0	0	4	02	5	4	02	5	4	0	7	0	0
11	4	02	8	4	02	8	4	02	8	4	0	7	1	0	4	02	8	4	02	8	4	0	7	1	0
12	4	03	0	4	03	0	4	03	0	4	0	7	2	0	4	03	0	4	03	0	4	0	7	2	0
13	4	03	3	4	03	3	4	03	3	4	0	7	3	0	4	03	3	4	03	3	4	0	7	3	0
14	4	03	5	4	03	5	4	03	5	4	0	7	4	0	4	03	5	4	03	5	4	0	7	4	0
15	4	03	8	4	03	8	4	03	8	4	0	7	5	0	4	03	8	4	03	8	4	0	7	5	0
16	4	04	0	4	04	0	4	04	0	4	0	7	6	0	4	04	0	4	04	0	4	0	7	6	0
17	4	04	3	4	04	3	4	04	3	4	0	7	7	0	4	04	3	4	04	3	4	0	7	7	0
18	4	04	5	4	04	5	4	04	5	4	0	7	8	0	4	04	5	4	04	5	4	0	7	8	0
19	4	04	8	4	04	8	4	04	8	4	0	7	9	0	4	04	8	4	04	8	4	0	7	9	0
20	4	05	0	4	05	0	4	05	0	4	0	8	0	0	4	05	0	4	05	0	4	0	8	0	0
21	4	05	3	4	05	3	4	05	3	4	0	8	1	0	4	05	3	4	05	3	4	0	8	1	0
22	4	05	5	4	05	5	4	05	5	4	0	8	2	0	4	05	5	4	05	5	4	0	8	2	0
23	4	05	8	4	05	8	4	05	8	4	0	8	3	0	4	05	8	4	05	8	4	0	8	3	0
24	4	06	0	4	06	0	4	06	0	4	0	8	4	0	4	06	0	4	06	0	4	0	8	4	0
25	4	06	3	4	06	3	4	06	3	4	0	8	5	0	4	06	3	4	06	3	4	0	8	5	0
26	4	06	5	4	06	5	4	06	5	4	0	8	6	0	4	06	5	4	06	5	4	0	8	6	0
27	4	06	8	4	06	8	4	06	8	4	0	8	7	0	4	06	8	4	06	8	4	0	8	7	0
28	4	07	0	4	07	0	4	07	0	4	0	8	8	0	4	07	0	4	07	0	4	0	8	8	0
29	4	07	3	4	07	3	4	07	3	4	0	8	9	0	4	07	3	4	07	3	4	0	8	9	0
30	4	07	5	4	07	5	4	07	5	4	0	9	0	0	4	07	5	4	07	5	4	0	9	0	0
31	4	07	8	4	07	8	4	07	8	4	0	9	1	0	4	07	8	4	07	8	4	0	9	1	0
32	4	08	0	4	08	0	4	08	0	4	0	9	2	0	4	08	0	4	08	0	4	0	9	2	0
33	4	08	3	4	08	3	4	08	3	4	0	9	3	0	4	08	3	4	08	3	4	0	9	3	0
34	4	08	5	4	08	5	4	08	5	4	0	9	4	0	4	08	5	4	08	5	4	0	9	4	0
35	4	08	8	4	08	8	4	08	8	4	0	9	5	0	4	08	8	4	08	8	4	0	9	5	0
36	4	09	0	4	09	0	4	09	0	4	0	9	6	0	4	09	0	4	09	0	4	0	9	6	0
37	4	09	3	4	09	3	4	09	3	4	0	9	7	0	4	09	3	4	09	3	4	0	9	7	0
38	4	09	5	4	09	5	4	09	5	4	0	9	8	0	4	09	5	4	09	5	4	0	9	8	0
39	4	09	8	4	09	8	4	09	8	4	0	9	9	0	4	09	8	4	09	8	4	0	9	9	0
40	4	10	0	4	10	0	4	10	0	4	0	10	0	0	4	10	0	4	10	0	4	0	10	0	0
41	4	10	3	4	10	3	4	10	3	4	0	10	1	0	4	10	3	4	10	3	4	0	10	1	0
42	4	10	5	4	10	5	4	10	5	4	0	10	2	0	4	10	5	4	10	5	4	0	10	2	0
43	4	10	8	4	10	8	4	10	8	4	0	10	3	0	4	10	8	4	10	8	4	0	10	3	0
44	4	11	0	4	11	0	4	11	0	4	0	10	4	0	4	11	0	4	11	0	4	0	10	4	0
45	4	11	3	4	11	3	4	11	3	4	0	10	5	0	4	11	3	4	11	3	4	0	10	5	0
46	4	11	5	4	11	5	4	11	5	4	0	10	6	0	4	11	5	4	11	5	4	0	10	6	0
47	4	11	8	4	11	8	4	11	8	4	0	10	7	0	4	11	8	4	11	8	4	0	10	7	0
48	4	12	0	4	12	0	4	12	0	4	0	10	8	0	4	12	0	4	12	0	4	0	10	8	0
49	4	12	3	4	12	3	4	12	3	4	0	10	9	0	4	12	3	4	12	3	4	0	10	9	0
50	4	12	5	4	12	5	4	12	5	4	0	11	0	0	4	12	5	4	12	5	4	0	11	0	0
51	4	12	8	4	12	8	4	12	8	4	0	11	1	0	4	12	8	4	12	8	4	0	11	1	0
52	4	13	0	4	13	0	4	13	0	4	0	11	2	0	4	13	0	4	13	0	4	0	11	2	0
53	4	13	3	4	13	3	4	13	3	4	0	11	3	0	4	13	3	4	13	3	4	0	11	3	0
54	4	13	5	4	13	5	4	13	5	4	0	11	4	0	4	13	5	4	13	5	4	0	11	4	0
55	4	13	8	4	13	8	4	13	8	4	0	11	5	0	4	13	8	4	13	8	4	0	11	5	0
56	4	14	0	4	14	0	4	14	0	4	0	11	6	0	4	14	0	4	14	0	4	0	11	6	0
57	4	14	3	4	14	3	4	14	3	4	0	11	7	0	4	14	3	4	14	3	4	0	11	7	0
58	4	14	5	4	14	5	4	14	5	4	0	11	8	0	4	14	5	4	14	5	4	0	11	8	0
59	4	14	8	4	14	8	4	14	8	4	0	11	9	0	4	14	8	4	14	8	4	0	11	9	0
60	4	15	0	4	15	0	4	15	0	4	0	12	0	0	4	15	0	4	15	0	4	0	12	0	0

18	SUN PLANETS			ARIES			MOON			v or Corr <sup>n</sup>			19	SUN PLANETS			ARIES			MOON			v or Corr <sup>n</sup>		
	s	'	"	s	'	"	s	'	"	s	'	"		s	'	"	s	'	"	s	'	"	s	'	"
00	4	30	0	4	30	0	4	30	0	0	0	0	0	4	30	0	4	30	0	0	0	0	0	0	
01	4	30	3	4	30	3	4	30	3	0	1	0	0	4	30	3	4	30	3	0	1	0	0	0	
02	4	30	5	4	30	5	4	30	5	0	2	0	0	4	30	5	4	30	5	0	2	0	0	0	
03	4	30	8	4	30	8	4	30	8	0	3	0	1	4	30	8	4	30	8	0	3	0	1	0	
04	4	31	0	4	31	0	4	31	0	0	4	0	1	4	31	0	4	31	0	0	4	0	1	0	
05	4	31	3	4	31	3	4	31	3	0	5	0	2	4	31	3	4	31	3	0	5	0	2	0	
06	4	31	5	4	31	5	4	31	5	0	6	0	2	4	31	5	4	31	5	0	6	0	2	0	
07	4	31	8	4	31	8	4	31	8	0	6	7	0	4	31	8	4	31	8	0	6</				



Table for 20m increments and corrections. Columns: SUN PLANETS, ARIES, MOON, and three columns of v or Corr<sup>n</sup>.

Table for 21m increments and corrections. Columns: SUN PLANETS, ARIES, MOON, and three columns of v or Corr<sup>n</sup>.

Table for 22m increments and corrections. Columns: SUN PLANETS, ARIES, MOON, and three columns of v or Corr<sup>n</sup>.

Table for 23m increments and corrections. Columns: SUN PLANETS, ARIES, MOON, and three columns of v or Corr<sup>n</sup>.



INCREMENTS AND CORRECTIONS

Table for page 24m showing astronomical data for Sun, Planets, Aries, Moon, and corrections.

Table for page 25m showing astronomical data for Sun, Planets, Aries, Moon, and corrections.

INCREMENTS AND CORRECTIONS

Table for page 26m showing astronomical data for Sun, Planets, Aries, Moon, and corrections.

Table for page 27m showing astronomical data for Sun, Planets, Aries, Moon, and corrections.



INCREMENTS AND CORRECTIONS

Table with columns for Sun Planets, Aries, Moon, and correction values (v or Corr) for various latitudes from 00 to 60 degrees.

TABLES FOR INTERPOLATING SUNRISE, MOONRISE, ETC.

TABLE I—FOR LATITUDE

Table I: Interpolating sunrise, moonrise, etc. for latitude. Includes columns for Tabular Interval and Difference between the times for consecutive latitudes.

Table I is for interpolating the L.M.T. of sunrise, twilight, moonrise, etc., for latitude. It is to be entered, in the appropriate column on the left, with the difference between true latitude and the nearest tabular latitude which is less than the true latitude; and with the argument at the top which is the nearest value of the difference between the times for the tabular latitude and the next higher one; the correction so obtained is applied to the time for the tabular latitude; the sign of the correction can be seen by inspection. It is to be noted that the interpolation is not linear, so that when using this table it is essential to take out the tabular phenomenon for the latitude less than the true latitude.

TABLE II—FOR LONGITUDE

Table II: Interpolating longitude. Includes columns for Long. East or West and Difference between the times for given date and preceding date (for east longitude) or for given date and following date (for west longitude).

Table II is for interpolating the L.M.T. of moonrise, moonset and the Moon's meridian passage for longitude. It is entered with longitude and with the difference between the times for the given date and for the preceding date (in east longitudes) or following date (in west longitudes). The correction is normally added for west longitudes and subtracted for east longitudes, but if, as occasionally happens, the times become earlier each day instead of later, the signs of the corrections must be reversed.



ALTITUDE CORRECTION TABLES 0°-35°— MOON

App. Alt.	0°-4°	5°-9°	10°-14°	15°-19°	20°-24°	25°-29°	30°-34°	App. Alt.
	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	
00	0	5	10	15	20	25	30	00
10	33.8	58.2	62.1	62.8	62.1	60.8	58.8	10
20	37.8	58.7	62.2	62.8	62.1	60.7	58.8	20
30	39.6	58.9	62.3	62.8	62.1	60.7	58.7	30
40	41.2	59.1	62.3	62.8	62.0	60.6	58.6	40
50	42.6	59.3	62.4	62.7	62.0	60.6	58.5	50
00	1	6	11	16	21	26	31	00
10	44.0	59.5	62.4	62.7	62.0	60.5	58.5	10
20	45.2	59.7	62.4	62.7	61.9	60.4	58.4	20
30	46.3	59.9	62.5	62.7	61.9	60.4	58.3	30
40	47.3	60.0	62.5	62.7	61.9	60.3	58.2	40
50	48.3	60.2	62.5	62.7	61.8	60.3	58.2	50
00	2	7	12	17	22	27	32	00
10	50.0	60.5	62.6	62.6	61.7	60.1	58.0	10
20	50.8	60.6	62.6	62.6	61.7	60.1	57.9	20
30	51.4	60.7	62.6	62.6	61.6	60.0	57.8	30
40	52.1	60.9	62.7	62.6	61.6	59.9	57.8	40
50	52.7	61.0	62.7	62.6	61.5	59.9	57.7	50
00	3	8	13	18	23	28	33	00
10	53.3	61.1	62.7	62.6	61.5	59.8	57.6	10
20	53.8	61.2	62.7	62.5	61.4	59.7	57.4	20
30	54.3	61.3	62.7	62.5	61.4	59.6	57.4	30
40	54.8	61.4	62.7	62.5	61.4	59.6	57.4	40
50	55.2	61.5	62.8	62.5	61.3	59.6	57.3	50
00	4	9	14	19	24	29	34	00
10	55.6	61.6	62.8	62.4	61.2	59.5	57.2	10
20	56.0	61.6	62.8	62.4	61.2	59.4	57.1	20
30	56.4	61.7	62.8	62.3	61.1	59.3	57.0	30
40	56.7	61.8	62.8	62.3	61.1	59.2	56.9	40
50	57.1	61.9	62.8	62.3	61.1	59.2	56.9	50
00	5	10	15	20	25	30	35	00
10	57.4	61.9	62.8	62.3	61.0	59.1	56.8	10
20	57.4	61.9	62.8	62.3	61.0	59.1	56.8	20
30	57.4	61.9	62.8	62.3	61.0	59.1	56.8	30
40	57.7	62.0	62.8	62.2	60.9	59.1	56.7	40
50	57.9	62.1	62.8	62.2	60.9	59.0	56.6	50
HP	L U	L U	L U	L U	L U	L U	L U	HP
54.0	0.3 0.9	0.3 0.9	0.4 1.0	0.5 1.1	0.6 1.2	0.7 1.3	0.9 1.5	54.0
54.3	0.7 1.1	0.7 1.2	0.7 1.2	0.8 1.3	0.9 1.4	1.1 1.5	1.2 1.7	54.3
54.6	1.1 1.4	1.1 1.4	1.1 1.4	1.2 1.5	1.3 1.6	1.4 1.7	1.5 1.8	54.6
54.9	1.4 1.6	1.5 1.6	1.5 1.6	1.6 1.7	1.6 1.8	1.8 1.9	1.9 2.0	54.9
55.2	1.8 1.8	1.8 1.8	1.9 1.9	1.9 1.9	2.0 2.0	2.1 2.1	2.2 2.2	55.2
55.5	2.2 2.0	2.2 2.0	2.3 2.1	2.3 2.1	2.4 2.2	2.4 2.3	2.5 2.4	55.5
55.8	2.6 2.2	2.6 2.2	2.6 2.3	2.7 2.3	2.7 2.4	2.8 2.4	2.9 2.5	55.8
56.1	3.0 2.4	3.0 2.5	3.0 2.5	3.0 2.5	3.1 2.6	3.1 2.6	3.2 2.7	56.1
56.4	3.4 2.7	3.4 2.7	3.4 2.7	3.4 2.7	3.4 2.8	3.5 2.8	3.5 2.9	56.4
56.7	3.7 2.9	3.7 2.9	3.8 2.9	3.8 2.9	3.8 3.0	3.9 3.0	3.9 3.0	56.7
57.0	4.1 3.1	4.1 3.1	4.1 3.1	4.1 3.1	4.2 3.1	4.2 3.2	4.2 3.2	57.0
57.3	4.5 3.3	4.5 3.3	4.5 3.3	4.5 3.3	4.5 3.3	4.5 3.4	4.6 3.4	57.3
57.6	4.9 3.5	4.9 3.5	4.9 3.5	4.9 3.5	4.9 3.5	4.9 3.5	4.9 3.6	57.6
57.9	5.3 3.8	5.3 3.8	5.2 3.8	5.2 3.8	5.2 3.7	5.2 3.7	5.2 3.7	57.9
58.2	5.6 4.0	5.6 4.0	5.6 4.0	5.6 4.0	5.6 3.9	5.6 3.9	5.6 3.9	58.2
58.5	6.0 4.2	6.0 4.2	6.0 4.2	6.0 4.2	6.0 4.1	5.9 4.1	5.9 4.1	58.5
58.8	6.4 4.4	6.4 4.4	6.4 4.4	6.3 4.4	6.3 4.3	6.2 4.2	6.2 4.2	58.8
59.1	6.8 4.6	6.8 4.6	6.7 4.6	6.7 4.6	6.7 4.5	6.6 4.5	6.6 4.4	59.1
59.4	7.2 4.8	7.1 4.8	7.1 4.8	7.1 4.8	7.0 4.7	7.0 4.7	6.9 4.6	59.4
59.7	7.5 5.1	7.5 5.0	7.5 5.0	7.5 5.0	7.4 4.9	7.3 4.8	7.2 4.7	59.7
60.0	7.9 5.3	7.9 5.3	7.9 5.2	7.8 5.2	7.8 5.1	7.7 5.0	7.6 4.9	60.0
60.3	8.3 5.5	8.3 5.5	8.2 5.4	8.2 5.4	8.1 5.3	8.0 5.2	7.9 5.1	60.3
60.6	8.7 5.7	8.7 5.7	8.6 5.7	8.6 5.6	8.5 5.5	8.4 5.4	8.2 5.3	60.6
60.9	9.1 5.9	9.0 5.9	9.0 5.9	8.9 5.8	8.8 5.7	8.7 5.6	8.6 5.4	60.9
61.2	9.5 6.2	9.4 6.1	9.4 6.1	9.3 6.0	9.2 5.9	9.1 5.8	8.9 5.6	61.2
61.5	9.8 6.4	9.8 6.3	9.7 6.3	9.7 6.2	9.5 6.1	9.4 5.9	9.2 5.8	61.5

DIP					
Ht. of Eye		Corr <sup>n</sup>		Ht. of Eye	
m	ft.	m	ft.	m	ft.
2.4	2.4	8.0	9.5	5.5	31.5
2.6	-2.9	8.6	9.9	-5.5	32.7
3.0	-3.0	9.2	10.3	-5.7	33.9
3.2	-3.1	10.5	11.0	-5.8	35.1
3.4	-3.3	11.2	11.4	-6.0	37.6
3.6	-3.4	11.9	11.8	-6.1	38.9
3.8	-3.4	12.6	12.2	-6.1	40.1
4.0	-3.5	13.3	12.6	-6.2	41.5
4.3	-3.7	14.1	13.0	-6.3	42.8
4.5	-3.7	14.9	13.4	-6.4	44.2
4.7	-3.8	15.7	13.8	-6.5	45.5
5.0	-3.9	16.5	14.2	-6.6	46.9
5.2	-4.0	17.4	14.7	-6.7	48.4
5.5	-4.1	18.3	15.1	-6.8	49.8
5.8	-4.2	19.1	15.5	-6.9	51.3
6.1	-4.4	20.1	16.0	-7.1	52.8
6.3	-4.4	21.0	16.5	-7.1	54.3
6.6	-4.5	22.0	16.9	-7.2	55.8
6.9	-4.6	22.9	17.4	-7.3	57.4
7.2	-4.7	23.9	17.9	-7.4	58.9
7.5	-4.8	24.9	18.4	-7.5	60.5
7.9	-4.9	26.0	18.8	-7.6	62.1
8.2	-5.0	27.1	19.3	-7.7	63.8
8.5	-5.1	28.1	19.8	-7.8	65.4
8.8	-5.2	29.2	20.4	-7.9	67.1
9.2	-5.3	30.4	20.9	-8.0	68.8
9.5	-5.4	31.5	21.4	-8.1	70.5

MOON CORRECTION TABLE

The correction is in two parts; the first correction is taken from the upper part of the table with argument apparent altitude, and the second from the lower part, with argument HP, in the same column as that from which the first correction was taken. Separate corrections are given in the lower part for lower (L) and upper (U) limbs. All corrections are to be added to apparent altitude, but 30' is to be subtracted from the altitude of the upper limb.

For corrections for pressure and temperature see page A4.

For bubble sextant observations ignore dip, take the mean of upper and lower limb corrections and subtract 15' from the altitude.

App. Alt. = Apparent altitude  
= Sextant altitude corrected for index error and dip.

ALTITUDE CORRECTION TABLES 35°-90°— MOON

App. Alt.	35°-39°	40°-44°	45°-49°	50°-54°	55°-59°	60°-64°	65°-69°	70°-74°	75°-79°	80°-84°	85°-89°	App. Alt.
	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	Corr <sup>n</sup>	
00	35	40	45	50	55	60	65	70	75	80	85	00
10	56.5	53.7	50.5	46.9	43.1	38.9	34.6	30.1	25.3	20.5	15.6	10
20	56.4	53.6	50.4	46.8	42.9	38.8	34.4	29.9	25.2	20.4	15.5	20
30	56.3	53.5	50.2	46.7	42.8	38.7	34.3	29.7	25.0	20.2	15.3	30
40	56.2	53.3	50.0	46.5	42.7	38.5	34.1	29.6	24.9	20.0	15.1	40
50	56.1	53.2	49.9	46.3	42.4	38.2	33.8	29.3	24.5	19.7	14.8	50
00	36	41	46	51	56	61	66	71	76	81	86	00
10	56.0	53.1	49.8	46.2	42.3	38.1	33.7	29.1	24.4	19.6	14.6	10
20	55.9	53.0	49.7	46.0	42.1	37.9	33.5	29.0	24.2	19.4	14.5	20
30	55.8	52.8	49.5	45.9	42.0	37.8	33.4	28.8	24.1	19.2	14.3	30
40	55.7	52.7	49.4	45.8	41.8	37.7	33.2	28.7	23.9	19.1	14.1	40
50	55.6	52.6	49.3	45.7	41.7	37.5	33.1	28.5	23.8	18.9	14.0	50
00	37	42	47	52	57	62	67	72	77	82	87	00
10	55.5	52.5	49.2	45.5	41.6	37.4	32.9	28.3	23.6	18.7	13.8	10
20	55.4	52.4	49.1	45.4	41.4	37.2	32.8	28.2	23.4	18.6	13.7	20
30	55.3	52.3	49.0	45.3	41.3	37.1	32.6	28.0	23.3	18.4	13.5	30
40	55.2	52.2	48.8	45.2	41.2	36.9	32.5	27.9	23.1	18.2	13.3	40
50	55.1	52.1	48.7	45.0	41.0	36.8	32.3	27.7	22.9	18.1	13.2	50
00	38	43	48	53	58	63	68	73	78	83	88	00
10	55.0	52.0	48.6	44.9	40.9	36.6	32.2	27.6	22.8	17.9	13.0	10
20	55.0	51.9	48.5	44.8	40.8	36.5	32.0	27.4	22.6	17.8	12.8	20
30	54.9	51.8	48.4	44.6	40.6	36.4	31.9	27.2	22.5	17.6	12.7	30
40	54.8	51.7	48.2	44.5	40.5	36.2	31.7	27.1	22.3	17.4	12.5	40
50	54.7	51.6	48.1	44.4	40.3	36.1	31.6	26.9	22.1	17.3	12.3	50
00	39	44	49	54	59	64	69	74	79	84	89	00
10	54.6	51.5	48.0	44.2	40.2	35.9	31.4	26.8	22.0	17.1	12.2	10
20	54.5	51.4	47.9	44.1	40.1	35.8	31.3	26.6	21.8	16.9	12.0	20
30	54.4	51.2	47.8	44.0	39.9	35.6	31.1	26.5	21.7	16.8	11.8	30
40	54.3	51.1	47.6	43.9	39.8	35.5	31.0	26.3	21.5	16.6	11.7	40
50	54.2	51.0	47.5	43.7	39.6	35.3	30.8	26.1	21.3	16.5	11.5	50
00	40	45	50	55	60	65	70	75	80	85	90	00
10	54.1	50.9	47.4	43.6	39.5	35.2	30.7	26.0	21.2	16.3	11.4	10
20	54.0	50.8	47.3	43.5	39.4	35.0	30.5	25.8	21.0	16.1	11.2	20
30	53.9	50.7	47.2	43.3	39.2	34.9	30.4	25.7	20.9	16.0	11.0	30
40	53.8	50.6										



**Extracts from  
the  
Admiralty Tide Tables  
Volume I**

Extracts from the Admiralty Tide Tables (Vol. I) 2002 are published by permission of the Hydrographer to the Navy.





WALES; ENGLAND, WEST COAST

No.	PLACE	Lat. N	Long. W	TIME DIFFERENCES				HEIGHT DIFFERENCES (IN METRES)				ML Z <sub>0</sub> m
				High Water Zone UT(GMT)	Low Water	High Water	Low Water	MHWS	MHWN	MLWN	MLWS	
523	PORT OF BRISTOL (AVONMOUTH)	(see page 162)		0600 and 1800	1100 and 2300	0300 and 1500	0800 and 2000	13.2	9.8	3.8	1.0	
513	Barry	51 23	3 18	-0030	-0015	-0125	-0030	-1.8	-1.3	+0.2	0.0	6.09
513a	Flat Holm	51 23	3 07	-0015	-0015	-0045	-0045	-1.3	-1.1	-0.2	+0.2	6.2
513b	Steep Holm	51 20	3 06	-0020	-0020	-0050	-0050	-1.6	-1.2	-0.2	-0.2	6.1
514	Cardiff	51 27	3 09	-0015	-0015	-0100	-0030	-1.0	-0.6	+0.1	0.0	6.45
515	Newport	51 33	2 59	-0020	-0010	0000	-0020	-1.1	-1.0	-0.6	-0.7	6.03
516	River Wye Chepstow	51 39	2 40	+0020	+0020	0	0	0	0	0	0	0
523	PORT OF BRISTOL (AVONMOUTH)	(see page 162)		0000 and 1200	0600 and 1800	0000 and 1200	0700 and 1900	13.2	9.8	3.8	1.0	
England												
517	River Severn Sudbrook	51 35	2 43	+0010	+0010	+0025	+0015	+0.2	+0.1	-0.1	+0.1	6.66
518	Beachley (Aust)	51 36	2 38	+0010	+0015	+0040	+0025	-0.2	-0.2	-0.5	-0.3	6.42
519	Inward Rocks	51 39	2 37	+0020	+0020	+0105	+0045	-1.0	-1.1	-1.4	-0.6	5.74
520	Nariwood Rocks	51 39	2 36	+0025	+0025	+0120	+0100	-1.9	-2.0	-2.3	-0.8	0
521	White House	51 40	2 33	+0025	+0025	+0145	+0120	-3.0	-3.1	-3.6	-1.0	3.94
522	Berkeley	51 42	2 30	+0030	+0045	+0245	+0220	-3.8	-3.9	-3.4	-0.5	3.44
522a	Sharpness Dock	51 43	2 29	+0035	+0050	+0305	+0245	-3.9	-4.2	-3.3	-0.4	0
522b	Wellhouse Rock	51 44	2 29	+0040	+0055	+0320	+0305	-4.1	-4.4	-3.1	-0.2	3.25
522c	Epney	51 42	2 24	+0130	0	0	0	-9.4	0	0	0	0
522d	Minsterworth	51 50	2 23	+0140	0	0	0	-10.1	0	0	0	0
522e	Llanthony	51 51	2 21	+0215	0	0	0	-10.7	0	0	0	0
523	PORT OF BRISTOL (AVONMOUTH) (Royal Portbury Dock)	(see page 162)		0200 and 1400	0800 and 2000	0300 and 1500	0800 and 2000	13.2	9.8	3.8	1.0	6.95
River Avon												
523a	Shirehampton	51 29	2 41	0000	0000	+0035	+0010	-0.7	-0.7	-0.8	0.0	0
523b	Sea Mills	51 29	2 39	+0005	+0005	+0105	+0030	-1.4	-1.5	-1.7	-0.1	0
524	Cumberland Basin Entrance	51 27	2 37	+0010	+0010	0	0	-2.9	-3.0	0	0	0
524a	Portishead	51 30	2 45	-0002	0000	0	0	-0.1	-0.1	0	0	0
525	Clevedon	51 27	2 52	-0010	-0020	-0025	-0015	-0.4	-0.2	+0.2	0.0	6.8
525a	St. Thomas Head	51 24	2 56	0000	0000	-0030	-0030	-0.4	-0.2	+0.1	+0.1	6.7
526	English And Welsh Grounds	51 28	2 59	-0008	-0008	-0030	-0030	-0.5	-0.8	-0.3	0.0	6.5
527	Weston-super-Mare	51 21	2 59	-0020	-0030	-0130	-0030	-1.2	-1.0	-0.8	-0.2	6.1
River Parrett												
528	Burnham-on-Sea	51 14	3 00	-0020	-0025	-0030	0000	-2.3	-1.9	-1.4	-1.1f	0
529	Bridgwater	51 08	3 00	-0015	-0030	+0305	+0455	-8.6	-8.1	0	0	0
530	Hinkley Point	51 13	3 08	-0020	-0025	-0100	-0040	-1.7	-1.4	-0.2	-0.2	6.0
531	Watchet	51 11	3 20	-0035	-0050	-0145	-0040	-1.9	-1.5	+0.1	+0.1	5.87
532	Minehead	51 13	3 28	-0037	-0052	-0155	-0045	-2.6	-1.9	-0.2	0.0	5.71
533	Porlock Bay	51 13	3 38	-0045	-0055	-0205	-0050	-3.0	-2.2	-0.1	-0.1	5.62
534	Lynmouth	51 14	3 49	-0055	-0115	0	0	-3.6	-2.7	0	0	0
496	MILFORD HAVEN	(see page 154)		0100 and 1300	0700 and 1900	0100 and 1300	0700 and 1900	7.0	5.2	2.5	0.7	
535	Ilfracombe	51 13	4 07	-0016	-0016	-0041	-0031	+2.3	+1.8	+0.6	+0.3	5.04
Rivers Taw and Torridge												
536	Appledore	51 03	4 12	-0020	-0025	-0015	-0045	+0.5	0.0	-0.9	-0.5	3.68
537	Yelland Marsh	51 04	4 10	-0010	-0015	+0100	-0015	-0.4	-0.4	-1.2	-0.2	3.02
538	Fremington	51 05	4 07	-0010	-0015	+0030	-0030	-1.1	-1.8	-2.2	-0.5	0
539	Barnstaple	51 05	4 04	0000	-0015	-0155	-0245	-2.9	-3.8	-2.2	-0.4	0
540	Bideford	51 01	4 12	-0020	-0025	0000	0000	-1.1	-1.6	-2.5	-0.7	0
541	Clovelly	51 00	4 24	-0030	-0030	-0020	-0040	+1.3	+1.1	+0.2	+0.2	0
542	Lundy	51 10	4 40	-0025	-0025	-0020	-0035	+1.0	+0.7	+0.2	0.0	4.28
543	Bude	50 50	4 33	-0040	-0040	-0035	-0045	+0.7	+0.6	0	0	0
544	Boscastle	50 41	4 42	-0045	-0010	-0110	-0100	+0.3	+0.4	+0.2	+0.2	4.02
544a	Port Isaac	50 35	4 50	-0100	-0100	-0100	-0100	+0.5	+0.6	0.0	+0.2	4.13

SEASONAL CHANGES IN MEAN LEVEL

No.	Jan. 1	Feb. 1	Mar. 1	Apr. 1	May 1	June 1	July 1	Aug. 1	Sep. 1	Oct. 1	Nov. 1	Dec. 1	Jan. 1
476 - 482	+0.1	0.0	0.0	-0.1	-0.1	-0.1	0.0	0.0	0.0	0.0	+0.1	+0.1	+0.1
482a - 512	0.0	0.0	0.0	0.0	0.0	0.0	-0.1	0.0	0.0	0.0	+0.1	+0.1	0.0
513 - 534	0.0	0.0	0.0	-0.1	-0.1	-0.1	0.0	0.0	+0.1	+0.1	+0.1	0.0	0.0
535 - 544a	+0.1	0.0	0.0	-0.1	-0.1	-0.1	0.0	0.0	0.0	0.0	+0.1	+0.1	+0.1

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